

University of Southern Queensland
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Investigation into implement status awareness for autonomous tractors

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Abstract

Autonomous tractors are becoming more prevalent within agriculture. However, there is one thing that is hindering these machines from taking the role of an operator. The driver is currently the perception of the tractor and the only system that can stop the machine if something is about to or does go wrong. Developing a system that allows the tractor to have a better understanding of what it is doing and how its implement is operating will mean the requirement to have an operator sitting in the tractor seat is decreased.

The aim of the project is to determine if information exchanged via a tractor's CAN Bus system can provide a sense of machine perception for autonomous applications.

The first part of the project involved designing a testing methodology that allowed a range of implements and operating conditions to be tested. From the testing methodology, a system was set up to collect messages from a range of given sensors on the tractor via the CAN Bus system. The testing was then carried out following the designed procedure while recording the operating status of the tractor to a computer. This raw data was then sent to John Deere to be converted from hexadecimal into usable Matlab file format. The data was then exported into Excel for further analysis and graphing.

From the results analysis, it can be concluded that the engine % load is the best indicator of an issue occurring with the implement. Rear hitch height, engine fuel usage and engine RPM are also parameters that showed promising results.

Overall, the sensitivity of the in-built sensors is not suitable without refinement to provide a good understanding of what the implements status is. This project has shown that CAN Bus based implement awareness systems have potential, however a large amount of refinement and work needs to be completed to ensure the system is consistent and reliable, and sufficiently responsive to allow an autonomous tractor to operate safely and efficiently.

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Sam Green



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Abbreviated Terms

ATTA – AutoTrac Turn Automation

CAE – Centre for Agricultural Engineering (USQ)

CAN Bus – Controller Area Network Bus

ECU – Electronic Control Unit

GPS – Global Positioning System

PTO – Power Take Off

SCV – Selective Control Valve

Chapter 1 Introduction

1.1 Background

Agriculture will always be a growing industry as there will always be a requirement to feed the ever-expanding worldwide population. It is predicted that the world's population will be 10 billion by 2050, 3 billion more than in 2010. Agriculture will need to produce 56% more food by 2050, meanwhile suitable land is constantly being consumed by expanding cities and towns (Ranganathan et al. 2018). The large push towards reducing greenhouse gasses in the last couple of decades is also impacting agriculture as it contributes approximately 13% of Australia's greenhouse gas emissions (Climate Council 2021). In an attempt to improve the efficiency of farming, and make better uses of the resources available, autonomous tractors have been developed to undertake the monotonous jobs that have previously been undertaken by farmers.

Self-driving tractors have been around since the 1920's when Frank Zybach devised a tractor guide that would lead the machine along concentric circles around the field (Arens 2021). While this development occurred very early on, limited improvement occurred until the 1990's where the Silsoe Research Institute developed a driverless tractor system designed for vegetable and root crops. The modern autonomous tractor as we know it today wasn't established until the introduction of the ITEC Pro guidance system from John Deere which allows field operations such as navigation and end turns to be performed (Bear Flag Robotics 2022). The further release of Deere's AutoTrac Turn Automation in 2017 allowed the automation of end turns where-by controls such as lifting the hydraulics or 3-Point linkage can be performed by the tractor without the intervention of the driver (Spudman 2017). Autonomous tractors are heavily reliant on sensors to determine how both the machine and implement are operating. Sensors such as seed counters for each individual row have been built into planters and other implements for many years. The autonomous tractor itself has a variety of cameras and other sensors to guide it through the field and avoid obstacles when required. This technology has been crucial in the formulation of autonomous tractors as we know them today. The sensors of more advanced and modern implements communicate to the tractor via the CAN Bus, however the tractor does not have a way of determining the operating condition of simpler implements that don't have their own on-board

sensor systems such as cultivators, deep rippers or PTO mulchers. Investigation needs to be undertaken to determine if any existing sensors on the tractor can be related to the operating conditions of the implement, and if they would be suitable to be used as a control method for the tractor.

The outcome predicted from this research project is to provide an understanding of what sensors are already used on modern tractors, and how they can be used to provide an autonomous tractor a better interpretation of the state of operation of the implement behind it.

1.2 Project Aim

The aim of the project is to determine if information exchanged via a tractors CAN Bus system can provide a sense of machine perception for autonomous applications.

1.3 Project Objectives

- Develop a test procedure to simulate various field operational issues to assess machine perception.
- Assess the utility and sensitivity of information exchanged on a tractor CAN Bus for machine perception purposes.
- Develop recommendations for CAN Bus based perception systems that inform autonomous operations.

Chapter 2 Literature Review

2.1 Summary

The purpose of the literature review is to investigate, analyse and evaluate autonomous tractors and their sensor systems. The development of autonomous tractors continues to grow, and modern implements are evolving to communicate their state of operation with the tractor to allow the autonomous tractors to make decisions based on the outputs of the sensors. However, there is currently no way for these smart tractors to understand how a simple implement is operating as this is usually undertaken by the driver. While many implements in the future will have their own computer systems, there are many machines that will not, and therefore a tractor-based sensor system would be ideal as it would work with all types of implements.

2.2 Autonomous tractors and the need for perception

It is critical that an autonomous tractor can operate in the field without human interaction, however, still be able to take commands from the remote operator. As a result of previous work in this field, Blackmore et al. (2004) recommended the following features should be demonstrated by an autonomous tractor in the field:

- Remain in a safe and controlled operation state, especially in the case of a partial system failure
- Ability to operate with and around other machines in a co-ordinated manner
- Send and receive information wirelessly in regard to tasks to complete and operating status
- Be able to undertake a large variety of farming operations

To complete these tasks safely, autonomous tractors use on board sensors to detect obstacles including people, animals and other vehicles that may enter into the safe operation zone of the machine (Stentz et al. 2002). It is also critical that the tractor can interact and have an awareness of unstructured environments such as natural terrain allowing it to gain navigational control and optimise machinery operations (Baillie et al. 2017).

While an autonomous vehicle must understand its immediate surroundings, it is also important that it can monitor and understand what the implement is doing. Through environment, vehicle and implement monitoring, the state of operation can be determined. Using the information from on board sensors, the tractor can adjust its operating parameters to best perform the job at hand (Jensen 2022). Noah Schwartz, a head perception engineer at Bear Flag Robotics “says there are a lot of robust AI (artificial intelligence), models and algorithms built into the system to ensure the tractor has a constant feed of high-quality information about what is going on in its environment” (Jensen 2022).

Perception in autonomous tractors is an essential requirement to allow the machine to detect issues before they become a safety hazard and endanger the lives of nearby people or cause damage to property. Driverless equipment in agriculture has a major disadvantage when compared to automated robots in factories, the machines have to operate around the general public. Given the autonomous tractors are operating in the public’s eye, they must be seen to be doing the correct thing at all times. It would only take a single “news report of a malfunctioning machine crashing into a neighbour's yard or a machine that fails to recognise a dog or child and runs [them] over to spark a firestorm of negative publicity” (Lowenberg-DeBoer 2002). When an issue arises and harm is caused to either the operator, the public or someone’s property, there is a legal requirement to compensate the victim. There is major concern as to who will take the blame if an autonomous tractor were to cause harm. In terms of autonomous robots, faults can be considered a machines fault and therefore the machine is responsible or the programmer or manufacturer who designed the system. Currently it is accepted that the autonomous machines are not smart enough to be able to cause an issue if they are designed and programmed correctly. Current legal frameworks show that the manufacturer or programmer of the machine will most likely be held responsible in the case of an accident (Petrovic 2021).

Research work completed by Torrance (2020) investigated autonomous tractors and developed a comparative test procedure for the assessment of performance of autonomous tractors. Prior to the Torrance (2020) investigation, the only standardised comparative testing criteria that assesses the mechanical capabilities for tractors was the Nebraska Tractor Test (Nebraska Tractor Test Laboratory 2022). The aim of the Nebraska Tractor Test is to compare the functions and capabilities of different makes and models of tractors so they can be compared to allow the farmer to choose the most appropriate tractor for their operations (Torrance 2020). The Nebraska Tractor Test only assesses the mechanical performance of the tractors and does not consider the usability

or control capabilities. There has been work by Desai (2012) which adds usability requirements to the typical tractor test by including row width adaptation and manoeuvrability tests for the row crop tractors; these tests however are currently not universally accepted. Torrance's work further developed the tractor testing procedures by adding tests more suited to autonomous tractors and how capable current tractors are at being autonomous (Torrance 2020).

2.3 The CAN Bus system on modern agricultural machinery

Most modern tractors utilise a controller area network (CAN) Bus system for controller and sensor communication within the machine and certain implements. The CAN Bus is a two-wire communication system whereby all information has a given CAN address. This system allows sensors to broadcast information to the rest of the system where it can be accepted by its respective controller (CSS Electronics 2022). A diagram showing the typical setup of a CAN Bus communication system can be seen in Figure 1. (Maurizfa et al. 2020)

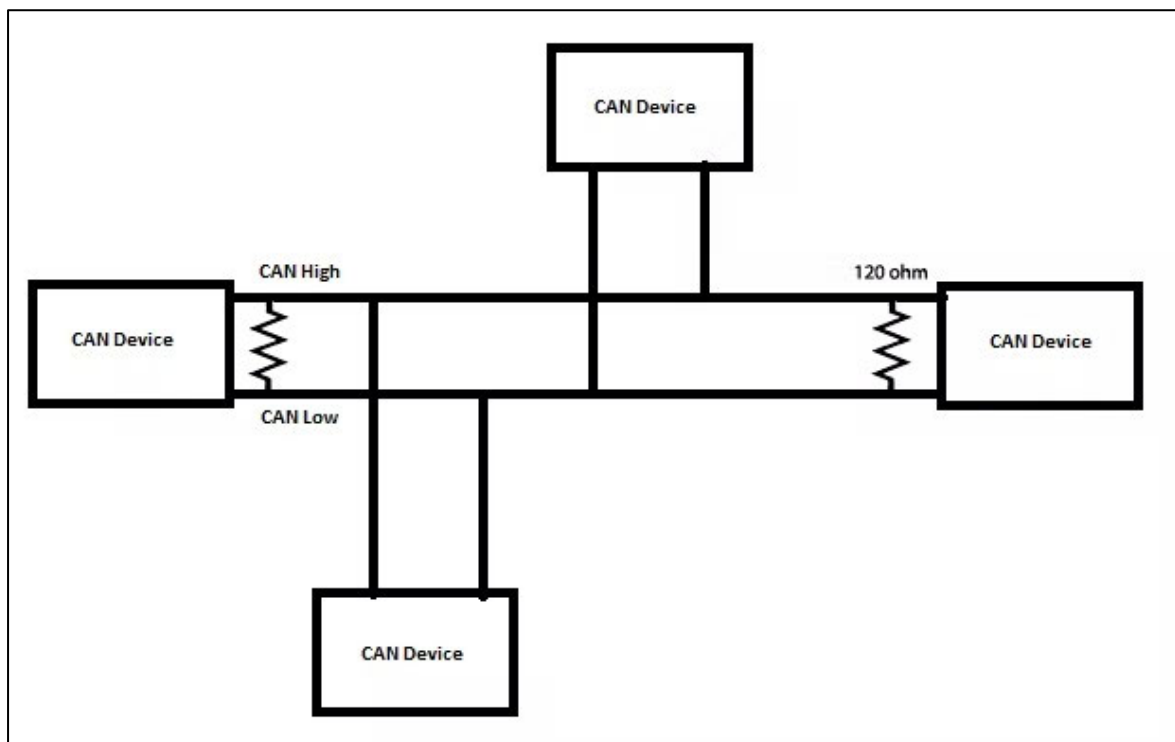


Figure 1 - Basic CAN Bus wiring diagram (Maurizfa et al. 2020)

CAN Bus systems allow an increase in machine productivity, more rapid problem diagnosis and a method for implements to communicate with the tractor. The CAN system is standardised across many industries using the Society of Automotive Engineers standard SAE J1939 (Copperhill Technologies 2022). This standard allows the diagnostics and control of machine operating parameters including engine control, transmission control, brake control (Marx 2015). As a subdivision of SAE J1939, the International Organisation for Standardisation (ISO) created ISO 11783 which is defined to be the universal standard for CAN communication and serial control for agricultural and forestry machinery (John Deere 2013). One of the major sections of ISO 11783 is the ability for the on-board computer to communicate with the implement. This allows sensors on the implement to be seen by the tractor as well as the tractor being able to pass control information back to the implement such as a sprayer or planter (Tohunny Van Do 2021).

Electronic control units built into the machine communicate the information necessary for effective management from the internal sensors via the CAN Bus. Sensors are located throughout the machine, especially the engine, gearbox and cabin, allowing the machine to understand its operation state (Čupera & Sedlák 2011). The CAN Bus allows sensors to communicate with the machine, however, it also allows controllers to send information and commands to actuators and control elements that can change the operating state of the machine to improve efficiency and productivity.

The CAN Bus also allows quicker diagnosis of issues in the electrical system. Communication with John Deere machines occurs via the Service ADVISOR™ computer program. Using an Electronic Data Link (EDL) and the Service ADVISOR™ program, the technician can observe and trace communications between controllers on the machine to track down issues (John Deere 2013).

2.4 Sensors and technology that are on the tractors currently

Modern machinery consists of technology and sensors that allow the operator and the machine to have a greater understanding of its operating status. The control elements of the tractor communicate with the various sensors via the CAN Bus system and the Electronic Control Unit (ECU). Figure 2 shows the communication between the ECU and the other nodes of the CAN Bus system.



Figure 2 - Diagram of tractor systems interaction with a telematics device (Didmanidze et al. 2021)

The tractors control and sensor system can be broken into 5 major groups, (Didmanidze et al. 2021)

- Transmission
- Engine
- Hydraulics
- Drivetrain
- Navigation

Within these groups there are individual controllers that talk to each other and the respective sensors for that sub-section. Below is a list of sensor values that have been found on the CAN of a John Deere 6120R that may be useful to determine the general operational characteristics of the tractor and implement.

- | | | |
|-------------|------------------------------|----------------------------------|
| • Time | • Roll | • Engine Crankcase Pressure |
| • Latitude | • Speed | • Engine Fuel Rate |
| • Longitude | • Wheel Based Vehicle Speed | • Engine Fuel Temperature |
| • Altitude | • Engine Coolant Temperature | • Engine Intercooler Temperature |
| • Course | | |
| • Pitch | | |

- Engine Oil Temperature
- Engine Speed
- Req Engine Speed
- IVT Set Speed
- Rear Hitch Height
- Transmission Oil Temperature
- Engine Load
- Rear PTO Speed

The research undertaken by Torrance (2020) determined that the John Deere 6120R was a reasonably well suited to autonomous operations due to advanced headland management and operational safety protocols, however the tractor is limited from driverless capabilities due to a lack of depth perception and awareness of its surroundings.

While not directly related to the agriculture industry, autonomous vehicle standards and information can be drawn from the automotive industry. SAE J3016 provides a framework that defines a vehicles level of automation. A cars automation can be classified into 6 levels ranging from level zero where a vehicle will provide warnings and temporary assistance through to level five where complete driverless capabilities are available in all driving conditions (Shuttleworth 2019). The intermediate levels and their characteristics can be seen below in Figure 3.

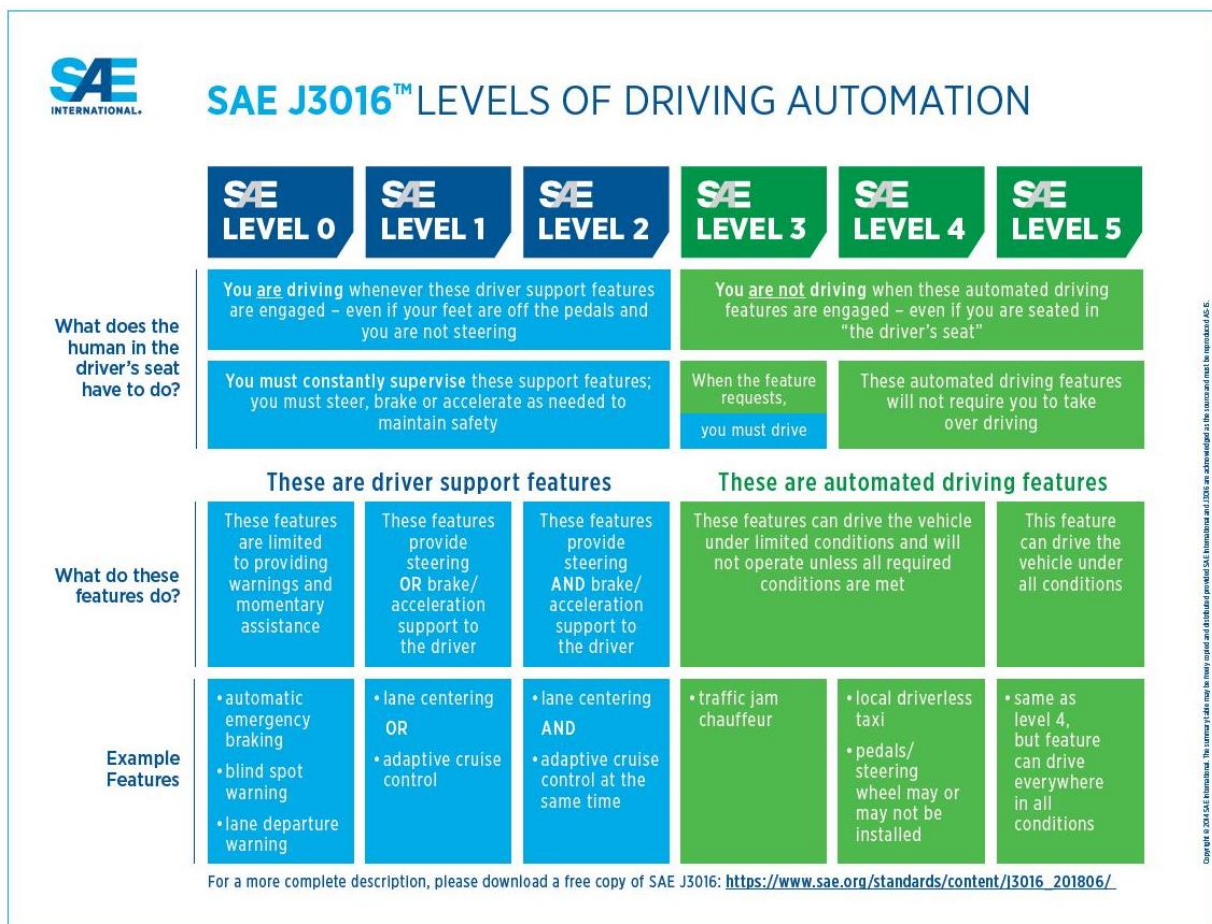


Figure 3 - Graphical representation of SAE J3016 (Shuttleworth 2019)

A similar description has been developed by Case IH Agriculture where there are 5 levels of automation for agriculture; guidance, coordination and optimisation, operator assisted autonomy, supervised autonomy and finally full autonomy (Case IH 2022). Figure 4 shows Case IH's adaptation of the automation levels.

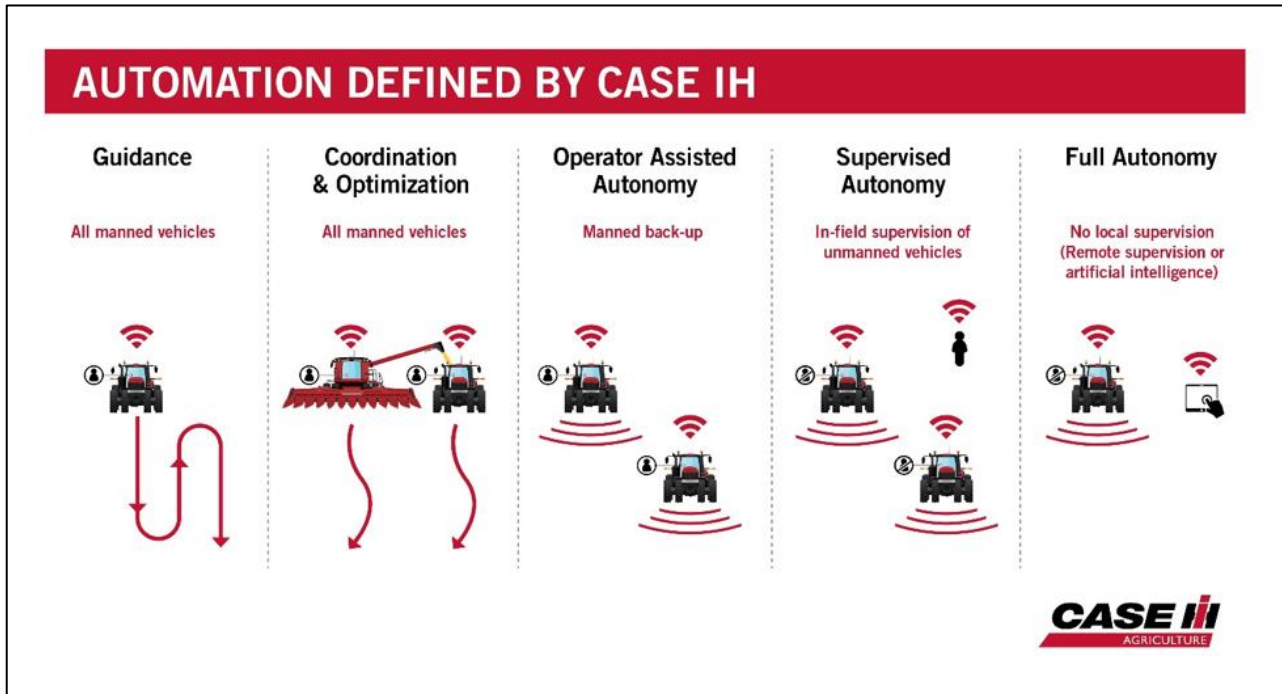


Figure 4 - Levels of automation described by Case IH (Case IH 2022)

Guidance is based around GPS technology and allows the tractor to operate along a prescribed track. Coordination and optimisation is a level that allows communication between vehicles in the field, as well as path planning. Operator assisted autonomy involves automatic and manual adjustments of the implement and tractor while an operator remains in the vehicle for supervision. Supervised autonomy is the control of multiple machines from only one operator, the operator controls one machine while the others talk to the leading machine to receive operating parameters and desired conditions. Full autonomy allows the machines in the field to be operated from a remote point without the requirement for human intervention, however, this requires the capacity for perception and implement awareness (Case IH 2022).

For John Deere to consider a tractor to be autonomous, it must comply with level four or above. Currently, the 6120R can be considered a level three due to its advanced AutoTrac Turn Automation (ATTA) which allows the tractor to steer, change the throttle and control the implement before

completing a headland turn, however it still requires human intervention to activate the turn sequence (Torrance 2020). For the tractor to develop to a level four, it requires a system that will allow it to operate without any human intervention.

2.5 Testing equipment and procedures

Prior to using any of the equipment, it is critical to determine suitable operating speeds and depths. Through investigation it was found that 3kph is the most suitable speed for PTO mulching as seen in Figure 5. The operation depth was set to be 150mm as this is what the machine was set to from the previous use.

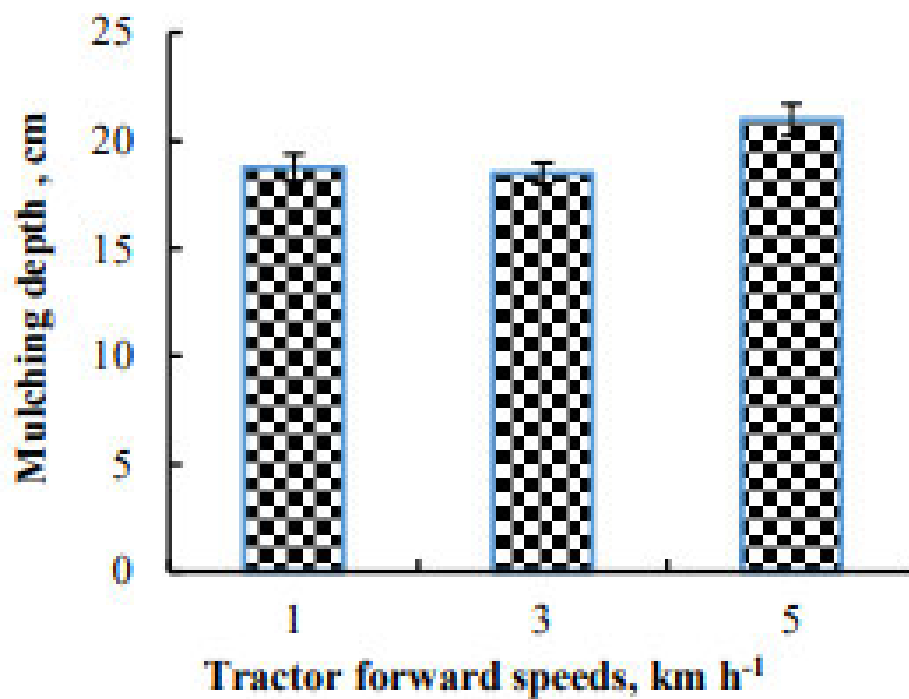


Figure 5 - Operating speeds of a PTO Mulcher (Jahun et al. 2021)

2.6 Real world issues for the tractor in an autonomous state

Tractors are currently heavily dependent on the operator in a perception sense. The operator is essential to stop the tractor in the case that an issue may occur with the machine or implement. Using sight and sound and relating back to previous experience, an operator can usually sense an issue when it occurs.

Based on the chosen operating states of an autonomous tractor being transport and 3-point linkage deep ripping, the following list of common operating issues has been developed. The issues listed below are concluded based upon previous experience operating the given machinery in the field.

Transporting

- Travelling too fast over rough terrain causing unnecessary shakes, vibrations and loads on the tractor and implement

3-point linkage deep ripper

- Ripper shank breaks off or shear pin breaks as a result of overload from hitting rocks or other obstacles in the ground
- Ripper begins to dig in too far causing the tractor to lose traction or stall as a result of incorrect operating height
- Bridging occurs across a number of tines of the ripper which results in a block up commonly caused by stringy plant material or debris laying on the surface of the soil
- Ripper is not engaged with the ground far enough causing improper soil disturbance due to incorrect operating depth
- The 3-point linkage is not lifted prior to the headland and beginning the turnaround sequence as a result of machine process error which may cause high loads on the tractor and ripper
- Rapidly changing ground incline causing the ripper to dig in further or not enough due to the tractor not changing 3-point linkage height to keep constant ground engagement depth

Using these known failure modes, an experimental procedure can be designed to replicate them in a controlled and repeatable manor so that data can be collected that will provide an insight into the sensitivity of the on-board sensors and their suitability to monitor what the implement is doing.

2.7 Knowledge Gap and Study Justification

Through an investigation of existing literature in the autonomous tractor field, it was found that there is currently no system that can detect the implements operation status using the sensors that are already built into the tractor. Therefore, the focus of this research project is to build on information gathered from both automotive industries and other agricultural work, to determine if existing sensors can provide a sense of machine and implement perception for autonomous applications.

Based on information gathered during the literature review, it is considered that the proposed project will be attainable and useable in the future. Findings gathered from this project will inform the agricultural industry as a whole, but more specifically the autonomous tractor industry. It will provide a development in autonomous technology and potentially provide the required steps to create a fully autonomous tractor based on existing tractor technology.

Chapter 3 Methodology

This chapter will consist of the formulation, development and analysis of a data collection and testing procedure to determine if an implement can be monitored through the existing CAN Bus data of the tractor. The testing procedure from which data will be collected from has been developed based upon information found during the literature review stages of the report. The testing procedure developed in this chapter will allow the implementation of experimental testing in the following chapter. This research also allows the developed testing procedure to be evaluated to determine its suitability for real world circumstances.

3.1 Research Focus

This research project draws on information and current standards from the agricultural industries while also implementing ideas and technologies from the transport and mining industries. The research aim and scope of the investigation can be seen in the following section.

3.1.1 Research Aim

The aim of this research is to determine if sensory information that is already on a tractor's CAN Bus system can provide a sense of machine and implement perception for autonomous applications. Analysis of the collected data from the designed testing procedure will allow conclusions to be drawn about the ability of the tractors sensors to determine the state of operation of the implement.

3.1.2 Research Scope

Due to the comprehensive nature of autonomous vehicles, and in particular, autonomous tractors within agriculture, the scope of this research project was narrowed down to allow for thorough

testing and analysis of a given problem. The project has been limited to John Deere tractors due to the resources such as the machine and data collection technology available at the time, as well as only a small variety of testing implements. This research project is a preliminary investigation into what sensors are available on current John Deere tractors, and whether they can detect issues and changes which may reflect the implements' operating status. Further development to this research may be carried out in the future with the aim of introducing it into autonomous tractors.

3.2 Project Methodology

Based on the scope of the research, the methodology of the project can be broken down into the following processes.

1. Conduct investigation into the process of data collection from the CAN Bus system of autonomous John Deere tractors.
2. Investigate which data may be useful in determining whether an issue may have occurred with the implement.
3. Secure machinery and site to allow testing to be undertaken safely and when required.
4. Develop an experimental procedure to simulate issues occurring on basic tractor implements that do not have their own sensor systems.
5. Conduct preliminary testing to verify that the data can be collected, and the testing procedure will be suitable, then if necessary, modify the testing procedure to ensure the correct data is collected.
6. Perform experiment procedure to capture data.
7. Process and evaluate the data collected in the experiments.
8. Present the findings of the experimental procedure and develop recommendations towards CAN Bus based perception systems in autonomous tractors.

3.3 Task Analysis

The following section of the report will provide a detailed understanding of how to set up the tractor, the implements being used and the data collection equipment. The first part of the method involves defining the preliminary methodology testing, this is then followed by the main body of the methodology and finally the data evaluation.

3.3.1 Preliminary methodology testing

Preliminary testing will be undertaken to ensure that the machines can be used and modified as required for the testing procedure to deliver the desired results. Performing this testing will allow any modifications to be undertaken regarding the methodology. Setting the machine up and using the implements will provide an understanding of how the data collection will operate.

Preliminary methodology to validate testing procedure

- Connect to CAN Bus system and log data performing simple operation such as driving through the field.
- Analyse data recorded to ensure suitable data has been collected and it is in a form that can be further analysed or displayed.

3.3.2 Testing Procedure

The modes of failure that have been identified are based on personal experience and general farming operations. Table 1 seen below shows the development of the possible modes of failure that may be encountered in the field for a 3-point linkage ripper and a PTO powered rotary hoe and in a general transport operating mode. The table also describes the general process of how the issue can be replicated in a controlled manor.

Table 1 – Issues encountered in the field and how they can be simulated in a controlled and repeatable manor

Implement	Modes of failure	How the issue can be simulated
3-Point linkage deep ripper	Base run	Run the tractor and ripper in the field to give a baseline data form to reference the rest of the ripper data from.
	Ripper shank shear pin breaks	Once completing the first pass, fit a smaller shear pin or bolt to the shank of the ripper that will result in the tine 'breaking off' when it reaches a buried piece of timber within the field.
	Ripper is digging in too far	With the ripper at a suitable operating height, complete a pass in the field. Then force the ripper to operate at a deeper depth to simulate an increased load on the machine.
	Bridging has occurred across 2 or more tines	Once the baseline run has been recorded, a timber board can be partially buried in the soil that is collected by 3 of the tines. This board then will create a bulldozing effect and collect the soil simulating a blockage.
	Ripper is not engaging in the ground enough	After the initial run, lift the ripper out of the ground so that less ground engagement is achieved and then repeat the testing procedure.
	Tractor fails to lift implement out of the ground prior to executing headland turn	Travel along with the implement in the ground, then reach the end of the run where the wheel tracks are most prominent in the headlands and lift up after the headland. This will mean that the ripper is operated through the more compacted areas of the field where it would typically be lifted up for the turn around procedure.
	Failure to react by lifting or lowering the 3PL when going through a washout	Operate the machine with the deep ripper through a washout without changing the 3PL height to apply loads to the tractor that it may not see in regular operation.

PTO powered rotary hoe	Base run	Operate the tractor and rotary hoe in the field under normal operating conditions to provide a reference for the rest of the PTO based data both in the field and on the dynamometer.
	Operating in already ripped ground	Operate the rotary hoe over a section of the field that has already been ripped with the deep ripper to provide different operating conditions to test the data collection methods.
No implement	Base run	Run the tractor in the field to get a base run of what to expect from the data and the machine.
	Hitting large ruts at speed in a transporting situation	Operating the tractor and driving through a pothole or washout and measuring the pitch, roll and other acceleration values from the GPS receiver.

The lists provided below are a more detailed description of the modes of failure and what operating parameters such as speed and cutting depth will be used.

No Implement

- Base run
 - Speed – 3kph, 5kph, 10kph
 - Travelling in a straight line using autosteer guidance
 - Operate in the field that the ripper testing will be carried out in
- Transporting
 - Speed – 3kph, 5kph, 10kph
 - Travel in a straight line using the autosteer guidance
 - Roughness of the ground (driving on rough cultivated ground)

3-Point linkage deep ripper

- Base run
 - Speed – 3kph, 5kph

- Travel in a straight line using the autosteer guidance
- Ripper depth of 200mm, 300mm, 350mm
- Operate the machine with the implement in the ground from one end of the field to the other then turn around and come back
- Ripper shank hear pin breaks
 - Speed – 3kph, 5kph
 - Travel in a straight line using the autosteer guidance
 - Ripper depth of 200mm, 300mm, 350mm
 - Fit pre-cut shear pin to the ripper
 - Bury a piece of timber in the soil half way along the run which will cause the shear pin to break and replicate a broken ripper shank
 - Operate the ripper at 300mm depth from one end of the field to the other with the timber in the middle of the run



Figure 6 - M24 Bolts used as shear pins for the ripper shank breakage testing



Figure 7 - Shear bolt installed in deep ripper ready for testing

- Ripper is digging in too far
 - Speed – 3kph, 5kph
 - Travel in a straight line using the autosteer guidance
 - Initial depth of 300mm then lower to 500mm half way through the run
 - Operate the machine at 300mm for half the run and then lower to 500mm while attempting to maintain the same ground speed, at the other end of the field, turn around and repeat the same process. Then repeat the process with a starting depth of 100mm.
- Bridging occurred across two or more tines
 - Speed – 3kph, 5kph
 - Travel in a straight line using the autosteer guidance
 - Ripper depth of 200mm, 300mm and 350mm
 - Boards of timber were screwed to the top of 2 tines as seen in Figure 8 to capture a large piece that is laying on the ground.
 - The large piece of timber is partially buried in the soil half way along the run, it will be picked up by the ripper shanks and then get caught under the screwed-on pieces causing the block up.



Figure 8 - Boards attached to the ripper shank to catch the large piece laying on the ground

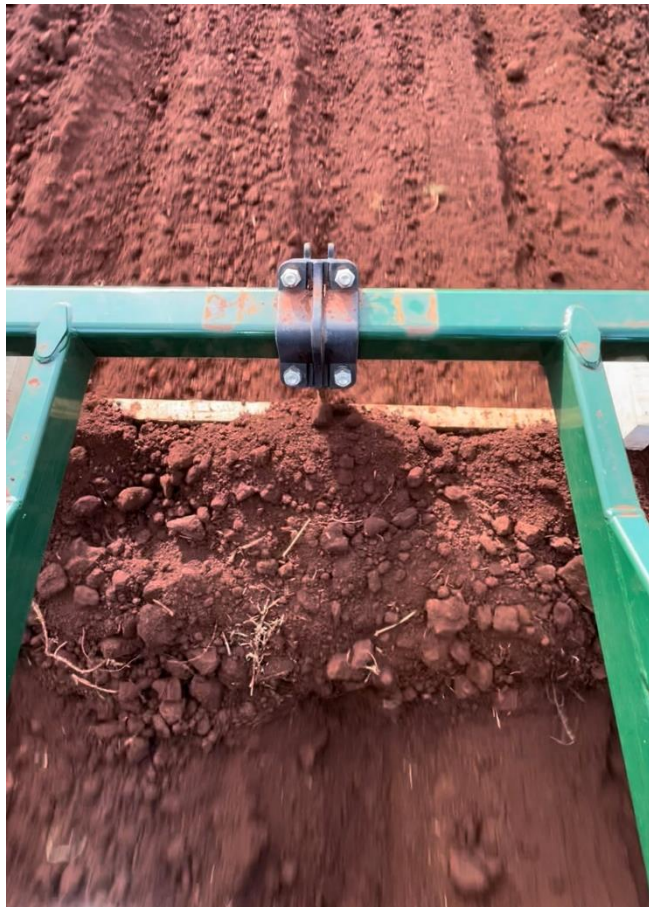


Figure 9 - Board of timber bridging 3 ripper tines causing a block up of soil

- Ripper is not engaging in the ground deep enough
 - Speed – 3kph, 5kph
 - Travel in a straight line using the autosteer guidance
 - Initial depth of 300mm then raise to 100mm half way through the run
 - Operate the machine at 300mm for half the run and then raise to 100mm while attempting to maintain the same ground speed, at the other end of the field, turn around and repeat the same process. Then repeat with a starting depth of 500mm.
- Tractor fails to lift implement out of the ground prior to headland turn
 - Speed – 3kph, 5kph
 - Travel in a straight line using the autosteer guidance
 - Ripper depth of 200mm, 300mm, 350mm
 - Operate the machine in standard configuration, however, continue with the implement in the ground into the headland area of the field to demonstrate a section that shouldn't be ripped in general field operation
- Failure to react to 3PL height when going through a washout
 - Speed – 3kph, 5kph
 - Travel in a straight line using the autosteer guidance
 - Ripper depth of 200mm, 300mm, 350mm
 - Operate the machine through a washout and keep the 3PL at the same height, this will result in less and greater levels of ripping depending on the angle of the implement relative to the ground



Figure 10 - Bank used to simulate the washout

PTO powered rotary hoe

- Base run
 - Speed – 3 kph
 - Travel in a straight line using the autosteer guidance
 - Rotary hoe depth of 150mm
 - Operate the machine in virgin ground that has not been ripped at the desired depth and speed to get a base line set of data
- Operating in pre-ripped ground
 - Speed – 3 kph
 - Travel in a straight line using the autosteer guidance
 - Rotary hoe depth of 150mm
 - Operate the machine in part of the field that has already been ripped to give an idea as to how the machine will operate in different working conditions

The testing matrix that was used in the field to ensure all required data was collected can be seen in Appendix A. The grey boxes indicate data that was not required or able to be collected, and the green boxes indicate the data that was collected.

3.3.3 Data Analysis

After recording the log files from the CAN Bus, the files were sent to Tyler Schleicher and Brandon McDonald from John Deere in the United States of America. There, the data was parsed which converts the CAN data format (hexadecimal) into Matlab format that can be easily interpreted. For ease of analysis, the required data variables were exported out of Matlab into Excel.

Once in Excel, graphs were made for the chosen parameters to allow them to be investigated. Various other comparative values are found in excel such as averages and variance, these values can be used to compare how the machine is operating before and after the issue has occurred.

From the Excel graphs, conclusions can then be drawn as to which parameters are the best indicator of when an issue has occurred. From the chosen parameters, the best 3 will be chosen that best depict or show when a mode of failure has occurred.

Data analysis method

- Analyse data to determine if there is a correlation between the data sources collected and the issue that was created on the machine.

3.4 Resource Analysis

The resources required to allow the completion of this research project can be seen below in Table 3.1. The financial costs of each item have also been included in the table to give an idea of the overall costs of the research. The main resources required for the project include the land for testing, the tractor to perform the data collection on, and the implements to use behind the tractor. These resources are already owned by UniSQ and have been provided to allow the research to be undertaken. The data collection equipment and software will be sourced from John Deere.

Table 3.1 – Resource Requirements

Resource	Source	Cost
Testing land	USQ	Owned
Tractor (John Deere 6120R)	USQ	Owned
Deep ripper	USQ	Owned
PTO mulcher	USQ	Owned
Timber Planks	USQ	Owned
CAN Case (CAN interpretation tool)	John Deere	Owned
Laptop with CAN Bus recording software (CAN Sniff)	Student	Owned
Data storage device	Student	Owned
General tools	Student	Owned
High-visibility vest	Student	Owned
Diesel (50 Litres)	Student	\$120
Shear bolts for the ripper	Student	\$50

The main cost for this project is the fuel to run the tractor as the majority of the equipment and supplies will be provided by the USQ, John Deere or the student. Fuel costs are high currently, however in the sense of a whole project it is very affordable. An exact cost value for the fuel cannot be provided, however an estimation is formed for the sake of the resource requirements and planning process.

3.4.1 John Deere 6120R Tractor

The John Deere 6120R is a 2020-year model tractor that UniSQ uses to carry out general agricultural operations and to undertake testing and experimental works. The tractor has an IVT transmission that is controlled by the CAN Bus system and allows the operator to vary the travel speed infinitely. Another benefit of the IVT transmission is the ability of the tractor to reduce the gearing and increase engine revolutions automatically as the implement demands more power. The tractor is fitted with AutoTrac guidance thanks to a Starfire 6000 GPS receiver and in-built steering control valve. As the tractor is of recent build, many of the controls such as the SCV's (hydraulic remotes), PTO, 3-point linkage and other touch buttons within the cab are transmitted via the CAN Bus. All of the sensors within the tractor are also communicated with via the vehicle CAN Bus allowing the readings from the sensors to be found in one place. Images of the tractor and the Starfire 6000 receiver can be seen below in Figure 11 and Figure 12.



Figure 11 - John Deere Starfire 6000 GPS receiver that is fitted to the 6120R



Figure 12 - John Deere 6120R tractor provided by UniSQ

3.4.2 Deep Ripper

The first implement chosen for the data collection section of the research project is a Gyrat deep ripper. This implement is owned by UniSQ and will be an ideal attachment for the tractor as issues can easily be simulated such as removing a tine or blocking up the area between two tines to increase drag. The deep ripper is simple and does not consist of any state of operation sensors, and therefore is ideal for this testing. The deep ripper will provide a draught load to the tractor using the 3-point linkage system which can be analysed on the CAN Bus. The lift forces applied on the 3-point linkage from the ripper in different field conditions can also be investigated. An image of the deep ripper can be seen in Figure 13.



Figure 13 - Gyrat deep ripper fitted to the John Deere 6120R tractor

3.4.3 PTO Mulcher

The second implement chosen for the testing procedure is a PTO mulcher which will provide a load to the tractor in terms of draught as well as PTO load. The reaction of the mulcher on the 3-point linkage in different field conditions can also be investigated. The mulcher used in the data collection can be seen in Figure 14.



Figure 14 - PTO powered mulcher mounted on the back of the UniSQ 6120R

3.4.4 CanCase CAN Bus Communication Device

Connecting to the tractors CAN Bus system using a computer requires a CANcase and a special harness that allows connection to the diagnostics port of the John Deere tractors. The CANcase supplied by John Deere is a Vector CANcaseXL as seen below in Figure 15. The harness used to connect the CANcase to the diagnostic port can be seen in Figure 16. The harness consists of CAN low and high wires for both the vehicle and implement CANs as well as a ground wire that serves as a reference plane for the data messages.



Figure 15 - Vector CANcaseXL that was used to communicate with the CAN Bus on the Joh Deere 6120R



Figure 16 - Diagnostic connector and harness used for CAN Bus communication

3.4.5 Can Sniff CAN Recording Software

To record the CAN Bus data through the CANcaseXL, CAN Sniff software is required. This program runs and creates a log file from information received via the USB cord from the CANcase. It was provided by John Deere to allow me to collect the data in the field.

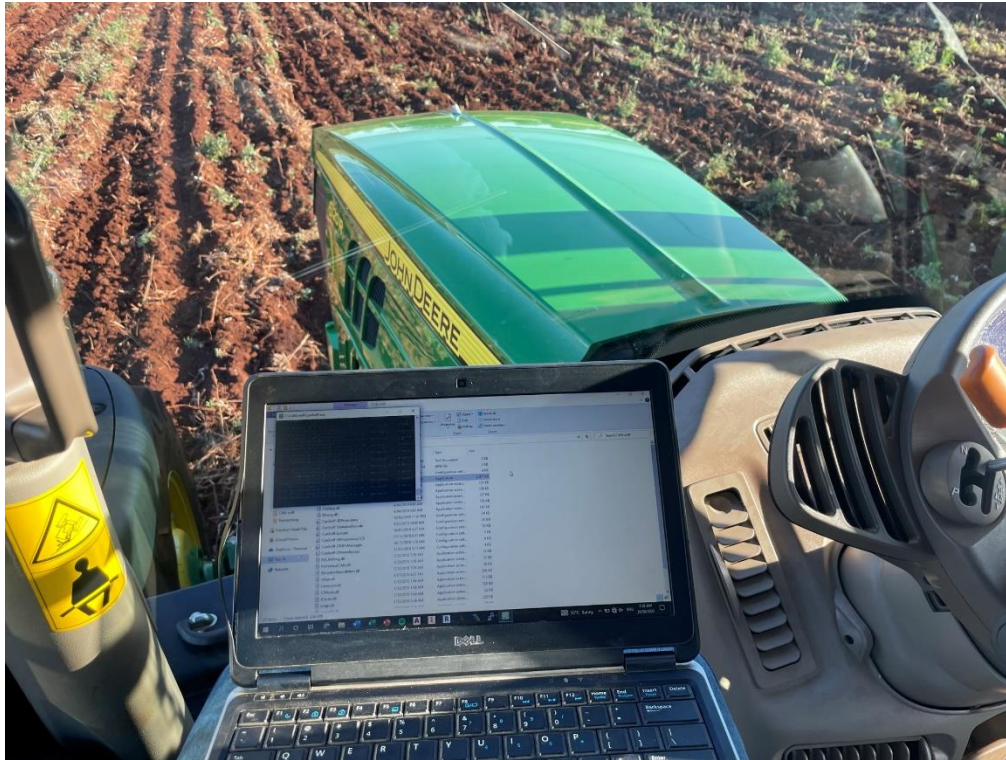


Figure 17 - Recording CAN Bus data using CANsniff software

3.4.6 Test Area

The layout plan as seen in Appendix C shows a map of the rear CAE plot and where the data will be collected. Some of the data was also collected in other areas of the CAE due to changes in field conditions and finding ideal spots to undertake each given test.

3.4.7 Camera recording setup

It was decided that it would be beneficial to record the bridging and shear pin breaking tests using

a camera. This would allow the exact time the issue occurred to be recorded and correlated back to the data recorded from the CAN Bus. Using extruded aluminium and t-nuts, a frame was constructed on the back of the deep ripper that a phone could be attached to. This held the phone in a stable position so that videos of the testing could be captured, the camera frame can be seen below in Figure 18 and Figure 19. The chosen placement for the frame allowed the tines of the ripper to be seen as well as in front and behind, an example of the field of view from the camera can be seen in Figure 20.



Figure 18 – Camera frame for videoing the data collection



Figure 20 – Camera frame for videoing the data collection

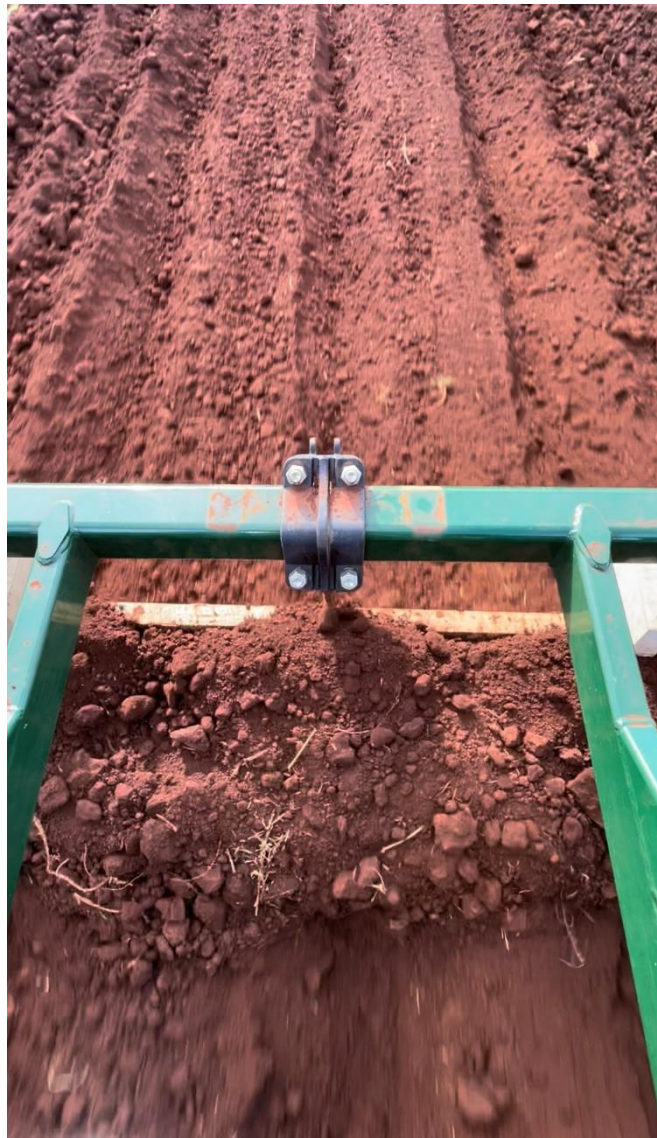


Figure 19 - Field of view from the camera mounted on the frame

Chapter 4 Results

4.1 Chapter Overview

The purpose of this chapter is to outline the outcomes of the experimental testing process and assess the data obtained. The data collection method is described within the methodology section of this report.

The essential information gathered from the data collection process is presented in Section 4.2 of this chapter. Each section of data also includes a short description including testing set up, observations made during the testing and other issues or notes that are important.

4.2 Testing Results

After analysing the raw data from Matlab, the list of parameters seen below were chosen based on their potential usefulness in determining implement status. General values such as the time and location of the machine were used provide an understanding of what the machine is doing. More advanced parameters such as engine load and fuel usage are the ones analysed to determine their suitability for implement awareness.

- | | |
|---|--|
| <ul style="list-style-type: none">• Day• Hours• Minutes• Seconds• lat_deg• long_deg• altitude_m• course_deg• pitch_deg• roll_deg• speed_kph• WheelBasedVehicleSpeed_kph• EngineCoolantTemp_degC | <ul style="list-style-type: none">• EngineCrankcasePressure_kPa• EngineFuelRate_lph• EngineFuelTemp_degC• EngineIntercoolerTemp_degC• EngineOilTemp_degC• EngineSpeed_rpm• ReqEngineSpeed• IVTSetSpeed1F_mps• RearHitchCurrentPosition_percent• TRF1_TransmissionOilTemp_degC• EngPctLoadatCurrSpeed_pct• RearPTOOutputShaftSpeed |
|---|--|

Figure 21 - Parameters exported out of Matlab and into Excel

Once in Excel, these values were graphed and it was concluded that not all of the parameters were proving anything, and therefore 7 (8 including PTO RPM for the PTO testing) parameters were chosen for further analysis. These parameters include:

- Speed
- Wheel-based speed
- Engine RPM
- Engine coolant temperature
- Engine fuel rate
- Engine % load
- Rear hitch height
- Rear PTO RPM

These seven parameters were plotted together on the same graph for each of the tests whereby data was collected. These graphs can be found in Appendices D through to N. It is important to note that the Engine RPM being a large number was graphed on a secondary y-axis to provide a reasonable resolution for the remaining parameters which were graphed on the primary vertical axis. All of the parameters are graphed against a progressive time value in seconds that starts when the data recording was commenced. Some of the parameters such as the speed and wheel-based speed are challenging to gauge when graphed on this scaled axis and so for clearer investigation, the seven parameters were graphed on their own.

The mean and standard deviation of the base run data was found for each of the three implements for their respective speeds and operating depths. The values 3 standard deviations above and below the mean were also found to provide a confidence window that 95% of the data should fall within. This information was only found on the base run data and then utilised in each respective test to provide a baseline reference.

The graphs for the individual parameters also contain the mean and $\pm 3SD$ values for their respective base run to provide a baseline that can be referenced between tests. All of the individual graphs can be seen in Appendices D through N for each mode of failure and operating speed and depth.

After graphing the seven parameters individually, five were chosen to be further analysed. Those chosen include percentage engine load, speed, engine fuel rate, rear hitch height and engine RPM.

Using these refined parameters, the mean and variance can be found for each test prior to and after the issue has occurred. The differences in the averages between the initial operating state and the final operating state can be found to provide a value of the amount of change or each parameter in the event of an issue occurring. The difference between the variances is also found as another measure of change of operating conditions.

4.2.1 No Implement

4.2.1.1 Base run

3kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 3kph no implement testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	29.942	3.056	7.191	2.957	84.741	92.020	1899.969
Std Dev	1.337	0.052	0.382	0.012	0.395	0.151	1.544
3 Std Dev	4.012	0.155	1.147	0.036	1.186	0.454	4.633
Mean + 3SD	33.954	3.212	8.338	2.993	85.927	92.474	1904.602
Mean - 3SD	25.930	2.901	6.044	2.922	83.554	91.566	1895.336

5kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 5kph no implement testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	34.423	5.103	8.514	4.952	84.000	92.027	1900.031
Std Dev	1.528	0.094	0.460	0.026	0.000	0.178	2.389
3 Std Dev	4.583	0.281	1.380	0.077	0.000	0.533	7.168
Mean + 3SD	39.006	5.384	9.894	5.029	84.000	92.560	1907.198
Mean - 3SD	29.840	4.822	7.133	4.874	84.000	91.494	1892.863

10kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 10kph no implement testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	49.005	10.160	12.589	9.918	76.298	92.000	1900.259
Std Dev	3.908	0.280	0.860	0.218	1.257	0.000	6.509
3 Std Dev	11.723	0.840	2.580	0.654	3.771	0.000	19.526
Mean + 3SD	60.728	10.999	15.169	10.572	80.070	92.000	1919.785
Mean - 3SD	37.282	9.320	10.009	9.265	72.527	92.000	1880.733

4.2.1.2 Transporting

The start and end cells are chosen based on when the actual testing process began and finished as the start of the recording isn't necessarily when the tractor was in its operating state. These values are slightly different for each table and therefore adjusted values can be seen.

3kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 1 to 787 as seen by the start and end cell values. These values are shown for each of the 5 parameters. It can be seen that the variance within the testing period was not very high.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	1	787	32.959	9.820
Speed			3.056	0.069
Engine Fuel Rate			8.194	5.170
Rear Hitch %			92.175	0.194
Engine RPM			1900.000	0.159

5kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 1 to 419 as seen by the start and end cell values. These values are shown for each of the 5 parameters. Very little variance can be seen from the data as seen in the table below.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	1	419	35.857	6.301
Speed			5.090	0.134
Engine Fuel Rate			8.951	2.223
Rear Hitch %			93.200	0.000
Engine RPM			1900.060	0.330

10kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 40 to 212 as seen by the start and end cell values. These values are shown for each of the 5 parameters. There is a rather large variation in the engine load throughout this test, due to a varying load, it is also expected that the fuel usage rate has some variability as seen below.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	40	212	44.002	35.422
Speed			10.128	0.185
Engine Fuel Rate			11.472	17.355
Rear Hitch %			93.013	0.204
Engine RPM			1899.855	3.415

4.2.2 3PL Deep Ripper

4.2.2.1 Base run

350mm - 3kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 350mm depth of cut, 3kph 3PL deep ripper testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	56.172	2.507	14.709	2.878	87.206	22.236	1899.962
Std Dev	3.243	0.111	0.753	0.038	1.966	1.503	3.928
3 Std Dev	9.729	0.333	2.259	0.114	5.898	4.509	11.783
Mean + 3SD	65.901	2.841	16.968	2.992	93.104	26.745	1911.745
Mean - 3SD	46.443	2.174	12.450	2.763	81.307	17.727	1888.178

350mm - 5kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 350mm depth of cut, 5kph 3PL deep ripper testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	68.326	4.766	17.503	4.954	85.122	26.195	1900.009
Std Dev	4.018	0.111	0.897	0.023	1.344	1.667	6.765
3 Std Dev	12.054	0.334	2.690	0.068	4.031	5.002	20.296
Mean + 3SD	80.380	5.101	20.193	5.022	89.153	31.197	1920.305
Mean - 3SD	56.271	4.432	14.814	4.885	81.091	21.194	1879.713

300mm – 3 kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 300mm depth of cut, 3kph 3PL deep ripper testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	44.001	2.988	11.507	2.959	88.186	31.124	1900.053
Std Dev	2.803	0.063	0.829	0.029	0.483	2.155	4.229
3 Std Dev	8.409	0.188	2.486	0.088	1.450	6.465	12.688
Mean + 3SD	52.410	3.176	13.993	3.047	89.636	37.589	1912.741
Mean - 3SD	35.592	2.800	9.022	2.872	86.736	24.659	1887.365

300mm – 5kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 300mm depth of cut, 5kph 3PL deep ripper testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	50.797	5.084	13.358	4.951	87.588	34.309	1899.934
Std Dev	3.320	0.080	0.779	0.026	1.052	1.288	7.249
3 Std Dev	9.960	0.240	2.338	0.079	3.155	3.865	21.748
Mean + 3SD	60.758	5.323	15.696	5.030	90.743	38.175	1921.682
Mean - 3SD	40.837	4.844	11.020	4.871	84.432	30.444	1878.186

200mm – 3kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 200mm depth of cut, 3kph 3PL deep ripper testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	34.867	3.115	8.627	2.959	87.677	42.481	1900.015
Std Dev	1.520	0.047	0.452	0.025	0.623	1.346	2.419
3 Std Dev	4.560	0.140	1.355	0.076	1.870	4.038	7.256
Mean + 3SD	39.427	3.255	9.982	3.035	89.547	46.520	1907.270
Mean - 3SD	30.308	2.975	7.272	2.882	85.807	38.443	1892.759

200mm – 5kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 200mm depth of cut, 5kph 3PL deep ripper testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM
Mean	44.218	5.148	11.603	4.954	84.496	40.605	1899.950
Std Dev	2.834	0.076	0.809	0.019	0.968	1.486	5.880
3 Std Dev	8.503	0.229	2.428	0.057	2.904	4.457	17.640
Mean + 3SD	52.721	5.377	14.031	5.011	87.400	45.063	1917.590
Mean - 3SD	35.715	4.919	9.175	4.898	81.592	36.148	1882.310

4.2.2.2 Ripper shank shear pin breaking

Single point analysis was completed for this operating condition as there was no significant evidence of a change in operating state during the test and therefore determining how much the whole data set varied will be more useful.

350mm – 3kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 23 to 404 as seen by the start and end cell values. These values are shown for each of the 5 parameters. Reasonable variation is evident within this test, however mostly in the rear hitch height and engine load.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	23	404	44.464	14.990
Speed			2.922	0.185
Engine Fuel Rate			11.664	4.898
Rear Hitch %			19.400	14.200
Engine RPM			1900.098	1.078

350mm – 3kph – 2

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 57 to 187 as seen by the start and end cell values. These values are shown for each of the 5 parameters. There is a large amount of variance of engine load in this test as seen in the table below, the rear hitch height is also variable throughout the test.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	57	187	50.056	53.426
Speed			2.914	0.700
Engine Fuel Rate			12.782	10.724
Rear Hitch %			23.025	35.928
Engine RPM			1899.918	4.318

350mm – 5kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 23 to 265 as seen by the start and end cell values. These values are shown for each of the 5 parameters. The main variation in this test is the engine load which is approximately 33%.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	23	265	60.634	33.413
Speed			4.812	2.018
Engine Fuel Rate			15.752	6.519
Rear Hitch %			21.538	12.120
Engine RPM			1900.087	3.113

350mm – 5kph – 2

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 20 to 89 as seen by the start and end cell values. These values are shown for each of the 5 parameters. There is a very large variation of the engine load and rear hitch height in this test, graphics of this variation can be seen in Appendix G to provide a better understanding of what is occurring.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	20	89	60.810	78.084
Speed			4.751	2.302
Engine Fuel Rate			15.794	14.613
Rear Hitch %			20.712	41.193
Engine RPM			1899.511	11.880

350mm – 5kph – half cut pin

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 23 to 99 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	23	99	60.838	57.049
Speed			4.920	0.349
Engine Fuel Rate			15.793	11.039
Rear Hitch %			20.039	28.207
Engine RPM			1900.805	7.745

300mm – 3kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 23 to 109 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	23	109	43.399	18.524
Speed			3.021	0.261
Engine Fuel Rate			11.301	4.027
Rear Hitch %			32.593	10.582
Engine RPM			1900.541	1.719

300mm – 5kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 38 to 109 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	38	109	49.695	221.929
Speed			3.796	35.178
Engine Fuel Rate			12.760	53.040
Rear Hitch %			30.025	19.681
Engine RPM			1899.616	11.894

200mm – 3kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 38 to 130 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	38	130	35.814	21.502
Speed			3.155	26.578
Engine Fuel Rate			8.970	8.182
Rear Hitch %			34.525	96.846
Engine RPM			1900.366	1.489

200mm – 5kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 8 to 101 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	8	101	40.547	54.527
Speed			4.673	8.839
Engine Fuel Rate			10.583	11.722
Rear Hitch %			37.476	15.762
Engine RPM			1900.013	3.992

4.2.2.3 Ripper digging in too far

Double point analysis using data from prior to the issue occurring as well as after was implemented for this data as there is a distinct change in operating parameters that allows when the issue occurred to be picked. This method will allow a difference in the mean and variance to be found for the data before and after the issue providing a greater understanding of whether the parameters can be used for implement awareness.

300mm – 3kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 47 to 468 for prior to the issue occurring, and then again after the issue

from 487 to 929. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	47	468	41.590	17.452	487	929	58.591	34.334	40.88	16.882
Speed			2.999	0.124			2.358	2.778	-21.36	2.654
Engine Fuel Rate			10.791	5.682			15.268	6.877	41.48	1.195
Rear Hitch %			33.025	10.023			23.512	11.720	-28.81	1.697
Engine RPM			1899.816	1.034			1900.055	0.734	0.01	0.300

300mm – 5kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 21 to 256 for prior to the issue occurring, and then again after the issue from 286 to 562. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	21	256	60.043	32.026	286	562	94.654	33.060	57.64	1.034
Speed			4.938	0.230			3.424	18.515	-30.67	18.286
Engine Fuel Rate			15.615	6.138			22.582	9.841	44.62	3.703
Rear Hitch %			31.796	8.092			22.176	23.167	-30.26	15.075
Engine RPM			1899.851	3.255			1934.151	189.468	1.81	186.212

200mm – 3kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 86 to 445 for prior to the issue occurring, and then again after the issue from 463 to 847. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	86	445	35.340	6.538	463	847	41.951	17.597	18.71	11.059
Speed			3.089	0.076			2.987	0.098	-3.30	0.021
Engine Fuel Rate			8.818	2.326			10.916	6.023	23.79	3.697
Rear Hitch %			40.614	2.531			31.581	7.727	-22.24	5.196
Engine RPM			1900.043	0.452			1900.126	0.941	0.00	0.489

200mm – 5kph

The following table shows the mean and percentage variance relative to the mean based upon the chosen operating period of 28 to 300 for prior to the issue occurring, and then again after the issue from 314 to 478. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	28	300	46.360	22.430	314	478	68.926	64.934	48.67	42.504
Speed			5.148	0.186			4.720	1.431	-8.31	1.245
Engine Fuel Rate			12.182	6.040			17.596	12.777	44.45	6.737
Rear Hitch %			39.955	2.551			27.423	7.683	-31.36	5.132
Engine RPM			1900.103	2.673			1900.558	2.154	0.02	0.520

4.2.2.4 Bridging across tines

Single point analysis was completed for this operating condition as there was no significant evidence of a change in operating state during the test and therefore determining how much the whole data set varied will be more useful.

350mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 350mm and 3kph operating conditions based upon the chosen operating period of 39 to 157 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	39	157	39.255	23.401
Speed			2.964	0.695
Engine Fuel Rate			10.044	8.204
Rear Hitch %			18.519	27.574
Engine RPM			1879.241	151.355

350mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 350mm and 5kph operating conditions based upon the chosen operating period of 61 to 167 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	61	167	48.641	96.187
Speed			4.488	12.454
Engine Fuel Rate			12.166	55.478
Rear Hitch %			18.732	22.696
Engine RPM			1763.026	2160.340

300mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 300mm and 3kph operating conditions based upon the chosen operating period of 76 to 234 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	76	234	34.928	30.772
Speed			3.053	0.834
Engine Fuel Rate			10.168	5.873
Rear Hitch %			29.732	5.131
Engine RPM			1882.112	254.598

300mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 300mm and 5kph operating conditions based upon the chosen operating period of 53 to 149 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	53	149	34.768	45.477
Speed			4.302	1.938
Engine Fuel Rate			8.381	16.375
Rear Hitch %			32.159	49.199
Engine RPM			1674.139	221.260

200mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 200mm and 3kph operating conditions based upon the chosen operating period of 23 to 181 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	23	181	33.571	19.716
Speed			3.099	0.352
Engine Fuel Rate			8.242	7.391
Rear Hitch %			39.329	168.689
Engine RPM			1900.142	1.390

200mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 200mm and 5kph operating conditions based upon the chosen operating period of 55 to 194 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	55	194	28.960	52.250
Speed			3.346	6.994
Engine Fuel Rate			6.687	25.260
Rear Hitch %			40.193	158.219
Engine RPM			1582.297	945.960

4.2.2.5 Ripper not digging in far enough

Double point analysis using data from prior to the issue occurring as well as after was implemented for this data as there is a distinct change in operating parameters that allows when the issue occurred to be picked. This method will allow a difference in the mean and variance to be found for the data before and after the issue providing a greater understanding of whether the parameters can be used for implement awareness.

350mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 350mm and 3kph operating conditions based upon the chosen operating period of 48 to 480 for prior to the issue occurring, and then again after the issue from 500 to 871. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	48	480	62.336	28.342	500	871	43.779	49.983	-29.77	21.641
Speed			2.518	2.461			2.995	0.412	18.97	2.049
Engine Fuel Rate			16.250	5.694			11.471	14.689	-29.41	8.995
Rear Hitch %			16.434	35.570			30.000	0.000	82.55	35.570
Engine RPM			1899.890	2.089			1899.856	1.404	0.00	0.685

350mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 350mm and 5kph operating conditions based upon the chosen operating period of 33 to 308 for prior to the issue occurring, and then again after the issue from 338 to 499. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	33	308	75.752	19.271	338	499	56.044	47.235	-26.02	27.965
Speed			4.427	3.511			4.976	0.222	12.39	3.289
Engine Fuel Rate			19.090	4.816			14.693	9.624	-23.03	4.807
Rear Hitch %			18.831	22.332			29.199	12.372	55.06	9.960
Engine RPM			1883.631	324.988			1900.421	3.524	0.89	321.465

300mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 300mm and 3kph operating conditions based upon the chosen operating period of 48 to 373 for prior to the issue occurring, and then again after the issue from 418 to 751. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	48	373	39.882	13.792	418	751	37.097	3.260	-6.98	10.532
Speed			3.054	0.147			3.128	0.108	2.44	0.039
Engine Fuel Rate			10.214	5.163			9.337	1.064	-8.59	4.099
Rear Hitch %			32.055	7.041			40.842	2.029	27.41	5.012
Engine RPM			1899.934	0.663			1899.957	0.227	0.00	0.437

300mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 300mm and 5kph operating conditions based upon the chosen operating period of 18 to 258 for prior to the issue occurring, and then again after the issue from 268 to 500. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	18	258	52.159	25.555	268	500	42.959	22.224	-17.64	3.331
Speed			5.032	1.818			5.190	0.162	3.15	1.656
Engine Fuel Rate			13.742	5.745			11.196	7.388	-18.53	1.643
Rear Hitch %			32.257	7.596			39.773	3.728	23.30	3.868
Engine RPM			1899.816	3.328			1899.887	2.061	0.00	1.268

4.2.2.6 Failing to lift the 3PL prior to headland execution

Single point analysis was completed for this operating condition as there was no significant evidence of a change in operating state during the test and therefore determining how much the whole data set varied will be more useful.

350mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 350mm and 3kph operating conditions based upon the chosen operating period of 1 to 205 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	1	205	43.933	17.066
Speed			2.969	0.226
Engine Fuel Rate			11.514	5.596
Rear Hitch %			23.665	8.393
Engine RPM			1900.120	1.420

350mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 350mm and 5kph operating conditions based upon the chosen operating period of 1 to 120 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	1	120	62.181	38.045
Speed			4.719	3.993
Engine Fuel Rate			16.103	7.524
Rear Hitch %			26.108	14.319
Engine RPM			1899.997	4.534

300mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 300mm and 3kph operating conditions based upon the chosen operating period of 33 to 220 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	33	220	38.268	11.406
Speed			3.052	0.163
Engine Fuel Rate			9.710	4.092
Rear Hitch %			31.832	15.023
Engine RPM			1900.107	0.582

300mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 300mm and 5kph operating conditions based upon the chosen operating period of 14 to 141 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	14	141	63.343	24.723
Speed			4.823	0.334
Engine Fuel Rate			16.358	4.643
Rear Hitch %			28.067	23.455
Engine RPM			1899.644	3.750

200mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 200mm and 3kph operating conditions based upon the chosen operating period of 1 to 250 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	1	250	33.849	7.100
Speed			3.100	0.102
Engine Fuel Rate			8.359	2.419
Rear Hitch %			39.686	6.754
Engine RPM			1900.125	0.347

200mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 200mm and 5kph operating conditions based upon the chosen operating period of 8 to 120 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	8	120	40.932	29.332
Speed			5.154	0.213
Engine Fuel Rate			10.572	10.189
Rear Hitch %			39.892	3.569
Engine RPM			1900.147	3.159

4.2.2.7 Travelling through washouts

Double point analysis using data from prior to the error as well as the complete data set was completed for these operating conditions. This is due to the change in operating state being temporary and eventually returning back to an average status.

350mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 350mm and 3kph operating conditions based upon the chosen operating period of 22 to 49 for prior to the issue occurring, and then again for the whole test from 22 to 131. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	22	49	37.251	19.459	22	131	40.237	86.142	8.02	66.683
Speed			2.952	0.256			2.943	4.573	-0.29	4.317
Engine Fuel Rate			9.441	8.214			10.296	28.444	9.06	20.230
Rear Hitch %			21.536	5.496			27.401	326.844	27.23	321.347
Engine RPM			1900.105	2.205			1899.990	6.755	-0.01	4.550

350mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 350mm and 5kph operating conditions based upon the chosen operating period of 13 to 36 for prior to the issue occurring, and then again for the whole test from 13 to 88. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	13	36	47.752	72.550	13	88	51.881	215.507	8.65	142.957
Speed			4.939	0.492			4.940	7.981	0.03	7.490
Engine Fuel Rate			12.517	19.134			13.462	52.855	7.55	33.721
Rear Hitch %			21.720	6.781			27.313	349.193	25.75	342.412
Engine RPM			1898.382	14.931			1899.216	19.079	0.04	4.148

300mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 300mm and 3kph operating conditions based upon the chosen operating period of 14 to 52 for prior to the issue occurring, and then again for the whole test from 14 to 121. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	14	52	29.324	24.982	14	121	32.073	54.664	9.38	29.683
Speed			3.041	0.472			3.057	3.657	0.52	3.185
Engine Fuel Rate			6.986	7.550			7.836	19.708	12.17	12.159
Rear Hitch %			35.501	14.440			39.200	154.484	10.42	140.044
Engine RPM			1898.985	1.959			1899.764	2.019	0.04	0.059

300mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 300mm and 5kph operating conditions based upon the chosen operating period of 15 to 38 for prior to the issue occurring, and then again for the whole test from 15 to 79. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	15	38	35.089	250.806	15	79	38.479	224.372	9.66	26.435
Speed			4.789	4.428			4.980	7.901	3.99	3.473
Engine Fuel Rate			8.663	79.188			9.638	72.444	11.26	6.743
Rear Hitch %			36.579	6.969			39.585	119.145	8.22	112.175
Engine RPM			1848.929	449.539			1881.497	204.905	1.76	244.634

200mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 200mm and 3kph operating conditions based upon the chosen operating period of 2 to 17 for prior to the issue occurring, and then again for the whole test from 2 to 79. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	2	17	28.530	12.367	2	79	32.194	47.219	12.84	34.851
Speed			2.996	0.427			3.060	5.412	2.11	4.984
Engine Fuel Rate			6.807	2.899			7.890	16.392	15.90	13.493
Rear Hitch %			44.974	1.008			48.967	135.599	8.88	134.590
Engine RPM			1899.653	1.481			1899.943	1.764	0.02	0.283

200mm – 5kph

The following table shows the mean and percentage variance relative to the mean for 200mm and 5kph operating conditions based upon the chosen operating period of 25 to 40 for prior to the issue occurring, and then again for the whole test from 25 to 78. These values are shown for each of the 5 parameters. The percentage difference between the means and variance can also be seen in the last two columns.

	Start Cell	End Cell	Mean	Variance	Start Cell	End Cell	Mean	Variance	% diff	Variance Difference
Engine % Load	25	40	35.583	172.838	25	78	37.997	257.631	6.78	84.792
Speed			4.924	1.227			5.094	7.347	3.45	6.120
Engine Fuel Rate			8.760	39.825			9.524	77.488	8.72	37.663
Rear Hitch %			40.261	1.062			45.533	125.279	13.10	124.216
Engine RPM			1895.445	13.593			1900.207	12.829	0.25	0.764

4.2.3 PTO Powered Mulcher

4.2.3.1 Virgin ground

150mm – 3kph

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 150mm depth of cut, 3kph PTO powered mulcher testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM	Rear PTO RPM
Mean	59.160	3.057	16.691	2.823	85.324	25.935	1960.048	535.458
Std Dev	9.120	0.048	2.421	0.026	0.738	4.982	11.527	9.591
3 Std Dev	27.359	0.143	7.264	0.077	2.214	14.946	34.582	28.774
Mean + 3SD	86.519	3.200	23.954	2.901	87.538	40.882	1994.630	564.233
Mean - 3SD	31.801	2.914	9.427	2.746	83.111	10.989	1925.466	506.684

150mm – 3kph – 2

The following table shows the values for the mean and $\pm 3SD$ from the mean for each parameter that are used as a baseline for all of the 150mm depth of cut, 3kph PTO powered mulcher testing data.

	Engine Load	Speed	Engine Fuel Rate	Wheel Based Speed	Coolant temp	Rear hitch %	Engine RPM	Rear PTO RPM
Mean	57.894	3.175	16.326	2.955	88.065	26.062	1959.202	529.576
Std Dev	8.744	0.064	2.268	0.030	1.830	7.138	14.701	56.552
3 Std Dev	26.231	0.192	6.805	0.089	5.490	21.414	44.103	169.655
Mean + 3SD	84.125	3.366	23.131	3.043	93.556	47.476	2003.304	699.231
Mean - 3SD	31.663	2.983	9.522	2.866	82.575	4.648	1915.099	359.920

4.2.3.2 Ripped ground

Single point analysis was completed for these operating conditions as there was no change in operating state during the test and therefore the data needs to be compared back to the baseline data.

150mm – 3kph

The following table shows the mean and percentage variance relative to the mean for 150mm and 3kph operating conditions based upon the chosen operating period of 66 to 750 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	66	750	49.959	32.504
Speed			3.193	0.061
Engine Fuel Rate			14.395	7.396
Rear Hitch %			27.090	5.090
Engine RPM			1960.292	2.394

150mm – 3kph – 2

The following table shows the mean and percentage variance relative to the mean for 150mm and 3kph operating conditions based upon the chosen operating period of 43 to 798 as seen by the start and end cell values. These values are shown for each of the 5 parameters.

	Start Cell	End Cell	Mean	Variance %
Engine % Load	43	798	51.426	45.832
Speed			3.178	0.067
Engine Fuel Rate			14.739	10.708
Rear Hitch %			26.475	5.527
Engine RPM			1959.997	3.528

4.3 Overall Results

All of the results tables were combined together, and a rank was applied to every parameter of every test with 1 being the largest difference in both mean and variance and 5 being the smallest. The sum of all ranks for each parameter was then found as seen in the table below. From the table it can be deduced that the engine % load is the best indicator of an implement issue with the rear hitch height being the next closest indicator. Both engine RPM and engine fuel rate were tied for third most suitable parameter. The speed is clearly not a good indicator of an issue as the tractor is already capable of changing gears and engine RPM to ensure the set speed is maintained at all times.

	Mean	Variance		
Engine % Load	87	68	1	1
Speed	170	161	5	5
Engine Fuel Rate	117	114	4	3
Rear Hitch %	88	82	2	2
Engine RPM	93	135	3	4

Given the majority of testing involved the 3PL, it is probably not a fair assumption to say it is a good indicating parameter for the wide variety of operations that a general tractor would undertake.

Chapter 5 Discussion

5.1 Chapter Overview

This chapter summarises and discusses the work completed within the project and its implications on the outcomes of the project and possible future developmental work.

This work will hopefully be able to be further developed along with industry inputs to reach a state where major agricultural machinery companies see the possibilities of the technology that already exists on their machines.

The testing procedure that was developed to simulate operational field issues, the results found from the testing procedure, as well as some recommendations as to the use of CAN Bus based perception systems in autonomous tractors will be discussed to satisfy the project objectives.

5.2 Achievement of Project Objectives

This research project was completed based around the aim of fulfilling pre-defined project objectives as seen in Chapter 1.3. Keeping these objectives as the main priority of the project allows the specific research question to be answered.

5.2.1 Objective 1 - Develop a test procedure to assess machine perception

The first objective of the research project was to develop a test procedure to simulate various field operational issues that would allow machine perception to be assessed.

Within the literature review, previous physical tractor testing methods were analysed such as the Nebraska Tractor Test developed by the Nebraska Tractor Test Laboratory at the University of Nebraska. While this test does not cover the same exact tests that are required for this project, it provides an appropriate base to develop a testing procedure that can be repeated in a consistent manner. This research project is also a development of the work completed by Torrance (2020) who developed a comparative test procedure for the assessment of autonomous tractor performance. He found that the John Deere 6120R tractor was lacking perception functionality and therefore could not be classified as an autonomous tractor. The work completed by Torrance (2020) also provides an understanding of how to set out a testing procedure which can be built upon for this project.

Through Chapter 2 (Literature Review) in particular Chapter 2.6, investigation was undertaken to determine what simple agricultural implements could be analysed and what issues may occur with these implements. The issues were decided on based upon personal experience and issues that an operator would sense. The purpose of this technology is to take the place of the operator due to its ability to detect issues that are currently sensed by the driver through either sight, sound or feeling. As a result, two basic farming operations, transporting and 3PL deep ripping were chosen as basic implements that do not contain an inbuilt sensor system. Proof of concept testing was also undertaken with a PTO powered mulcher to see if PTO powered machinery could also be monitored with the tractor's inbuilt sensors. Within each operation or implement, a range of operating states have been devised based around sensible and safe operating speeds and depths. Considering the machinery available to carry out the testing was also an essential part in deciding what implements to use. The John Deere 6120R tractor as well as 3PL deep ripper and PTO powered mulcher were borrowed from the University of Southern Queensland. The university also supplied the land on which the data collection process could be undertaken which made the whole process more streamlined.

Some issues that were identified that can occur with a 3PL ripper include the ripper shank shear pin breaking, the ripper digging in too far as a result of change in implement height or ground

conditions, bridging across two or more tines creating a bulldozing effect, the ripper not digging in far enough due to hard pans in the soil, failing to lift the 3PL prior to executing the headland manoeuvre and travelling through washouts resulting in a change of the operating depth of the implement. For no implement, a transporting mode of failure was investigated to determine if there is any sense of operation status from the tractor's sensors.

Each mode of failure had a test designed that would replicate the issue in a realistic manor. It is also essential that the testing method is safe and will not cause any harm or damage to the operator or machinery. The tests also had to be repeatable so that the methodology could be utilised on many different tractors and operating conditions. To carry out this data collection for other tractors, it would be important to run the baseline data tests again to allow all of the data to be referenced off a consistent data set.

From this, the testing procedure was designed to be safe, repeatable and replicatory of the real-world modes of failure. The testing procedure can be found in Chapter 3 (Methodology) specifically section 3.3.2.

Overall, the testing method developed provides a broad range of operating states and modes of failure that allow an investigation into whether the sensors that are on the tractor already can be utilised for implement perception.

After completing the data collection, it was obvious that there were a few improvements that could be made to the testing procedure. The bridging test was rather uncontrollable as the board on the ground would often not perch in its required spot to drag the soil along. Improvements could be made to this testing method to make it more repeatable and consistent. Attempting to collect all similar or related data on the same day would also be beneficial as there are multiple environmental changes that will affect how the tractor operates such as soil moisture and ambient temperature.

5.2.2 Objective 2 - Assess the utility and sensitivity of CAN Bus information

The second major objective of the research project was to assess the utility and sensitivity of information exchanged on the tractors CAN Bus for machine perception purposes.

To analyse the information exchanged on the CAN Bus, it is important to understand how the CAN Bus system of modern agricultural machinery works so that data can be collected from various sensors that are already installed on the tractor. It was determined in the methodology chapter (Chapter 3.4.4 and 3.4.5) that using a CANcaseXL and Can Sniff software was the best method of recording CAN Bus data off the John Deere tractor.

After recording the data using the software and hardware provided by John Deere, the data was sent to John Deere in the United States of America for conversion into a useable format. The data was sent back in Matlab format after which specific chosen parameters were exported into Excel for easier graphing and analysis.

The data in Excel was further refined and parameters that did not show any change in operating state were removed. Eventually, seven key parameters were decided upon; engine fuel rate (lph), speed (km/h), wheel-based speed (km/h), engine coolant temperature (degC), rear hitch height (%), engine load (%) and engine speed (RPM). These seven parameters were graphed against the mean and $\pm 3SD$ values from the base runs for each speed and operating depth. The mean and variance of each data set was also calculated to allow further refinement of the data to approach a finite answer as to which parameter is the best indicator of a possible issue occurring with the implement. After a ranking process based on the mean and variance values, it can be concluded that the engine % load is the best indicator that an issue has occurred. The second-best parameter is the rear hitch height, however this could be considered a false reading as the majority of tests undertaken revolved around the 3 point linkage and therefore the data may not be representative of drawbar or PTO powered implements. Further testing with these implements would need to be undertaken to ensure correct results. The third best parameter is a tie between engine fuel rate and engine RPM. Based on visual inspection of the graphs, either of these parameters could be suitable.

	Rank
Engine % Load	1
Rear Hitch %	2
Engine Fuel Rate	3
Engine RPM	3
Speed	4

The sensitivity of the chosen parameters is one of the most important parts of determining the feasibility of using the tractors existing sensors to examine the operating status of the implement. While the sensors are evidently sensitive enough to detect some change, the efficiency of their issue detection is left to be questioned. It can be concluded that the sensors are suitable for the job in terms of detecting a change in operating state, however their effectiveness in a system designed to detect operational issues with the implement may be underwhelming.

Further investigation through a wider range of tests and more detailed testing would be required to determine if the sensors are suitable for implement status awareness.

5.2.3 Objective 3 - Recommendations for CAN Bus based perception systems

The third objective for the research project was to develop recommendations for CAN Bus based perception systems that will inform autonomous operations.

After undergoing the data collection process and seeing the data that was obtained from the testing, conclusions can be drawn as to the effectiveness of CAN Bus based implement perception systems. Working through the data analysis and refinement of parameters to find the best suited for the process has shown that there is a large amount of variability within the data. This variability can be attributed to changing field conditions as well as slightly different operating conditions between runs. Changing field conditions is an issue that's always going to exist given the system would ideally use machine learning to understand that an issue has occurred and is resulting in the machine operating outside its standard operating zone. This standard operating zone is going to change across the field with differing soil characteristics and therefore the system would have to be able to adjust so that the chances of detecting an issue are still suitable.

Based on the information gathered within this research project, it can be determined that CAN Bus based perception systems would be suitable for informing autonomous operations, however, in

their current state the system would not operate efficiently. Further research needs to be completed to determine how to reduce the noise in the recording system to further increase the control of the system. The majority of the sensors that already are on the tractor are not sensitive enough to detect many of the minor issues that were tested in the data collection. Overall, the system has potential, however, a large amount of work still remains to refine the process to allow smooth consistent data for implement awareness.

5.3 Limitations

The main limitations for this research project were the time available and the data analysis stages.

The project was scaled to suit the available time given the short project timeframe. With more time, the project could be further developed to look at more implements and modes of failure that may occur in the field. While only simple implements were available for this research project, there are a large variety of implements that would benefit from this technology. Testing a range of implements and modes of failure will allow better conclusions to be drawn regarding the ability of the tractors in-built sensors to provide awareness of the operating state of the implement.

The data analysis was undertaken in a basic fashion, however, could be greatly improved by using more statistical methods. The large volume of data also made the analysis process difficult as graphs become crowded, or the number of graphs become too many. Developing an automated process of data analysis is something that would be beneficial if expanding the work into other implements and modes of failure.

The effect of environmental conditions on the results could not be tested due to the limited timeframe of the project. The majority of the data collection was undertaken in July/August and therefore a range of soil moistures and ground conditions couldn't be analysed. Changing these field conditions may have an effect on the accuracy and outcomes of the data and so would be worthwhile testing in future.

Chapter 6 Conclusion

6.1 Chapter Overview

This chapter encapsulates the key findings of the research project as well as presents recommendations based on the results from testing and analysis. Conclusions are made from all portions of the project and recommendations towards further work and the suitability of the tractors sensors for implement awareness.

6.2 Key Findings

The conclusions and key findings that were drawn from this project are summarised below:

- The testing procedure developed for data collection was suitable, however could have been expanded if more time was available. Expanding the testing variable would allow a more accurate response regarding the suitability of CAN Bus based perception systems for autonomous tractors.
- CAN Bus based systems are efficient and allow for easy access to sensor data, however the sensitivity and suitability of each sensor for issue detection is not up to the standard that would be required for implement perception.
- The sensor data is very noisy and therefore determining when an issue has occurred can be very challenging. It would be recommended that data from multiple sensors would be combined together to allow the case to be confirmed prior to setting off an alarm or assuming something has gone wrong.
- Further work and development should be implemented to further analyse the sensors available on the tractor as there is potential in the system, it just needs to be further refined to make it useful.

- Overall, CAN Bus based perception systems are the way of the future as it is efficient and simple to setup when a large number of sensors are installed on a machine such as an autonomous tractor.
- There may be aftermarket sensors that could be retrofitted to the tractor to provide a better understanding of what the implement's operating status is.

6.3 Further Work and Recommendations

After completing this project, the following points are proposed:

- Further develop the testing method and expand the quantity of tests to provide a better understanding of what the sensors are reading when the failures are occurring.
- Develop an analysis software package for the data to reduce the time that is required to receive a result due to the large volume of data that needs to be processed.
- Complete the testing procedure in a variety of soil types and environmental conditions to attempt to gain more of a real world understanding of how the sensors will react to an issue occurring.
- Explore other sensors that could be installed on the tractor to provide a better understanding of the implements operating status.
- Conduct further testing using drawbar and PTO powered implements to understand the suitability of this methodology on a wider range of tractor implement combinations.

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Appendices

Appendix A – Project Specification

ENG4111/ENG4112 Research Report

Project Specification

For:	Sam Green
Title:	Investigation into implement status awareness for autonomous tractors
Major:	Agriculture
Supervisors:	Justine Baillie Craig Baillie
Enrolment:	ENG4111 – ONC S1, 2022 ENG4112 – ONC S2, 2022
Project Aim:	The aim of this research is to determine if sensory information that is already on a tractors CAN Bus system can provide a sense of machine and implement perception for autonomous applications. Analysis of the collected data from the designed testing procedure will allow conclusions to be drawn about the ability of the tractors sensors to determine the state of operation of the implement.
Program:	Version 1, 22nd February 2022

1. Development of literature – investigate existing information regarding collecting CAN Bus data and utilising it to monitor a vehicles operating state. Also look into current testing procedures that could be modified to suit the data to be collected. Identify any gaps or works that can be built upon for this research project.

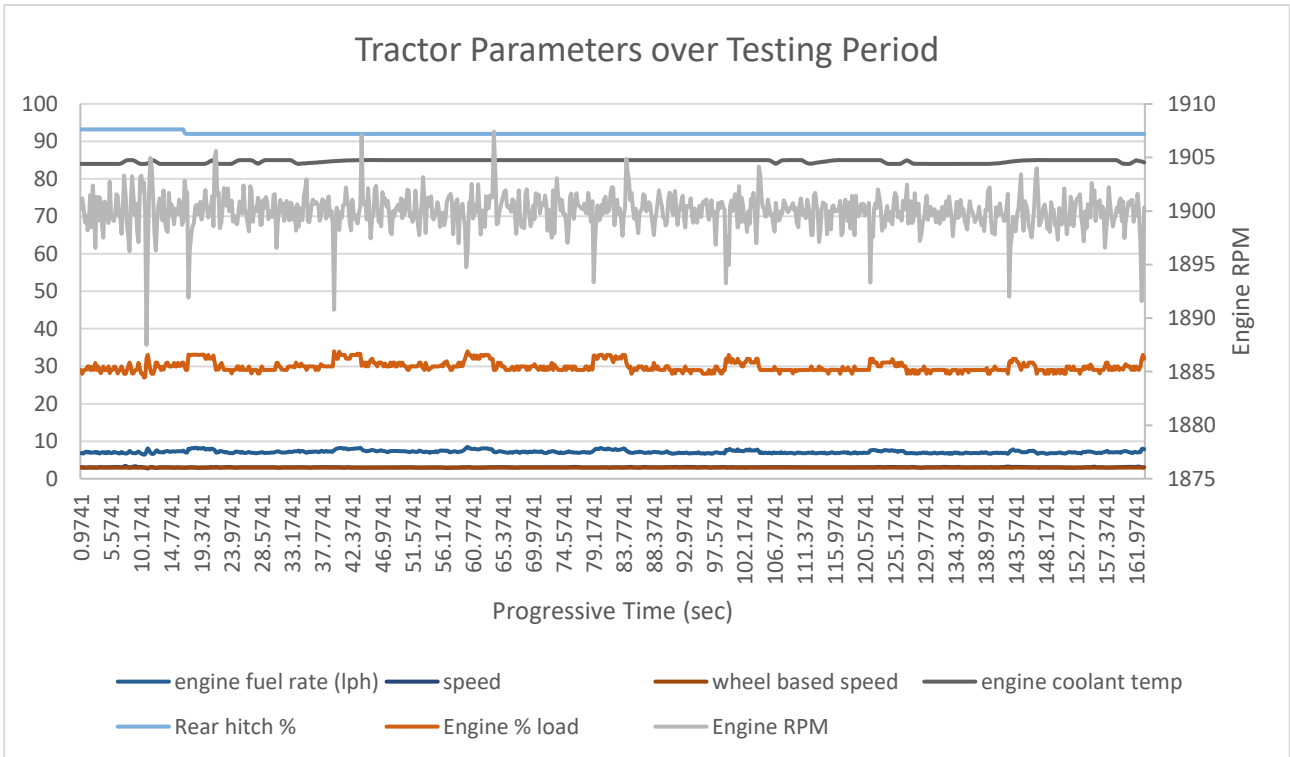
2. Conduct investigation into the process of data collection from the CAN Bus system of autonomous John Deere tractors.
3. Investigate which data may be useful in determining whether an issue may have occurred with the implement.
4. Secure machinery and site to allow testing to be undertaken safely and when required.
5. Complete the UniSQ WH&S forms to ensure machinery can be operated in a safe manor.
6. Develop an experimental procedure to simulate issues occurring on basic tractor implements that do not have their own sensor systems.
7. Conduct preliminary testing to verify that the data can be collected and the testing procedure will be suitable, then if necessary modify the testing procedure to ensure the correct data is collected.
8. Perform experiment procedure to capture data.
9. Process and evaluate the data collected in the experiments.
10. Present the findings of the experimental procedure and develop recommendations towards CAN Bus based perception systems in autonomous tractors.

Appendix B – Data collection testing matrix

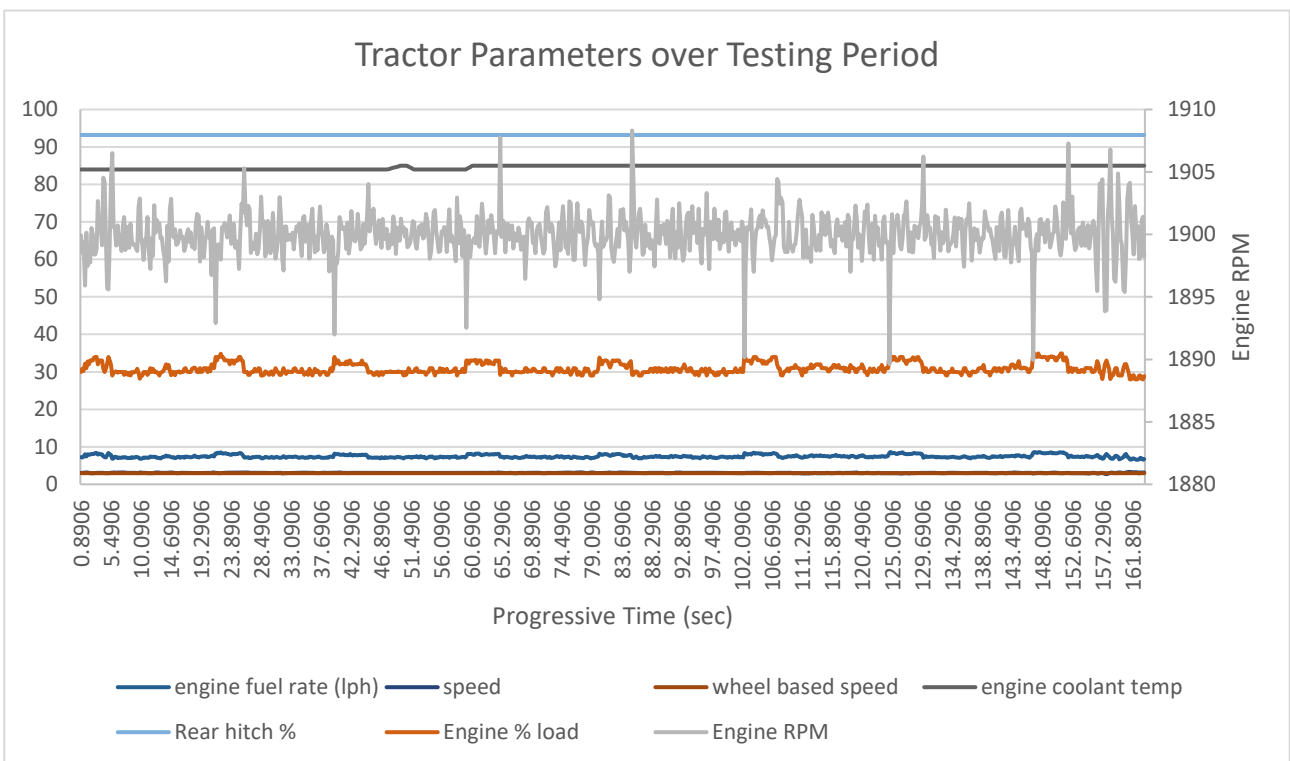
	3 km/h			5 km/h			10 km/h						
	40%	30%	20%	40%	30%	20%	40%	30%	20%				
No Implement	Operating Depth	N/A	200mm	300mm	350mm	N/A	200mm	300mm	350mm	N/A	200mm	300mm	350mm
	Base run on virgin ground												
	Transporting												
	Base run												
	Ripper shank breaking off												
	Ripper digging in too far												
3 Point Linkage Deep Ripper	Bridging occurred across tines												
	Ripper is not digging in far enough												
	Failing to lift implement prior to headland												
	Failing to change 3PL height when going through a washout												
PTO Powered Mulcher	150mm												
	Base run - virgin ground												
Operating in pre-ripped ground													

Appendix D – No Implement – Base Run Data

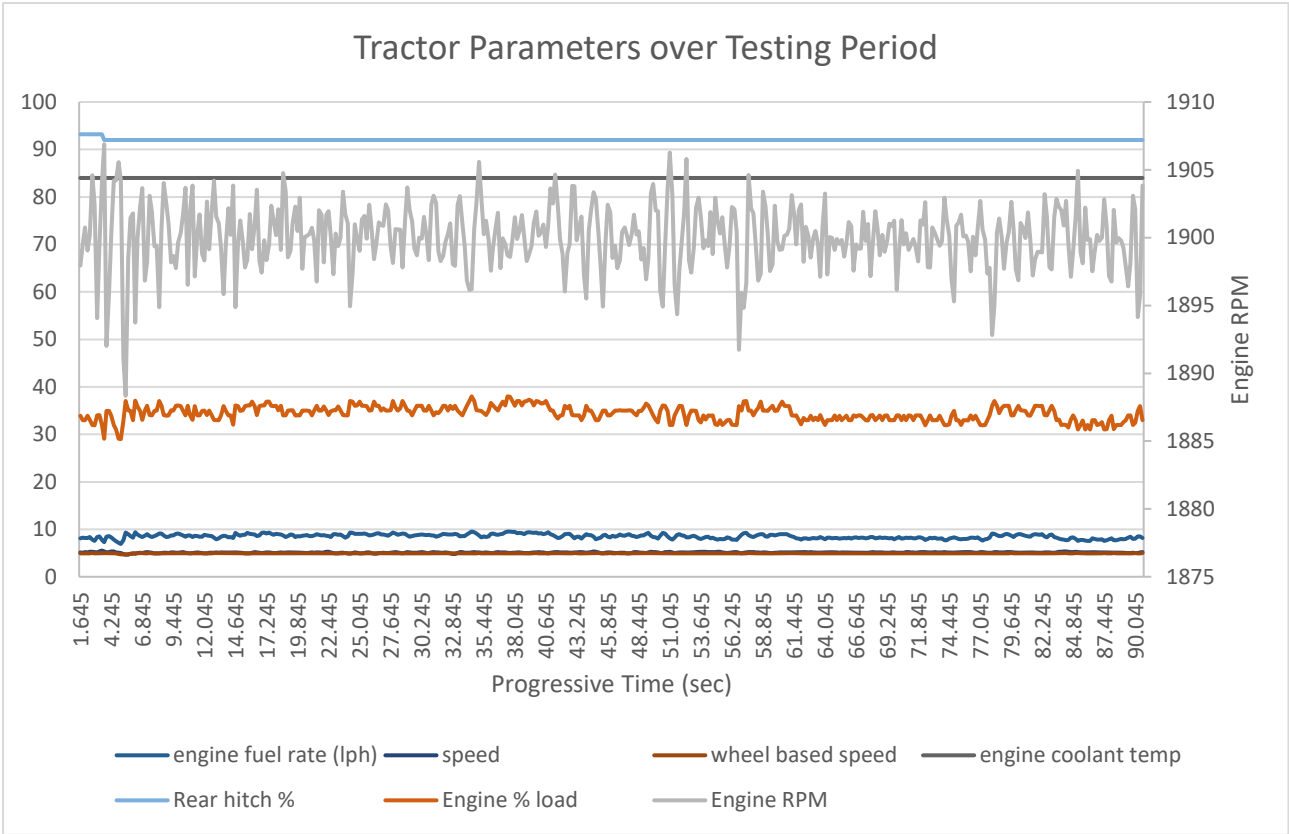
3kph



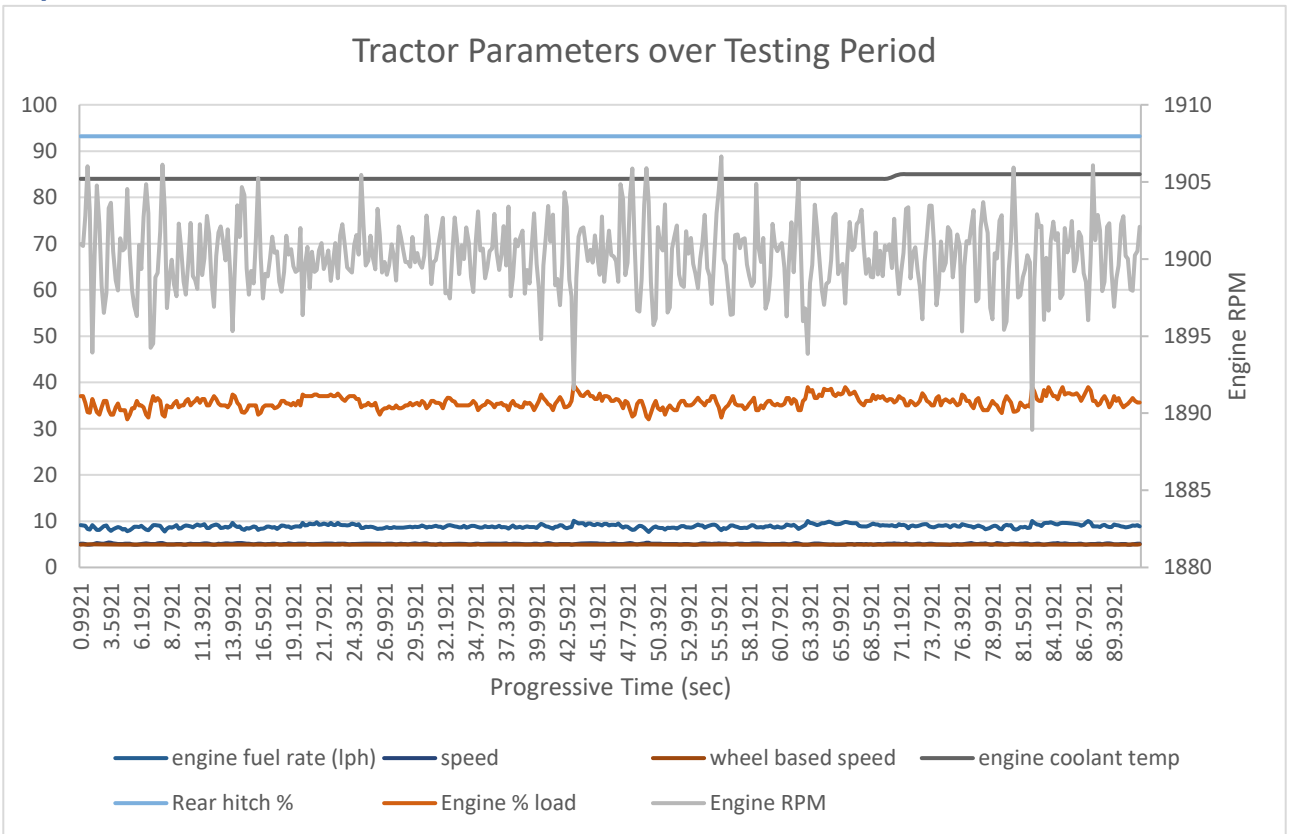
3kph – 2



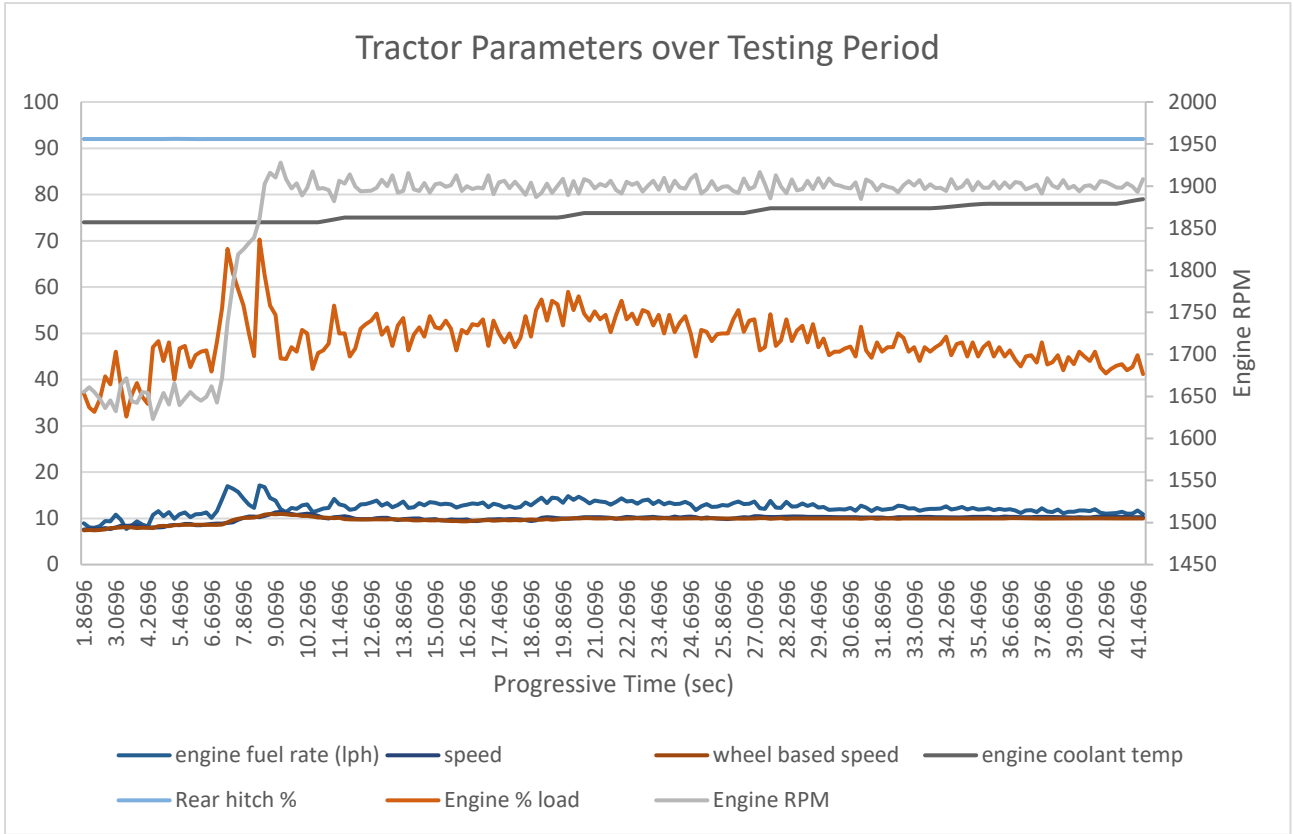
5kph



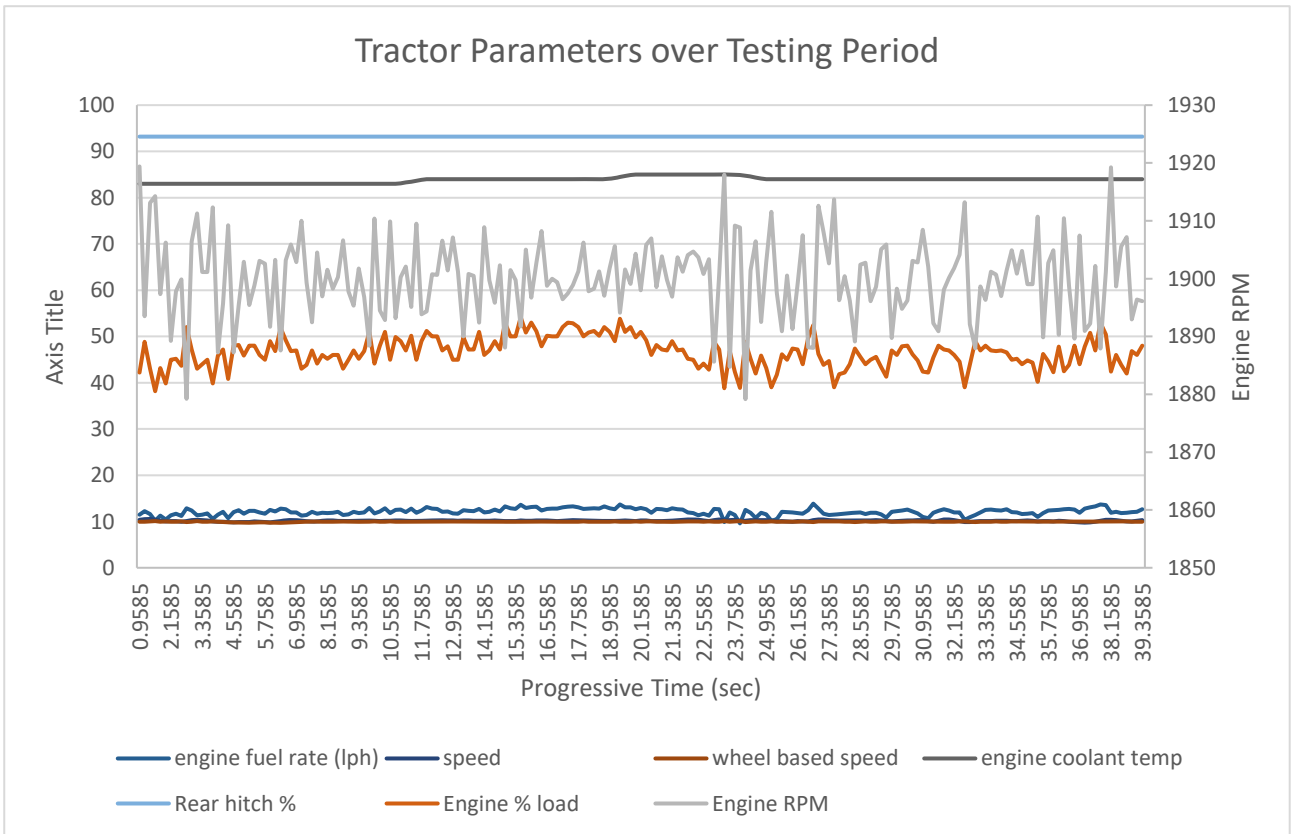
5kph - 2



10kph

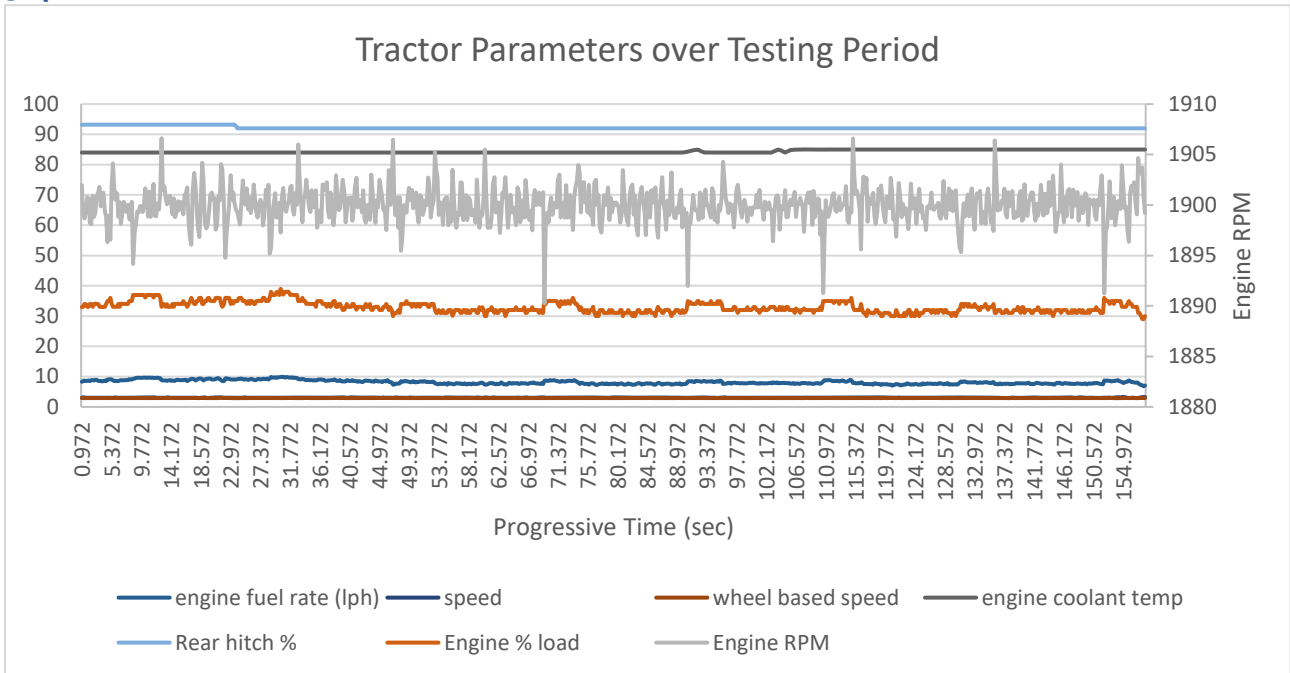


10kph - 2

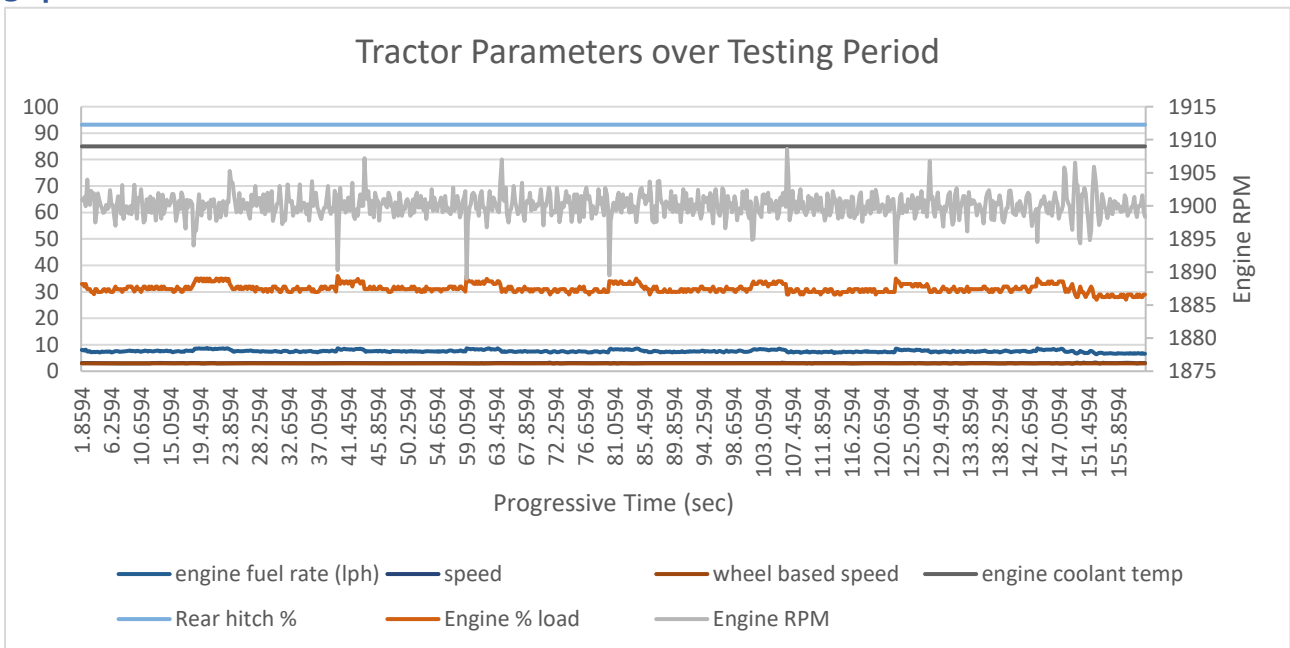


Appendix E – No Implement – Transporting data

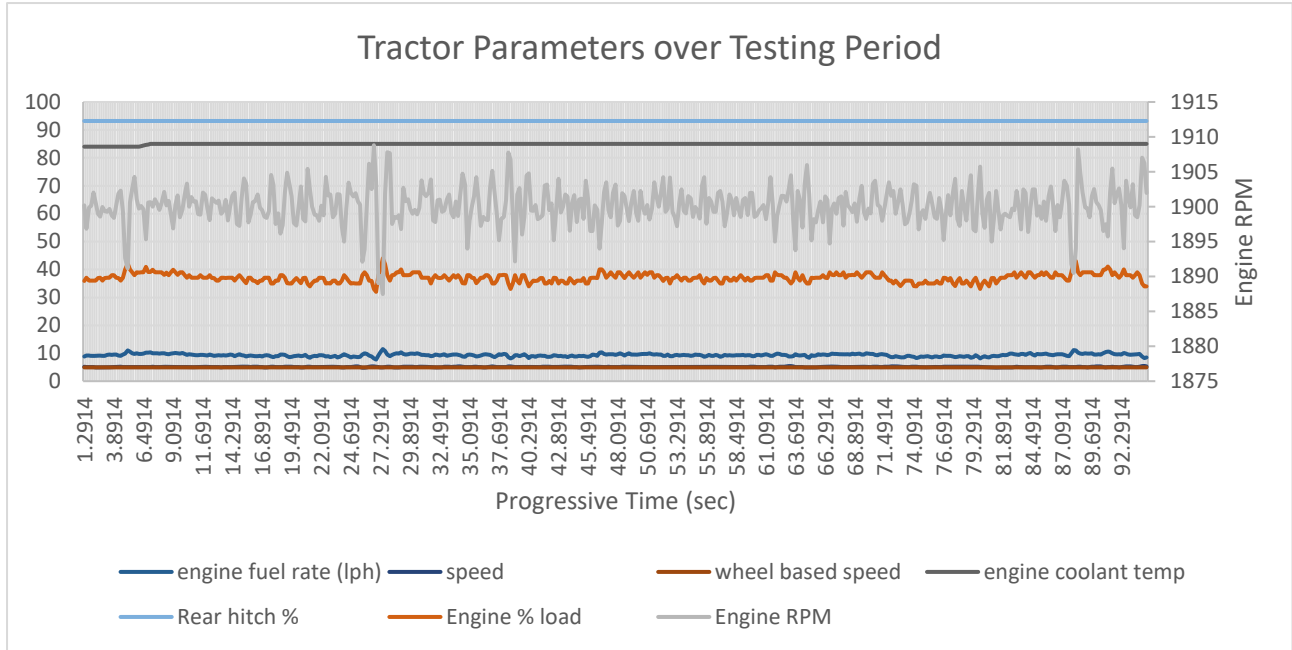
3kph



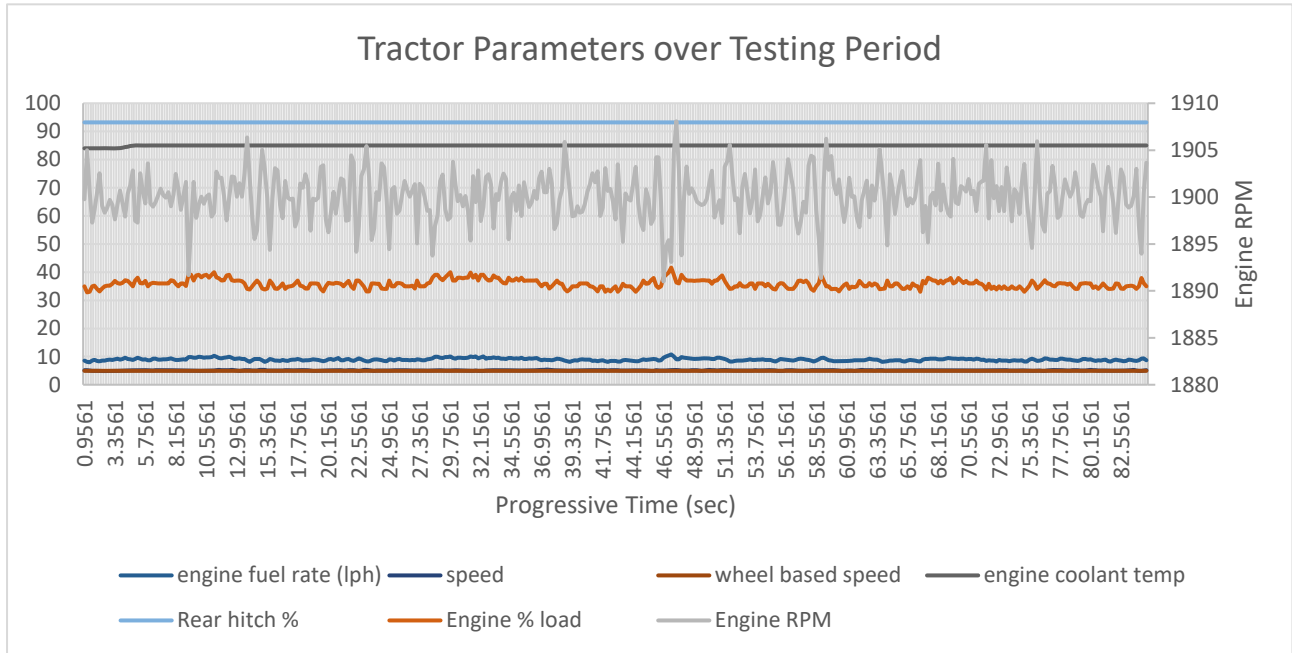
3kph – 2



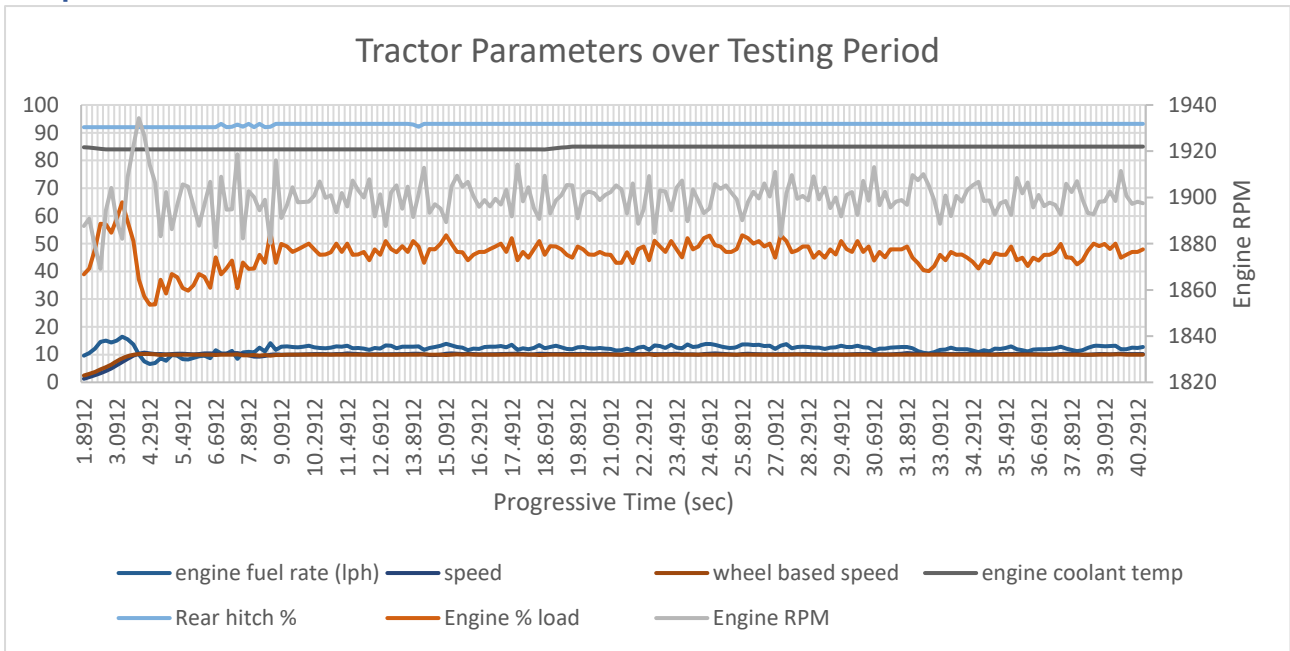
5kph



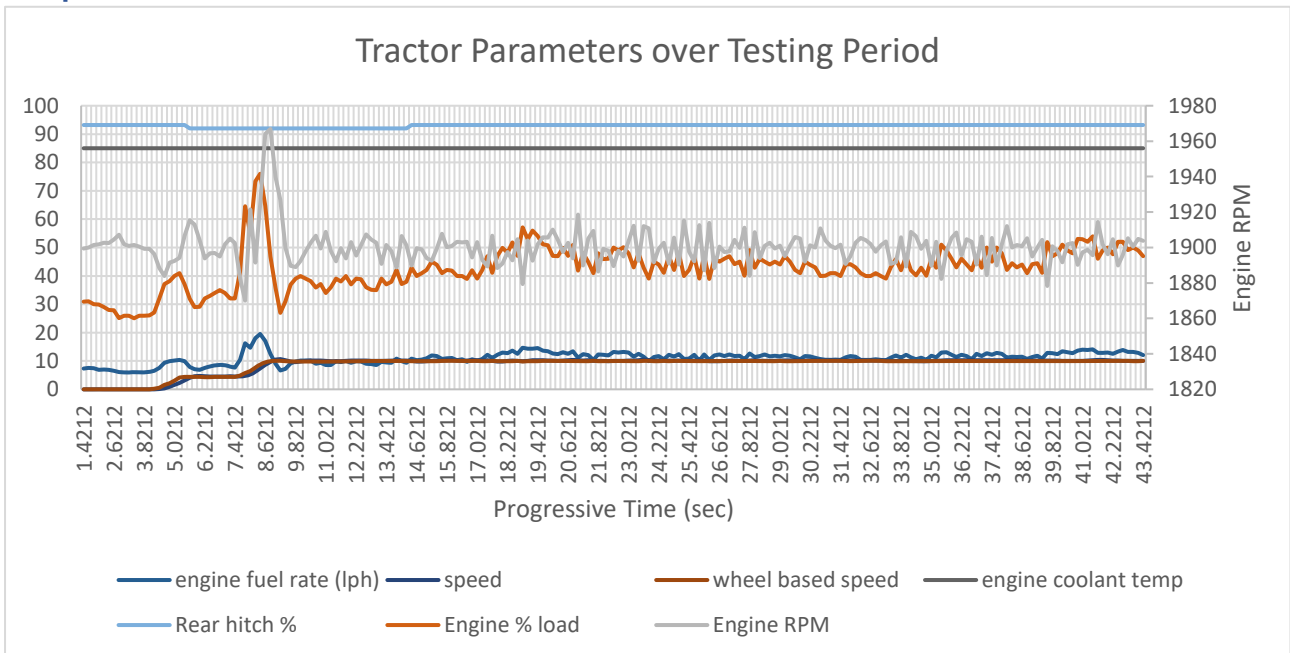
5kph - 2

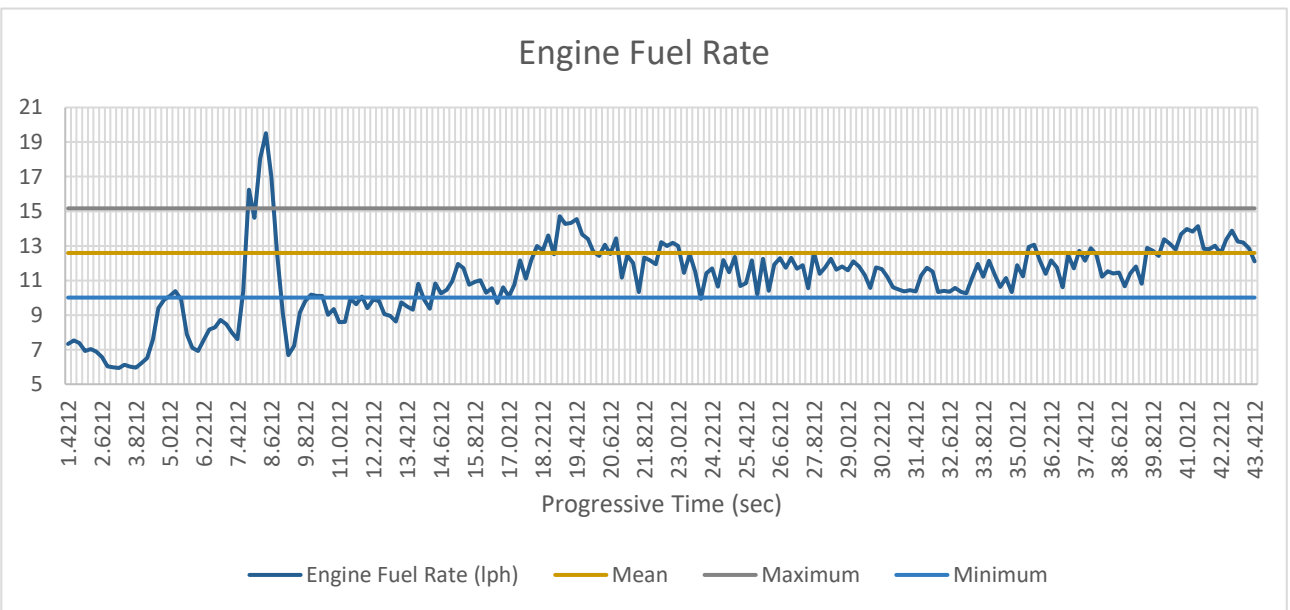
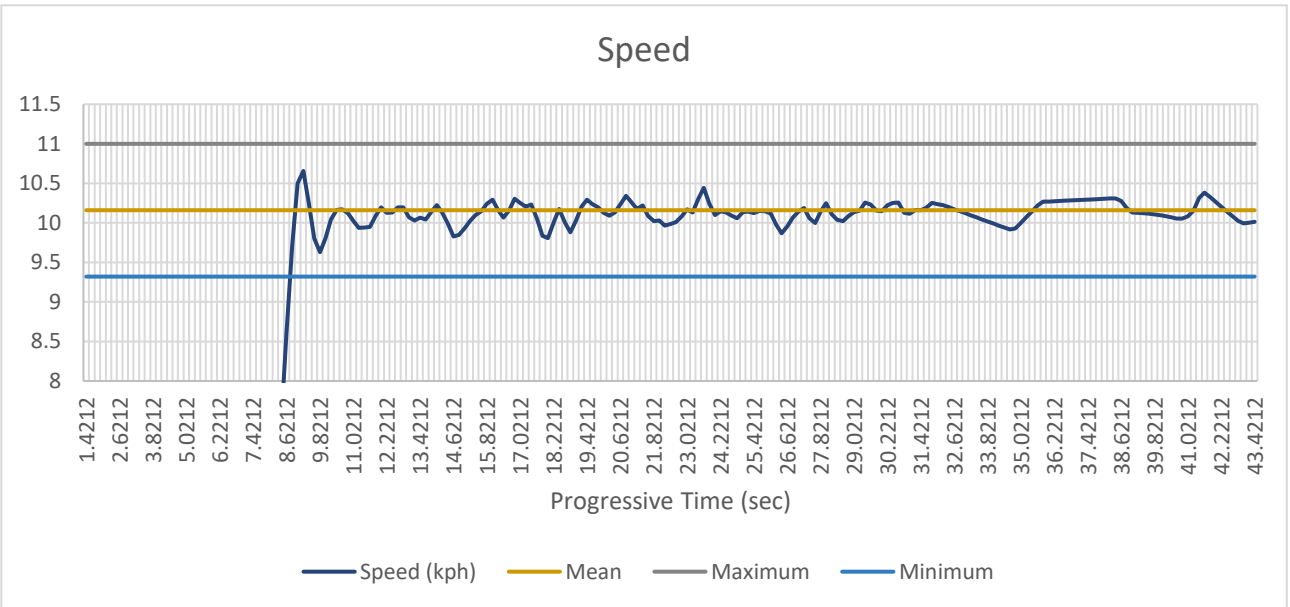
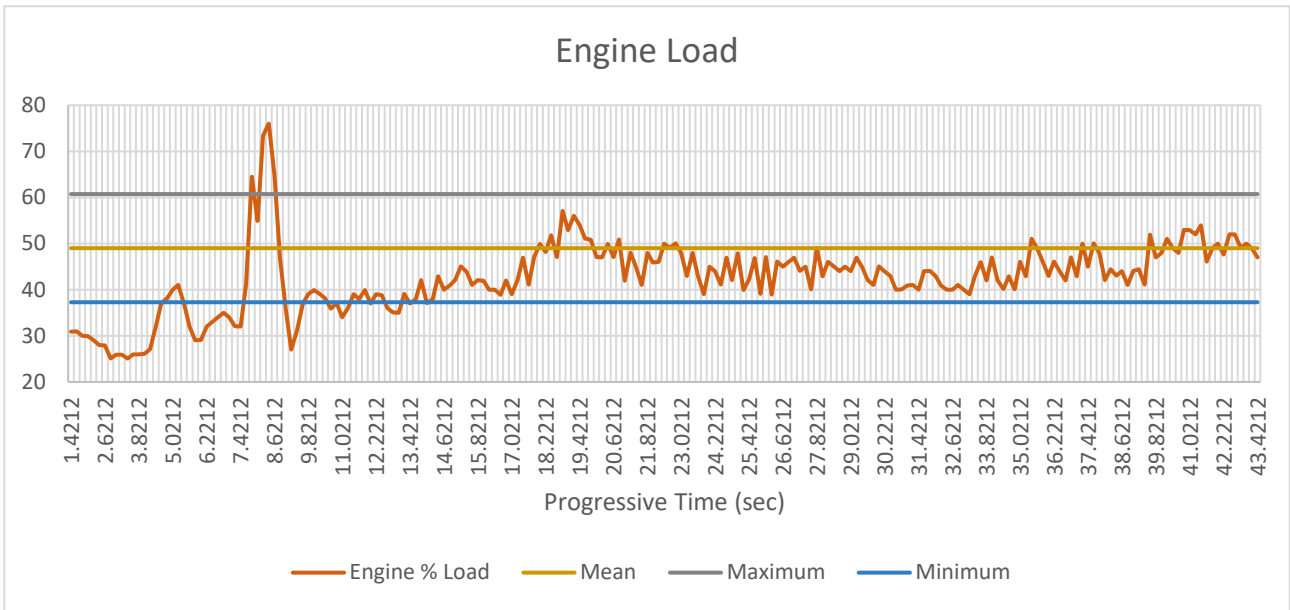


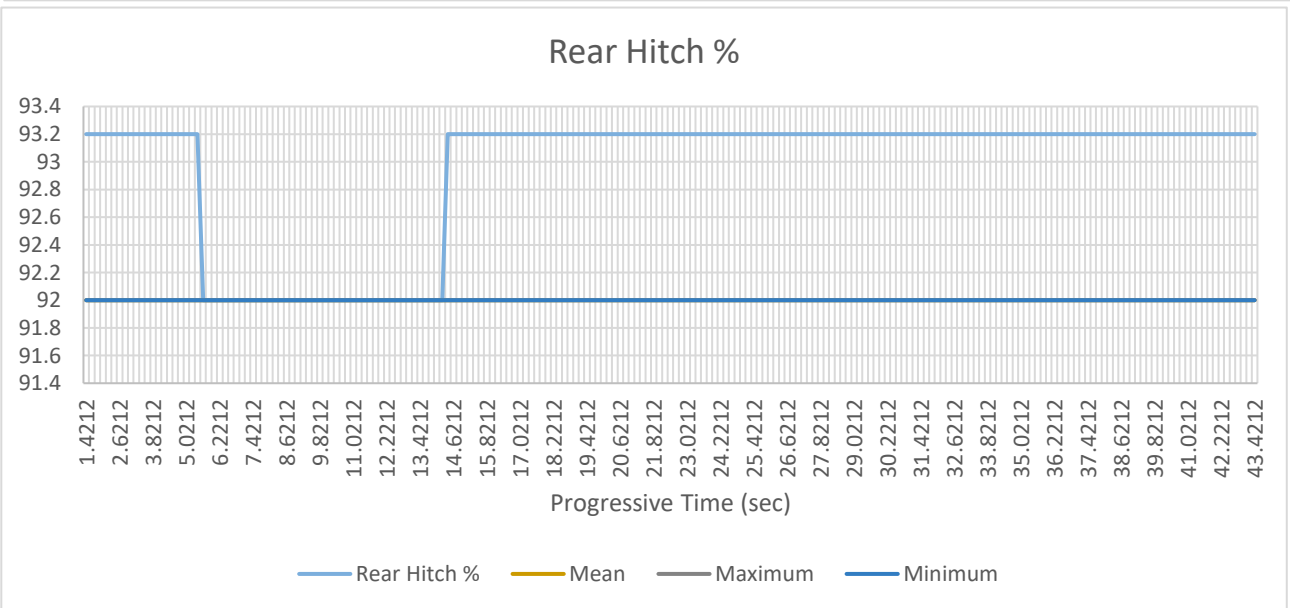
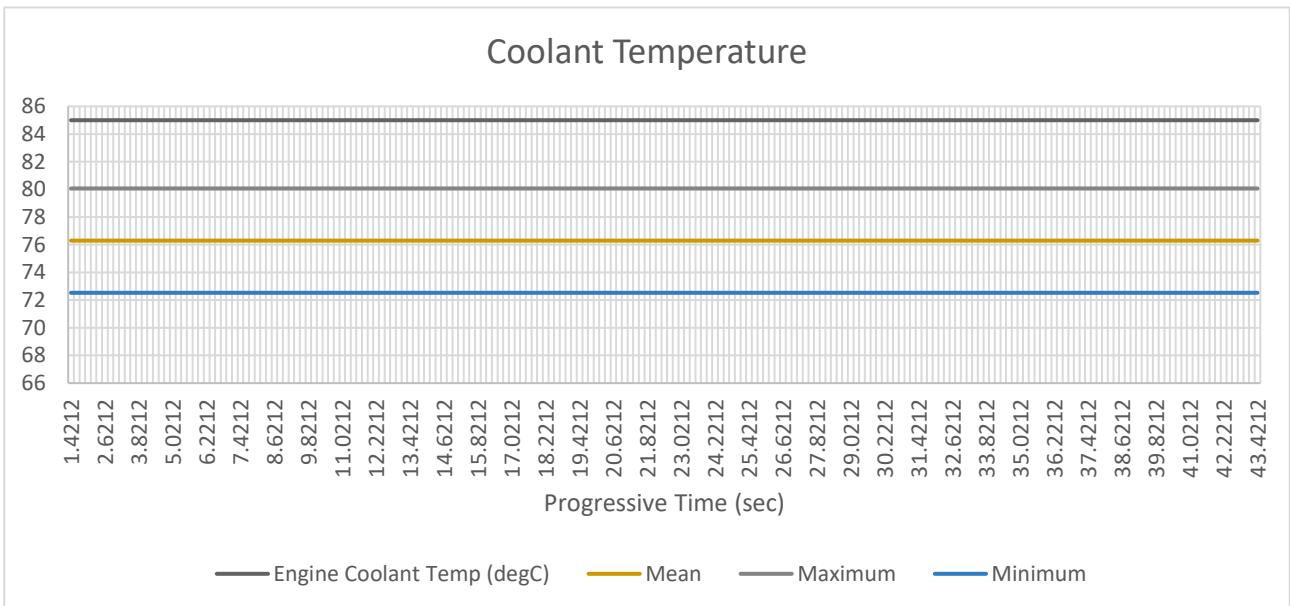
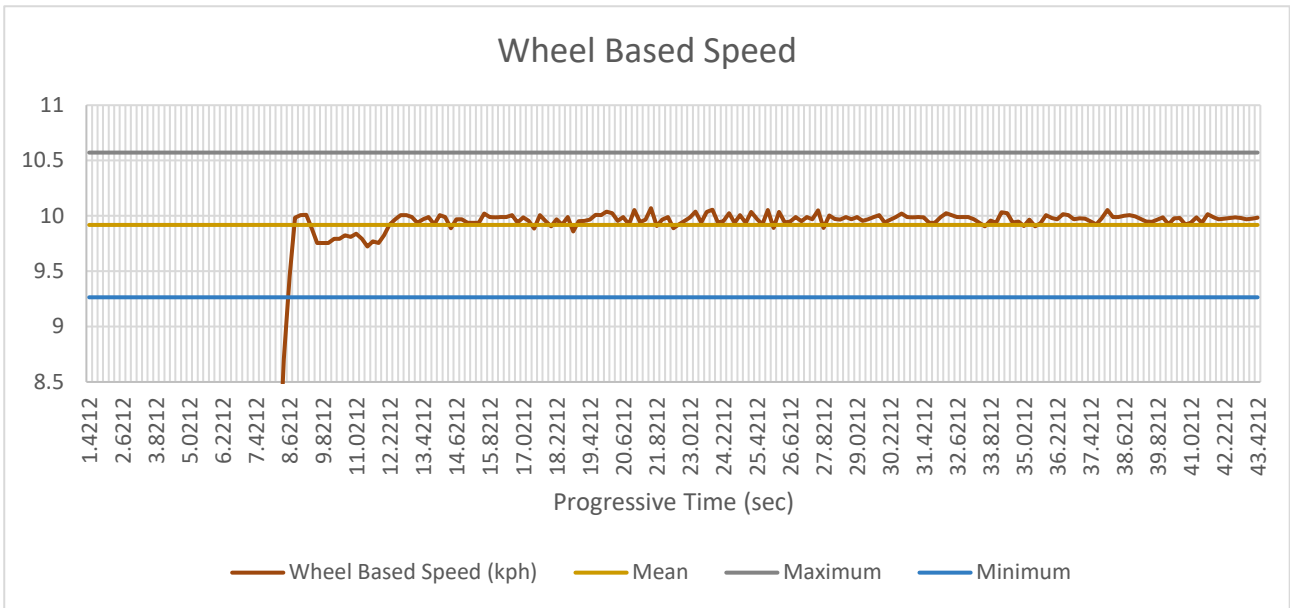
10kph



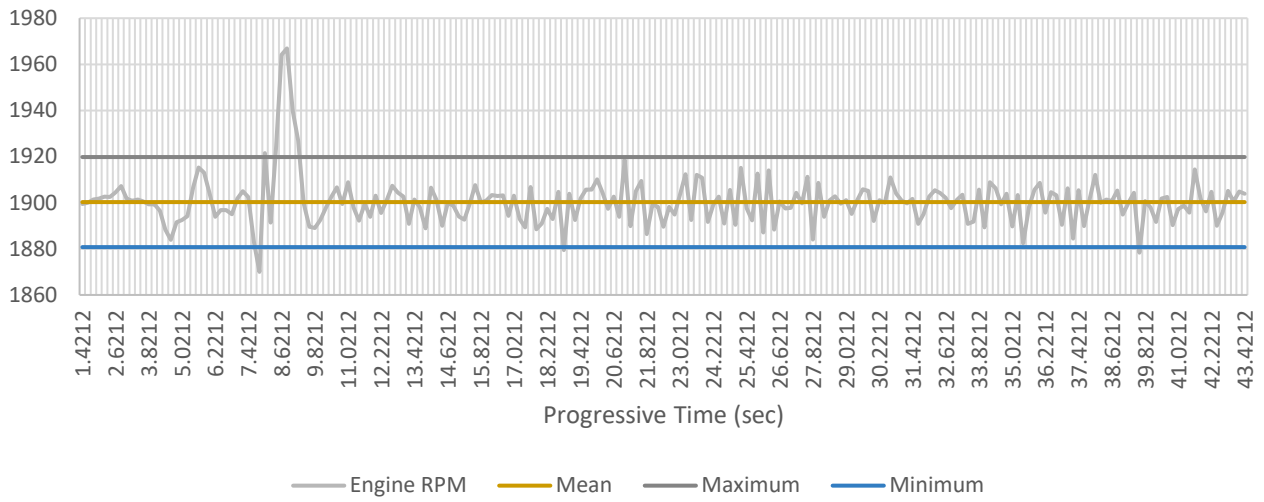
10kph - 2





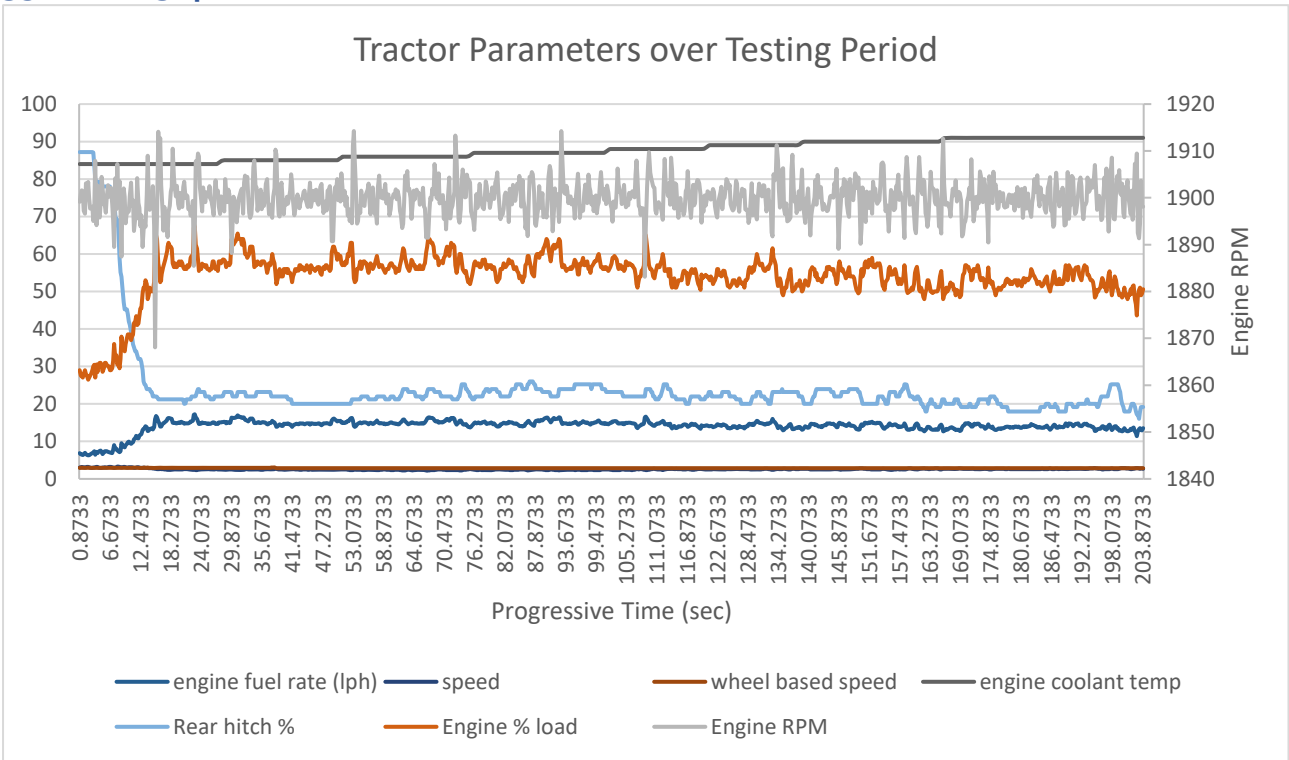


Engine RPM

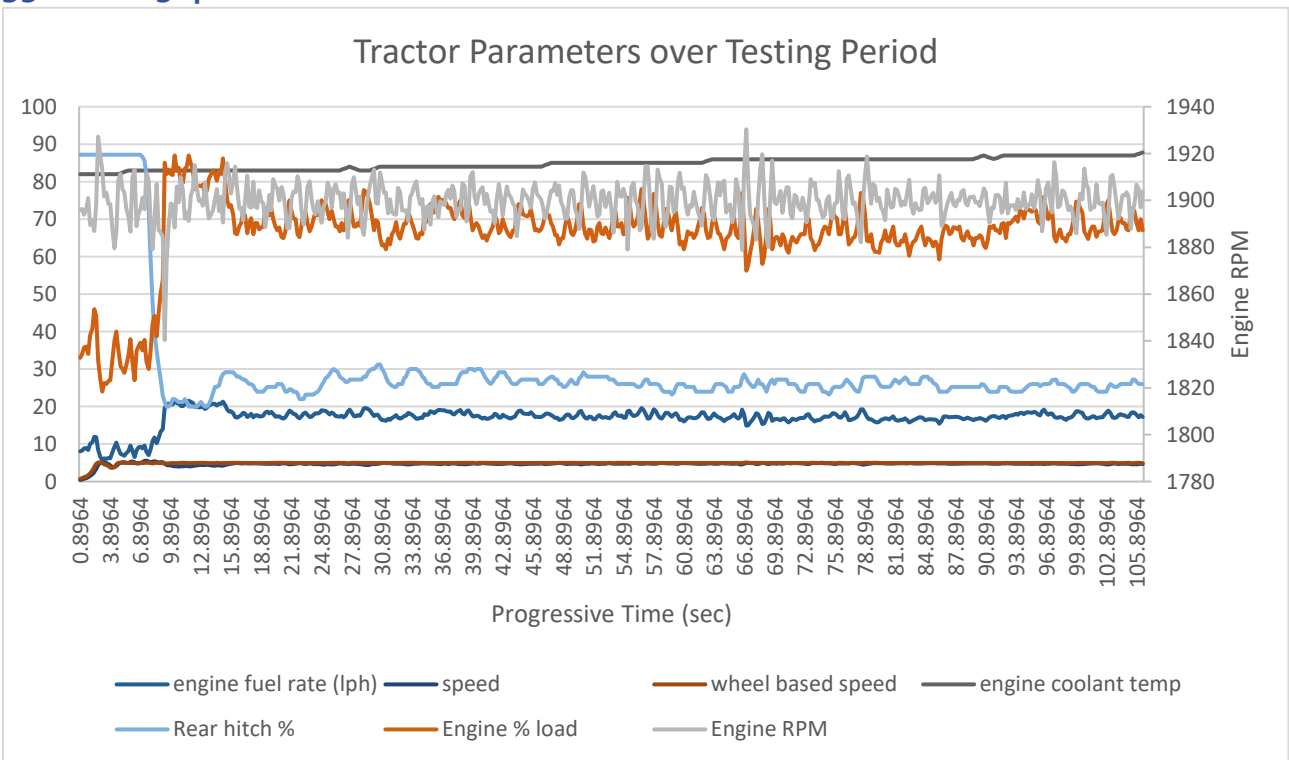


Appendix F – 3PL Deep Ripper – Base run data

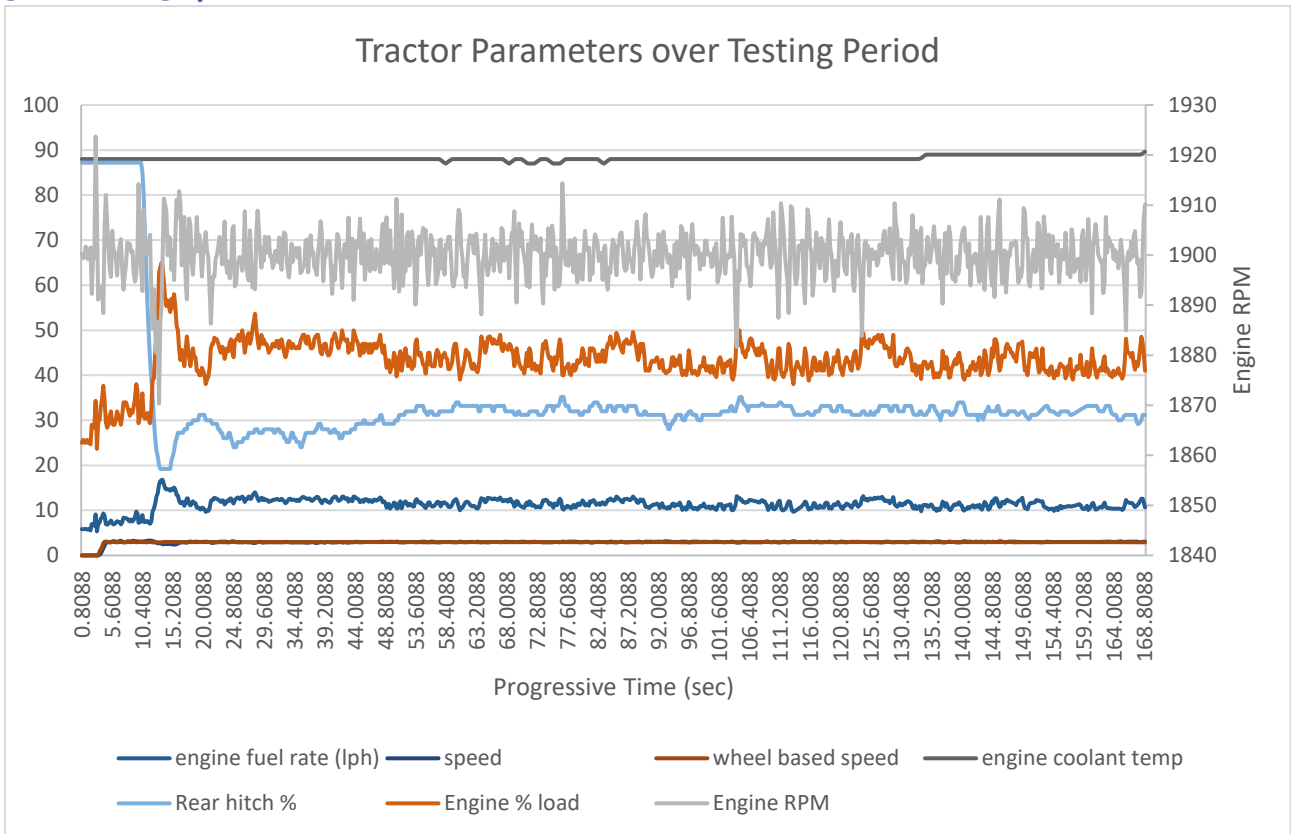
350mm – 3kph



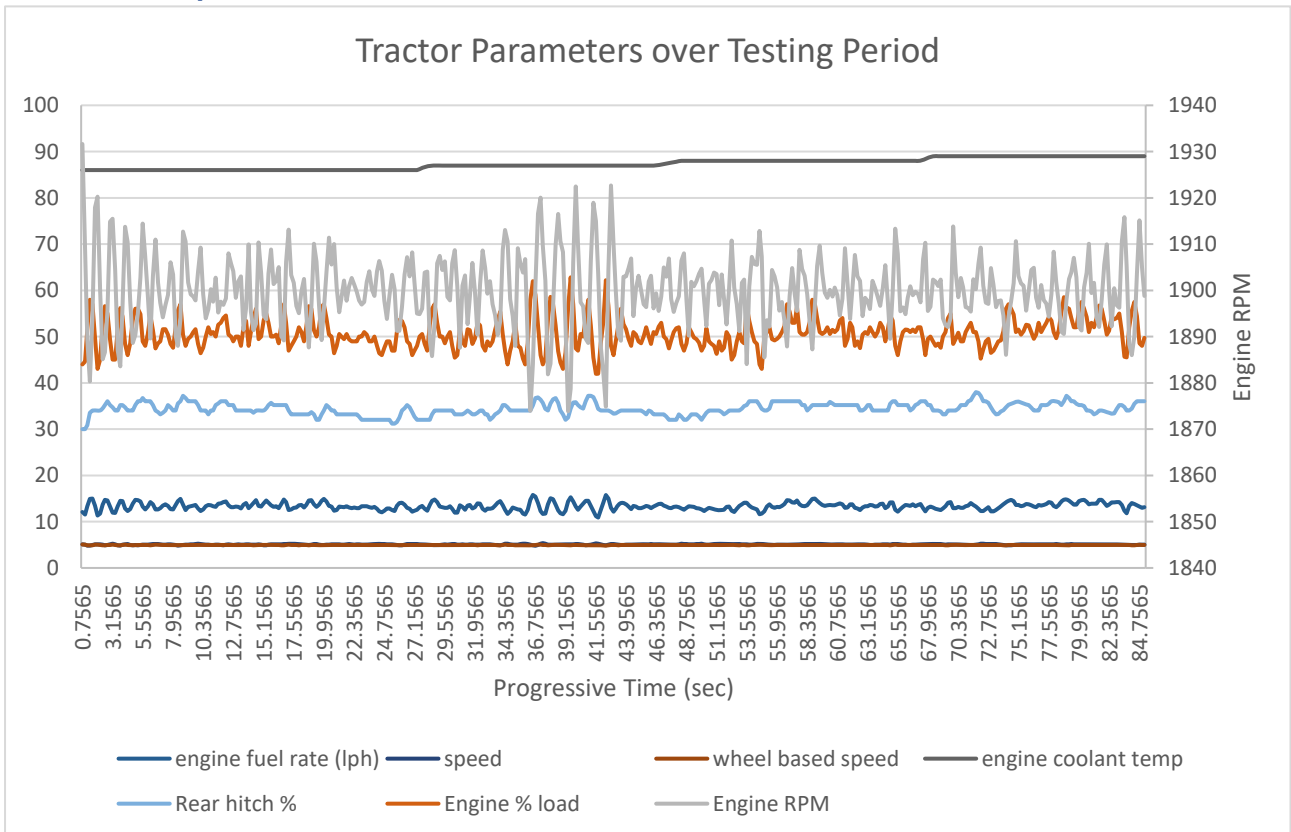
350mm – 5kph



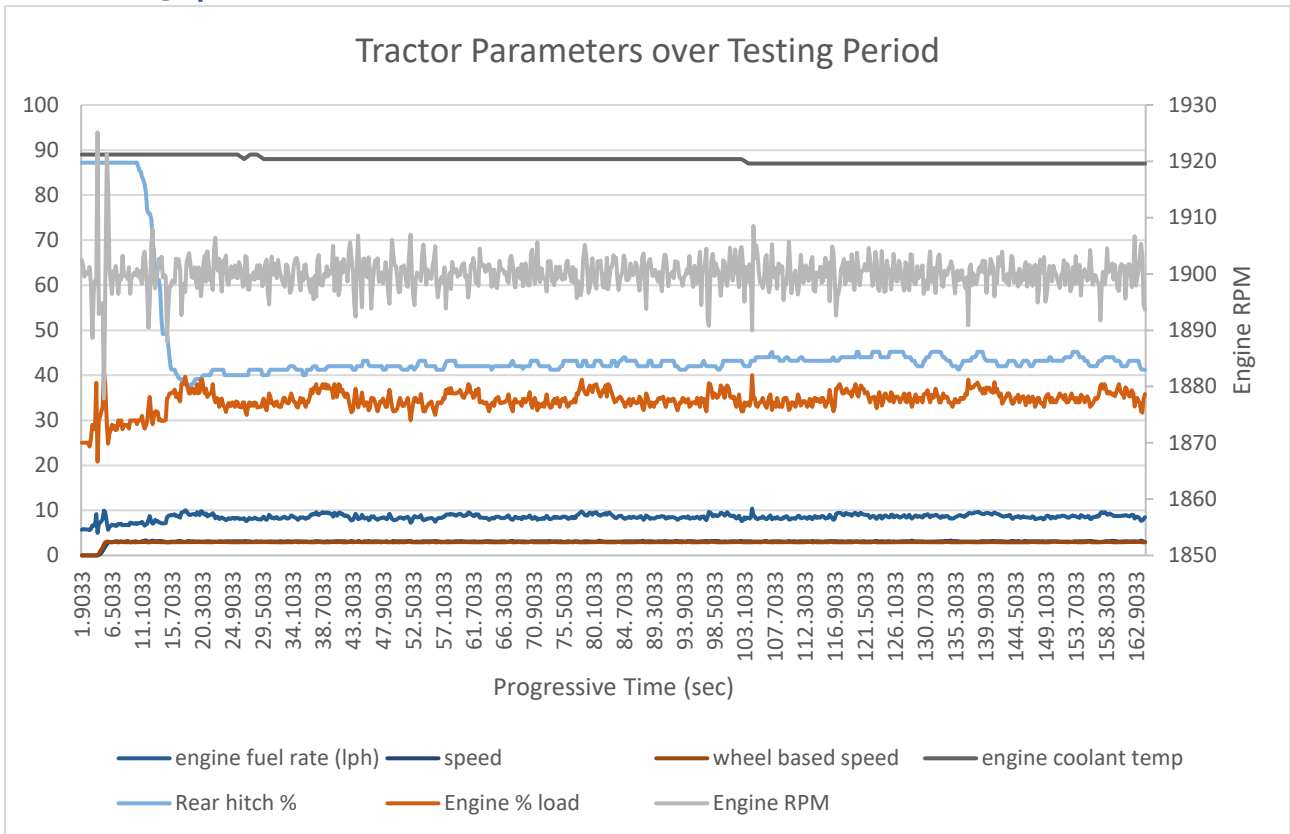
300mm – 3kph



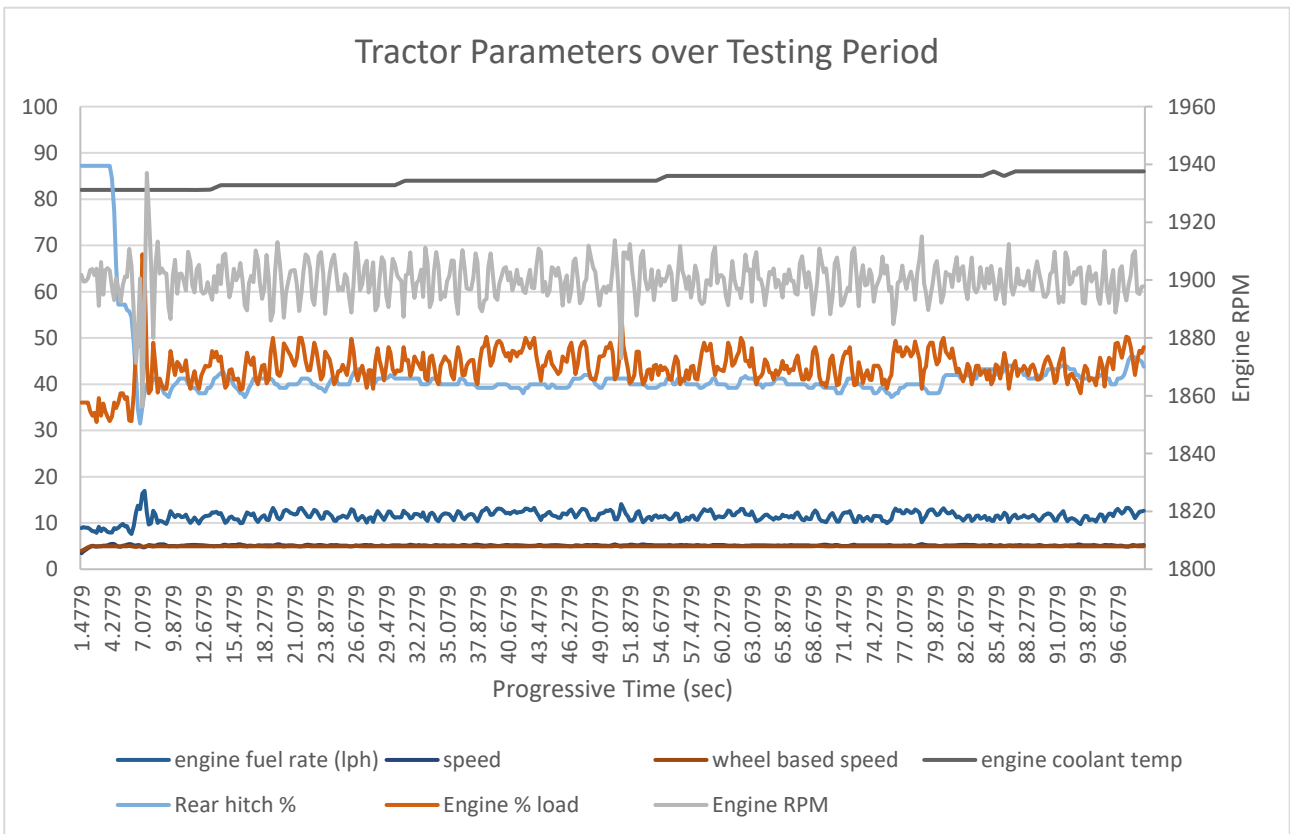
300mm – 5kph



200mm – 3kph

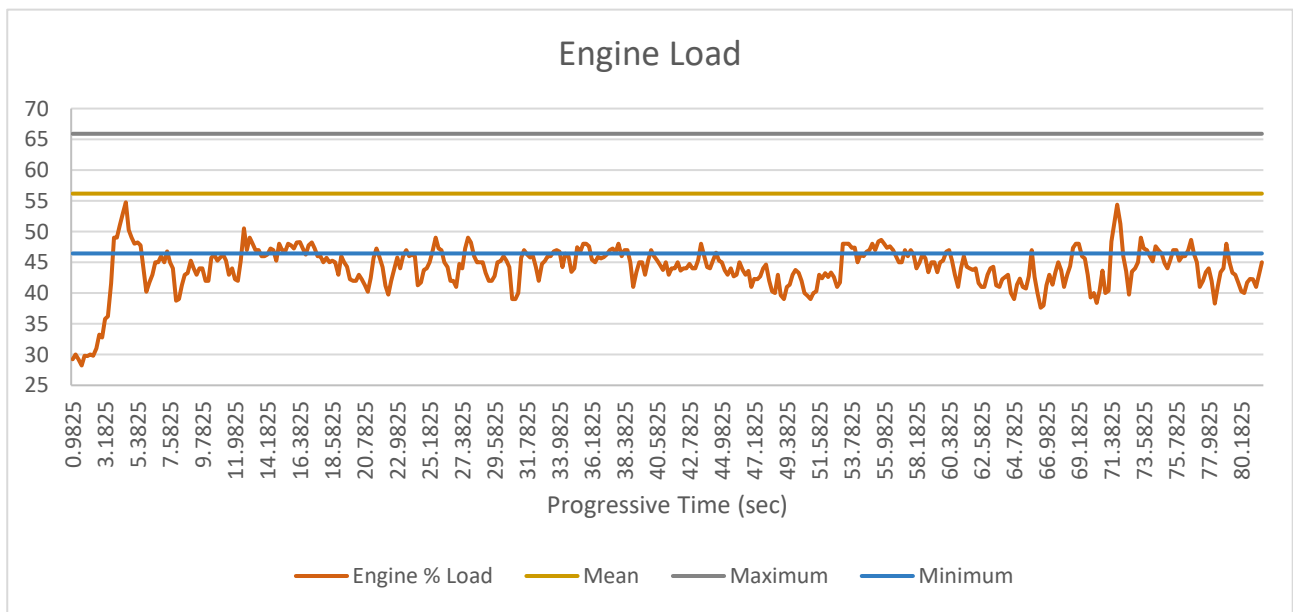
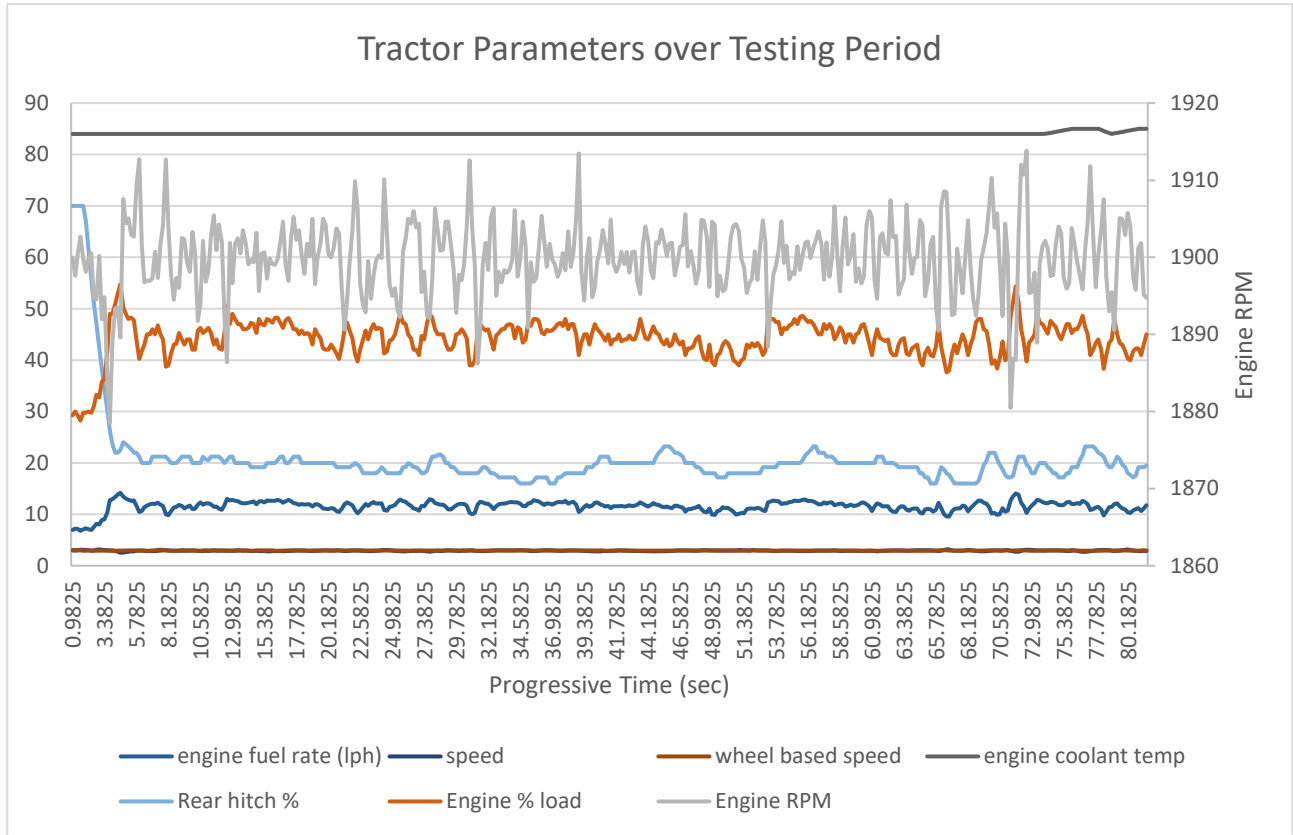


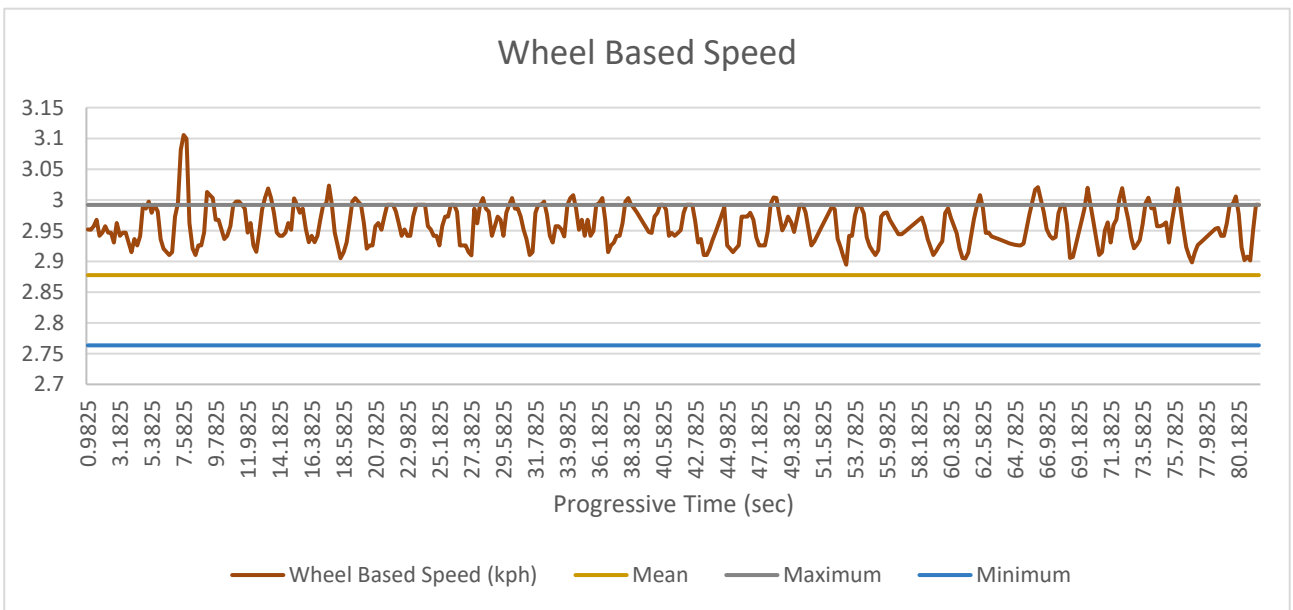
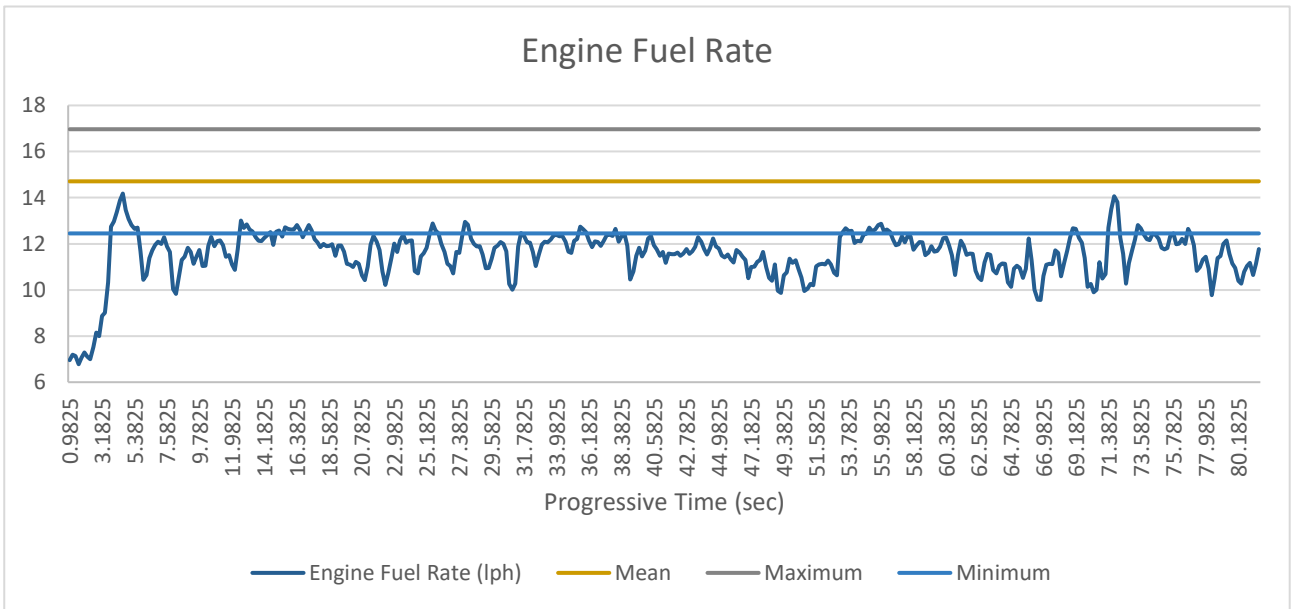
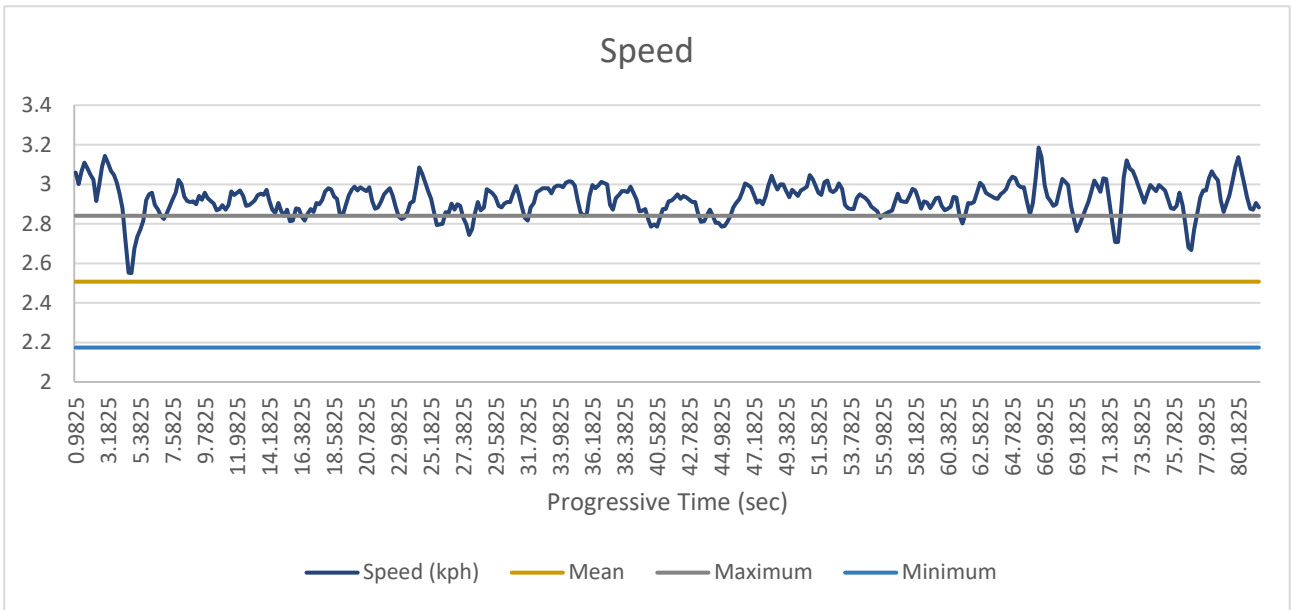
200mm – 5kph

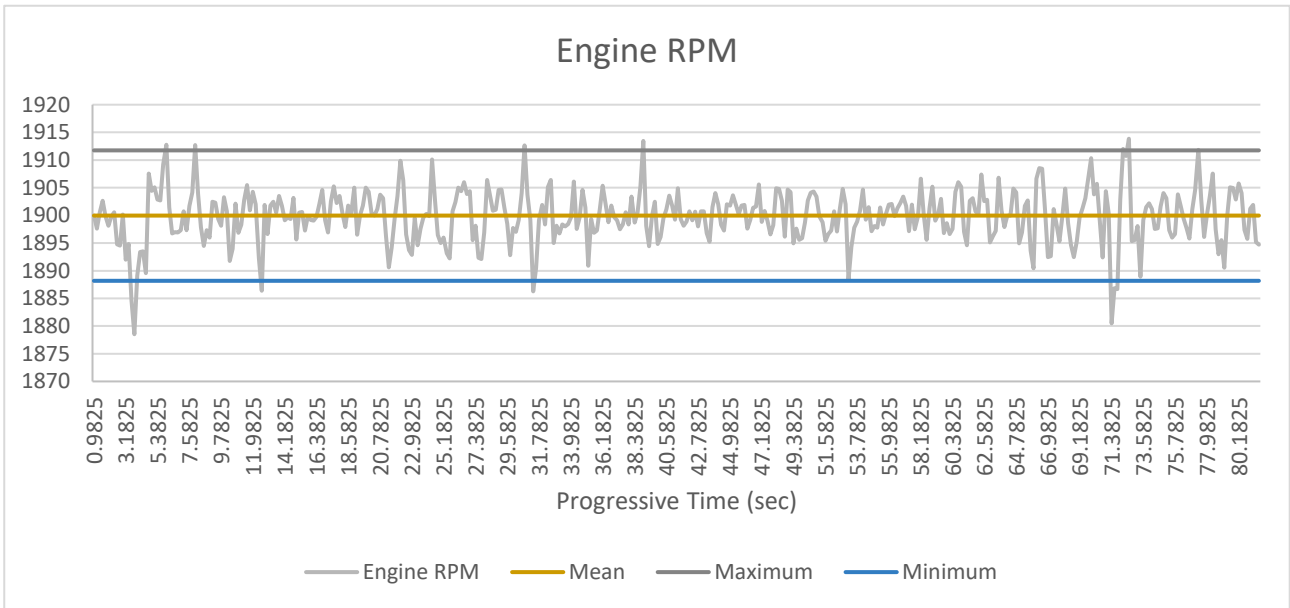
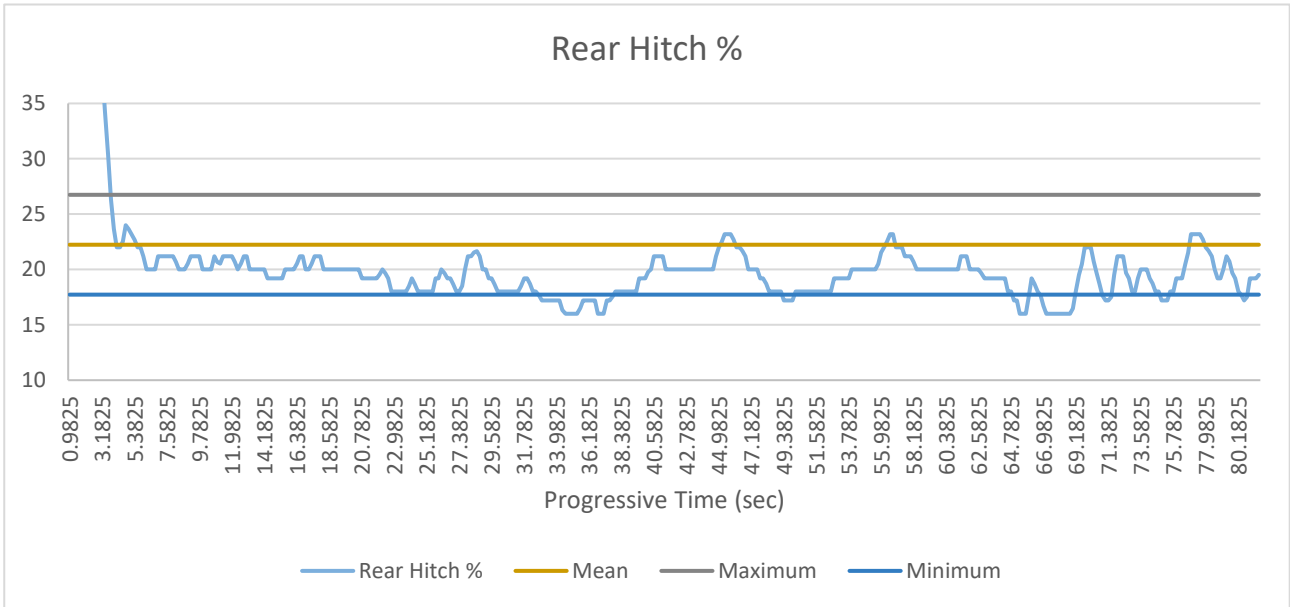
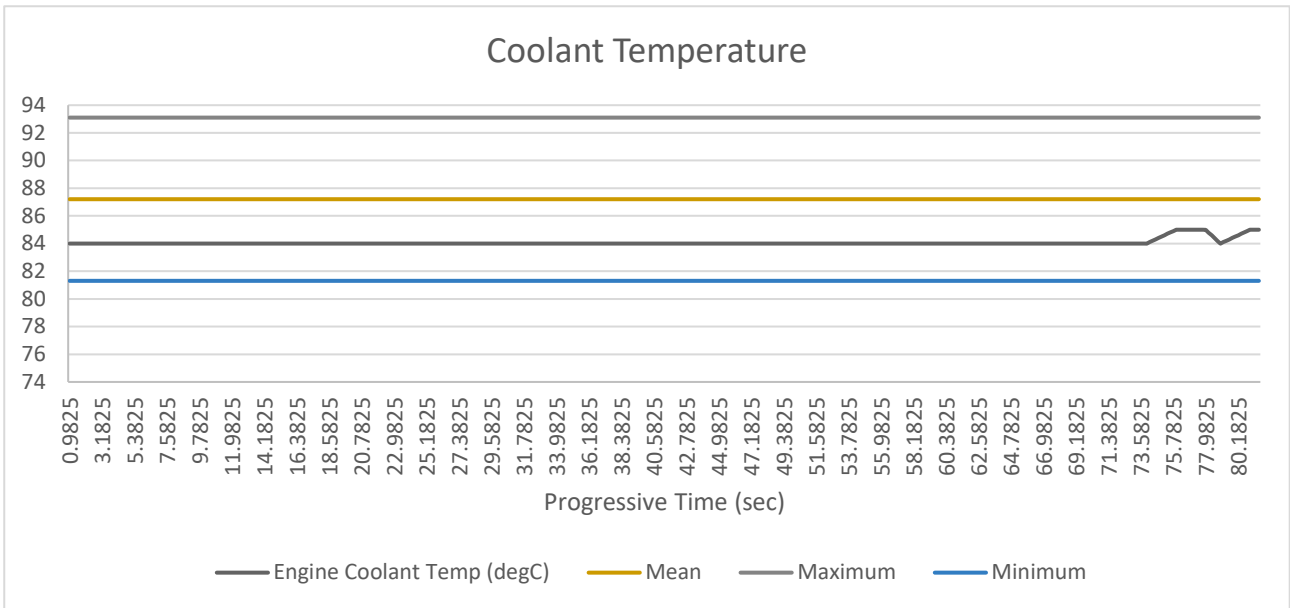


Appendix G – 3PL Deep Ripper – Ripper shank shear pin breaking data

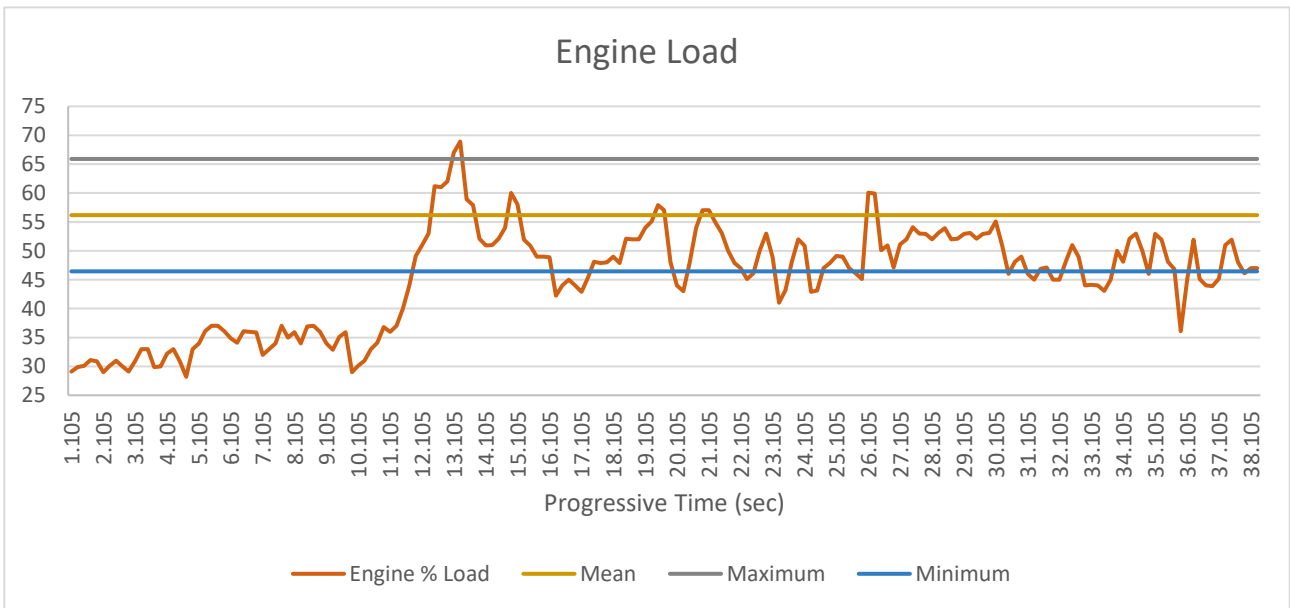
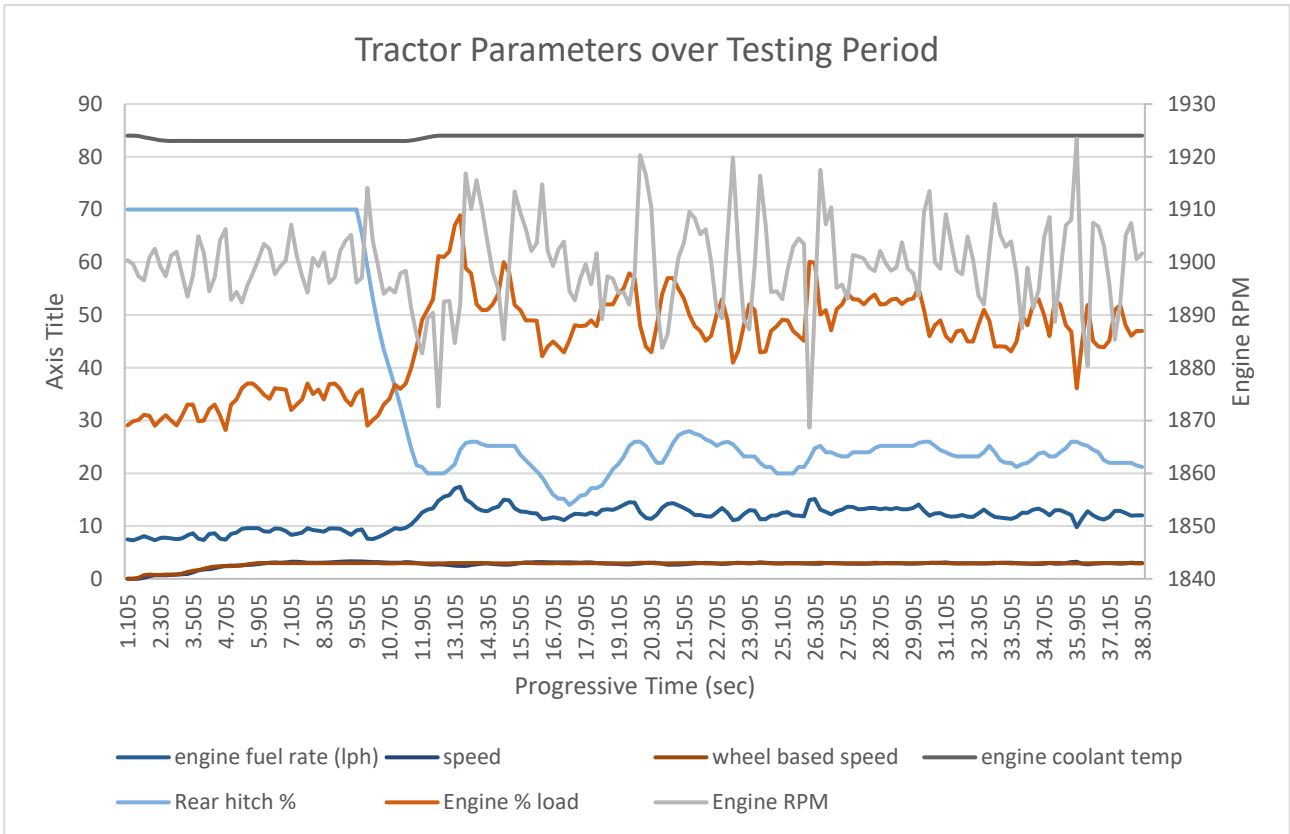
350mm – 3kph

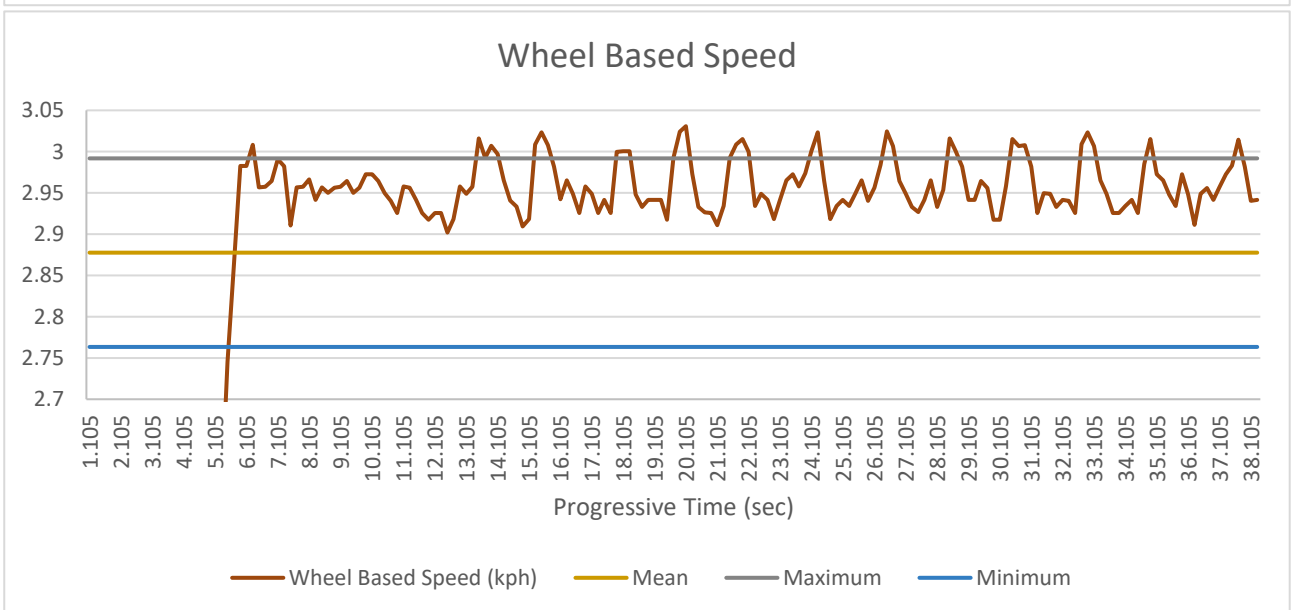
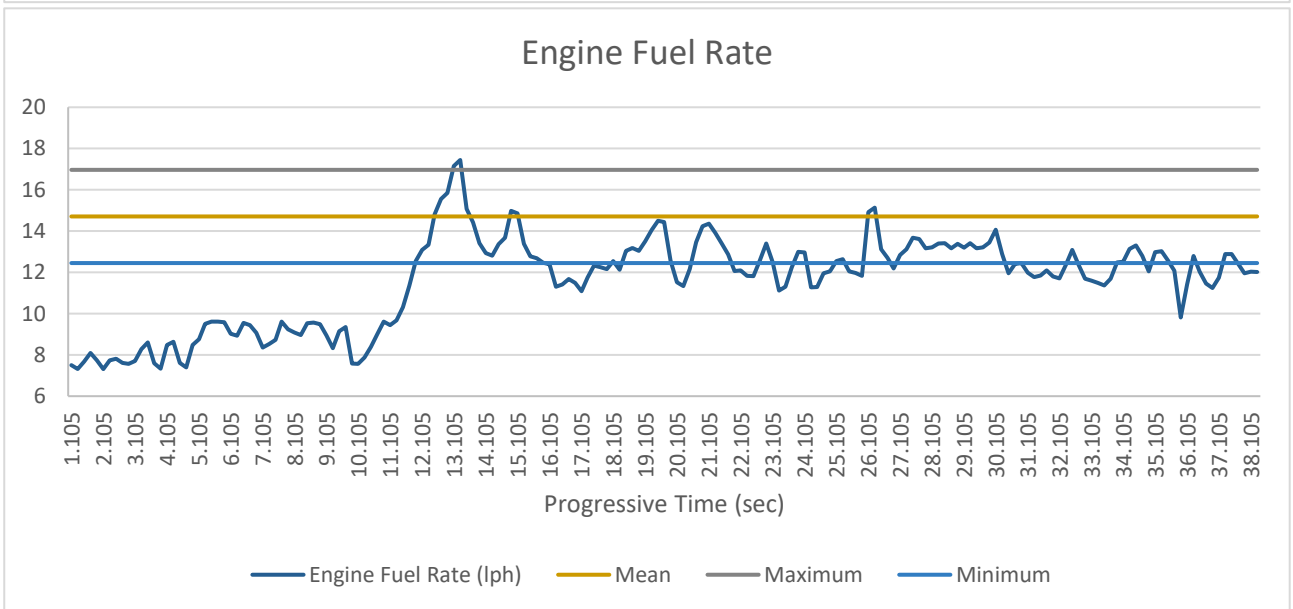
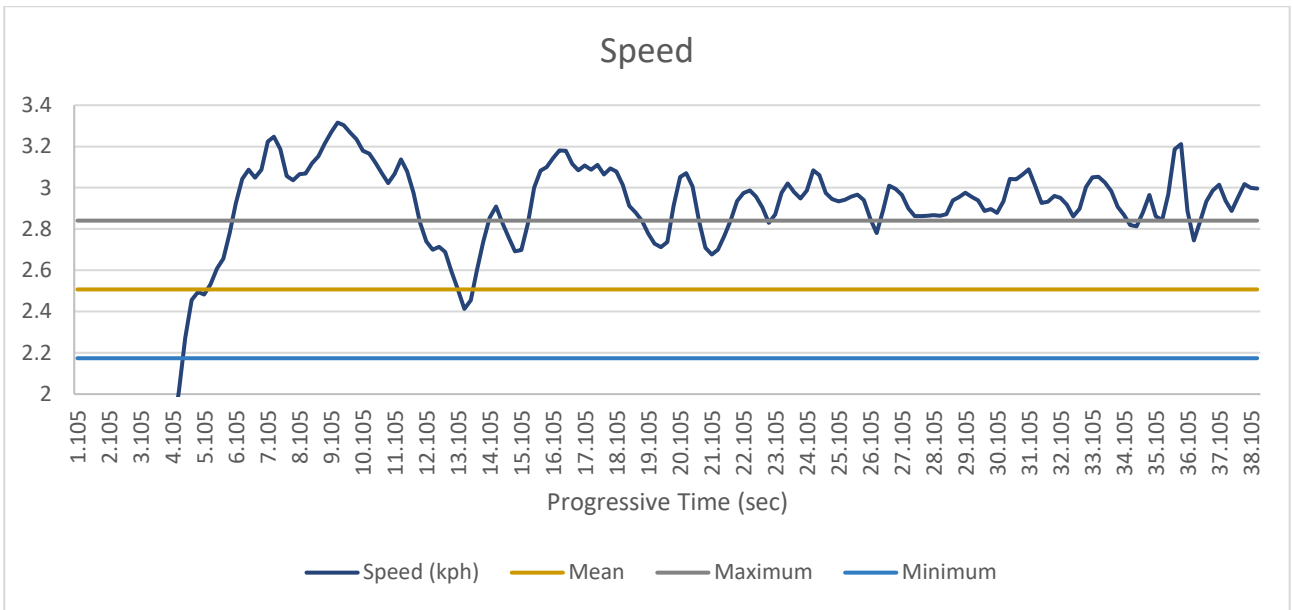


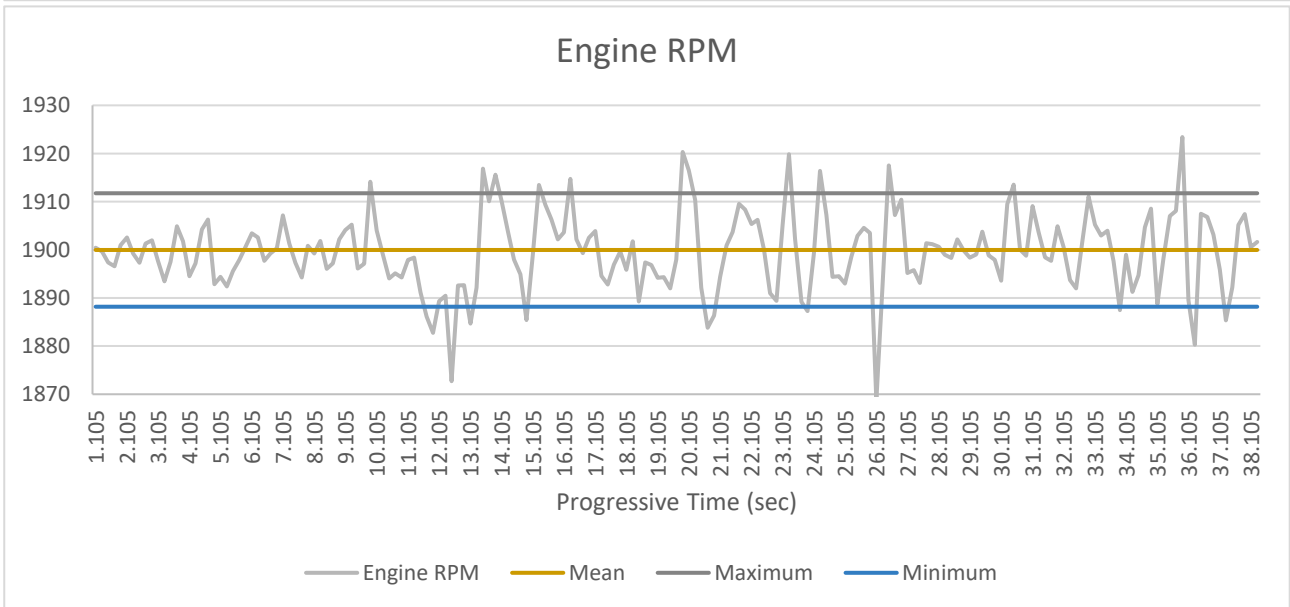
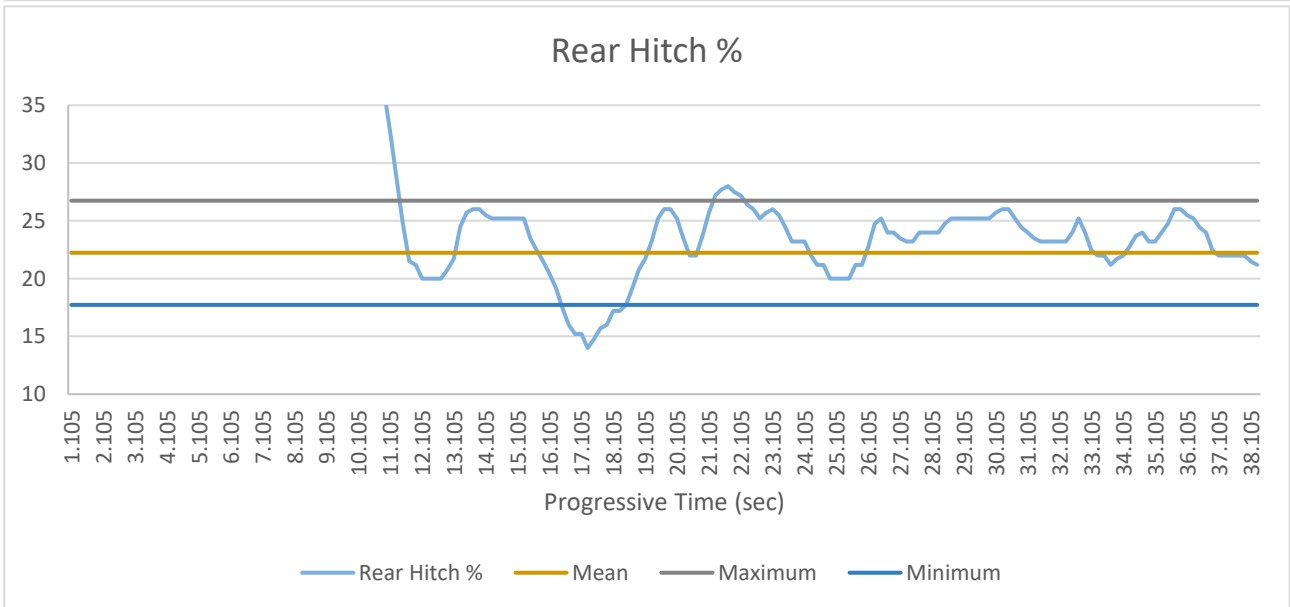
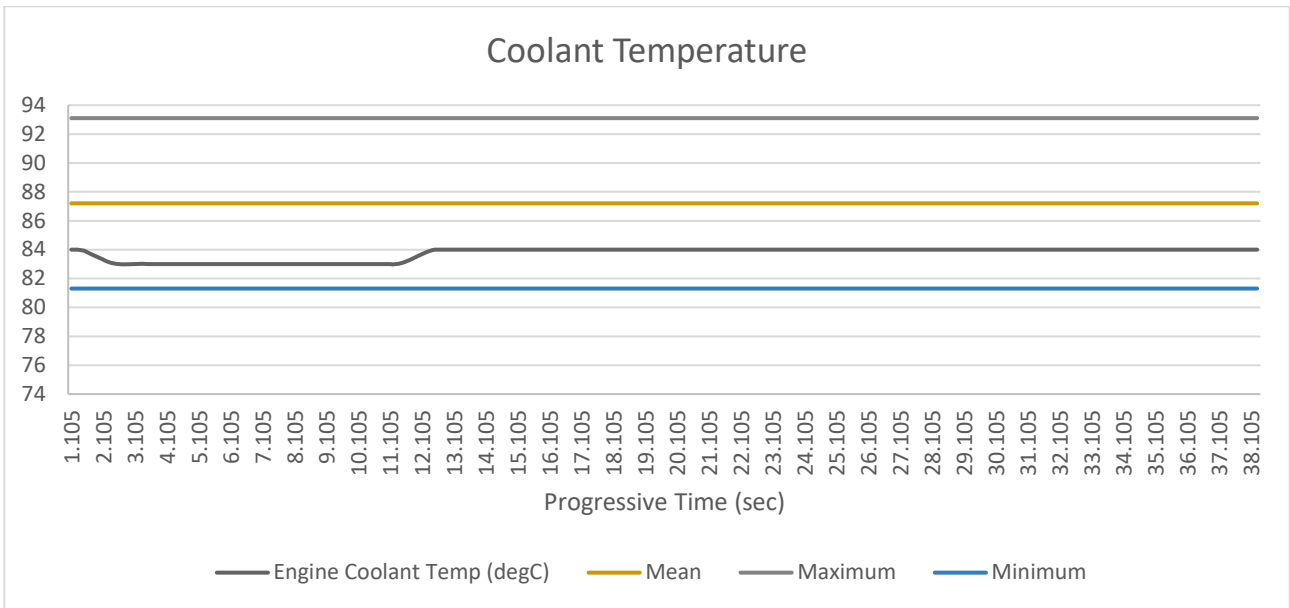




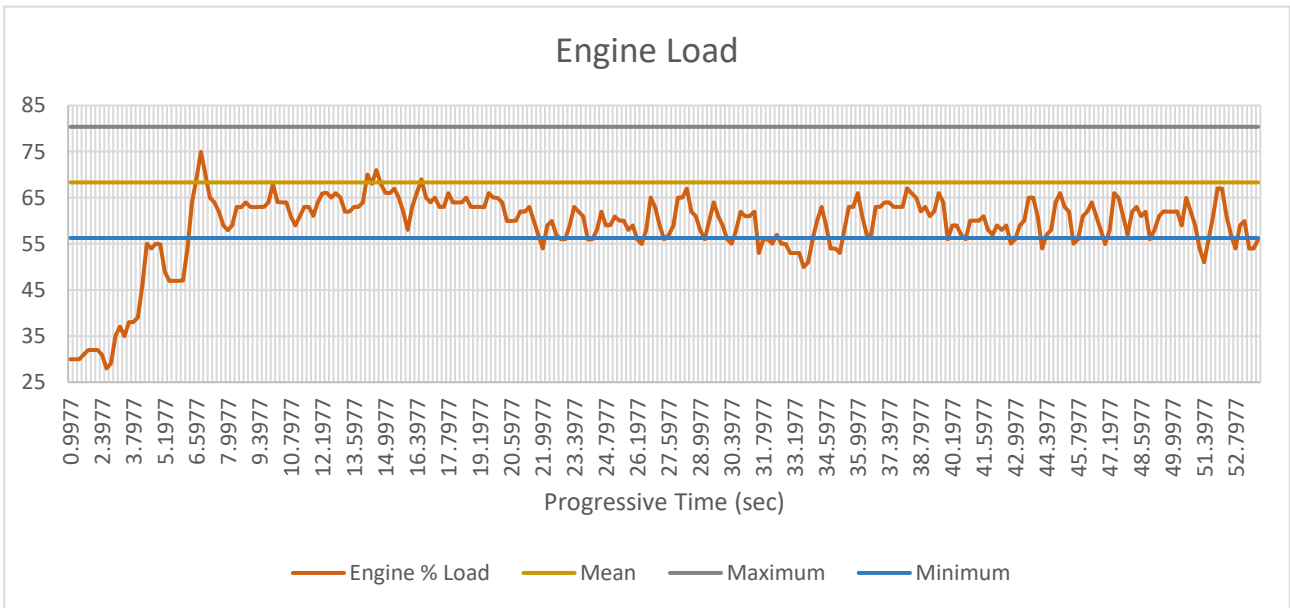
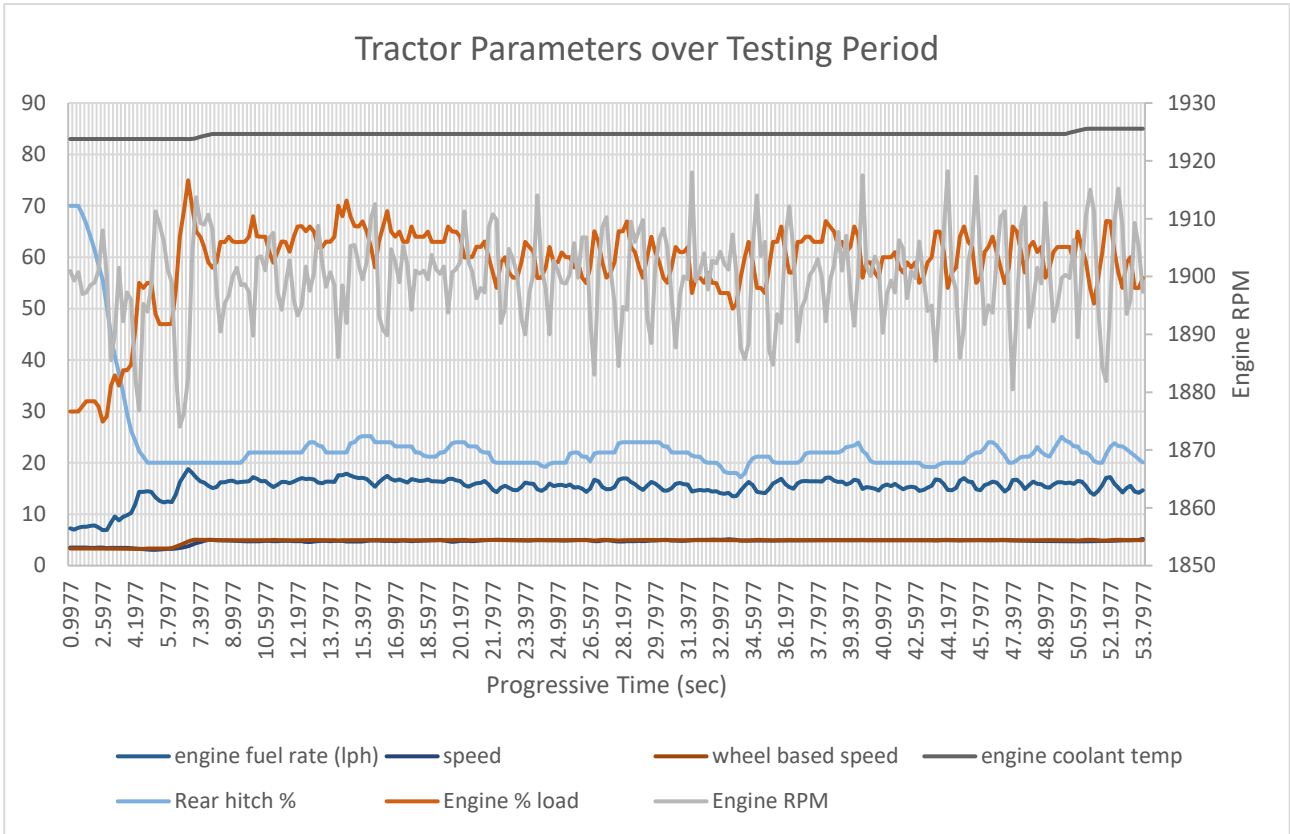
350mm – 3kph – 2

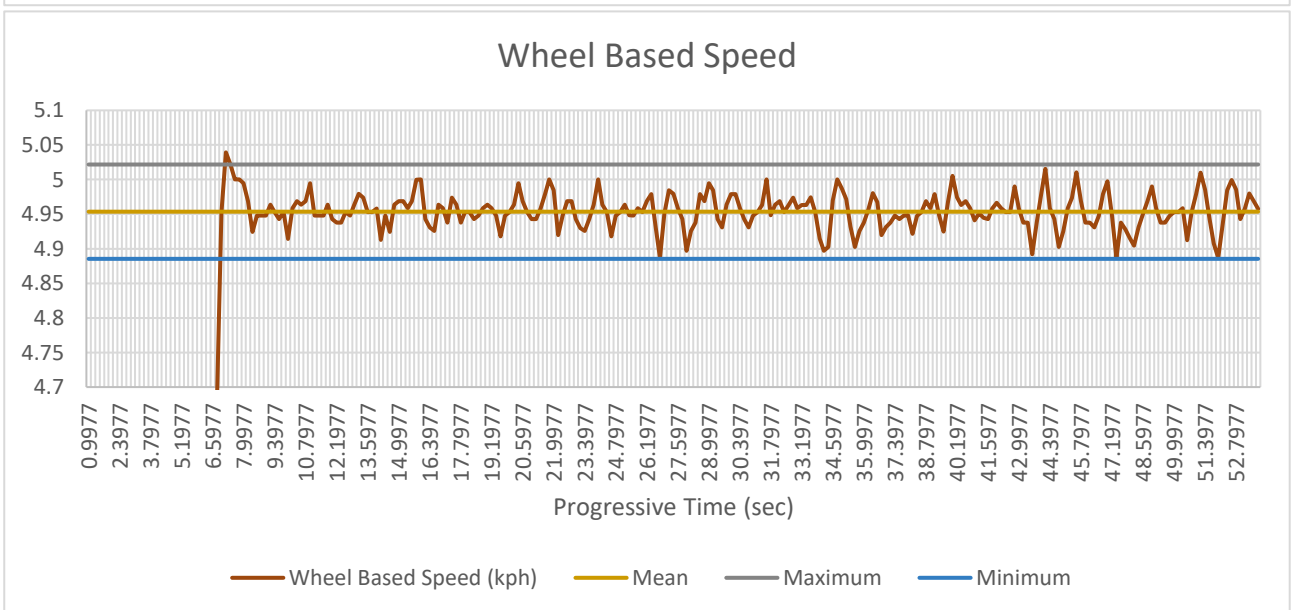
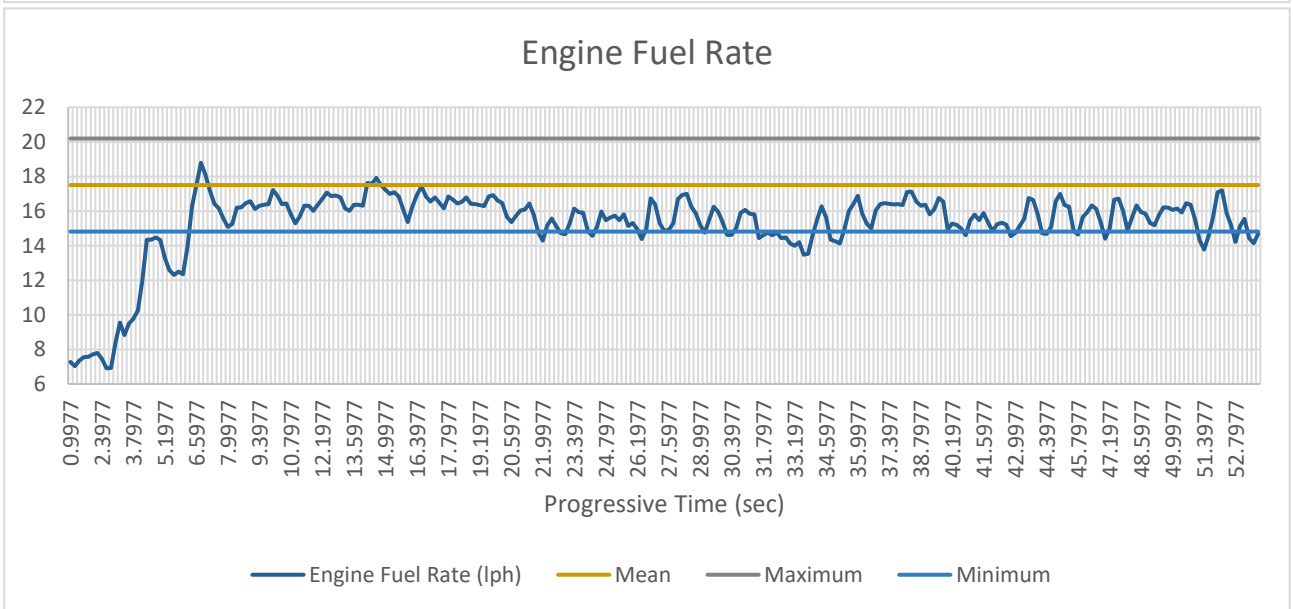
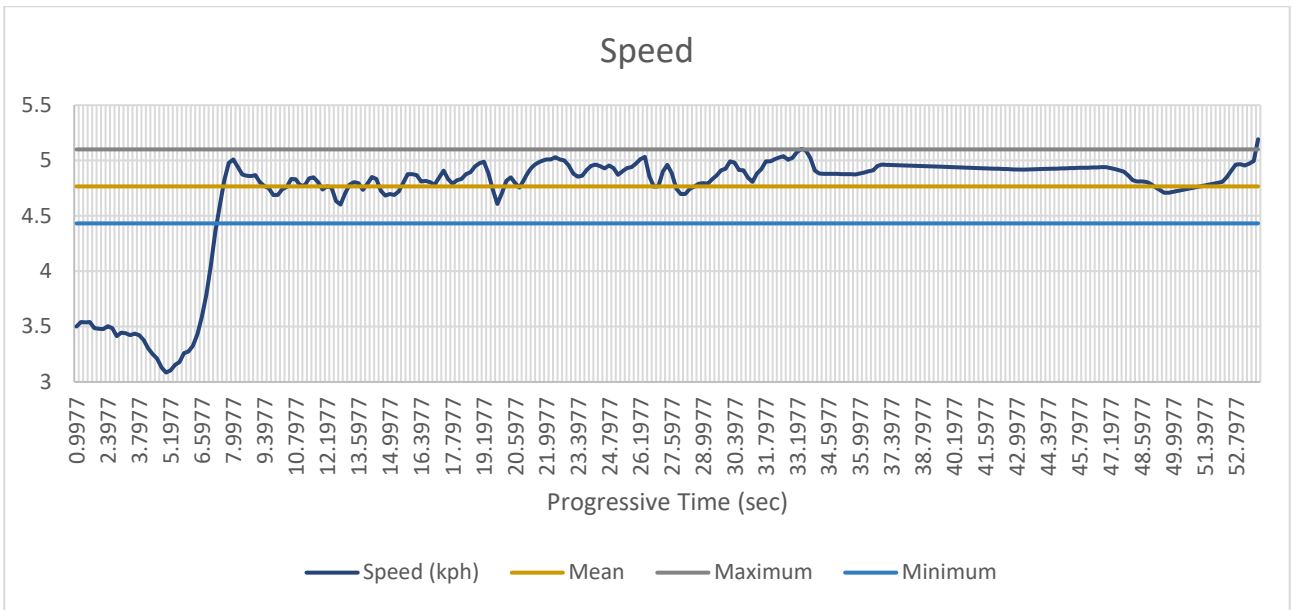




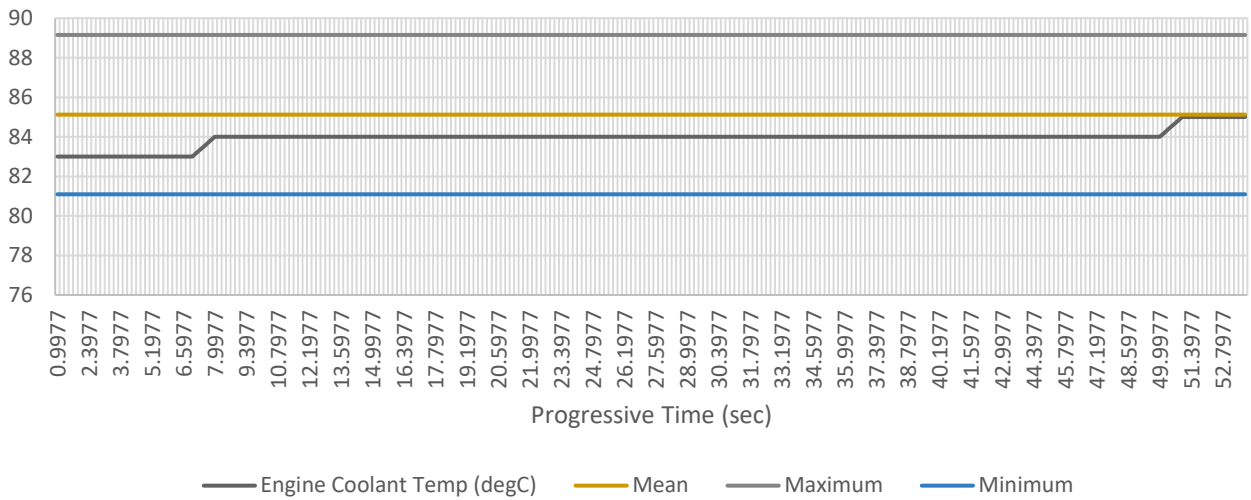


350mm – 5kph

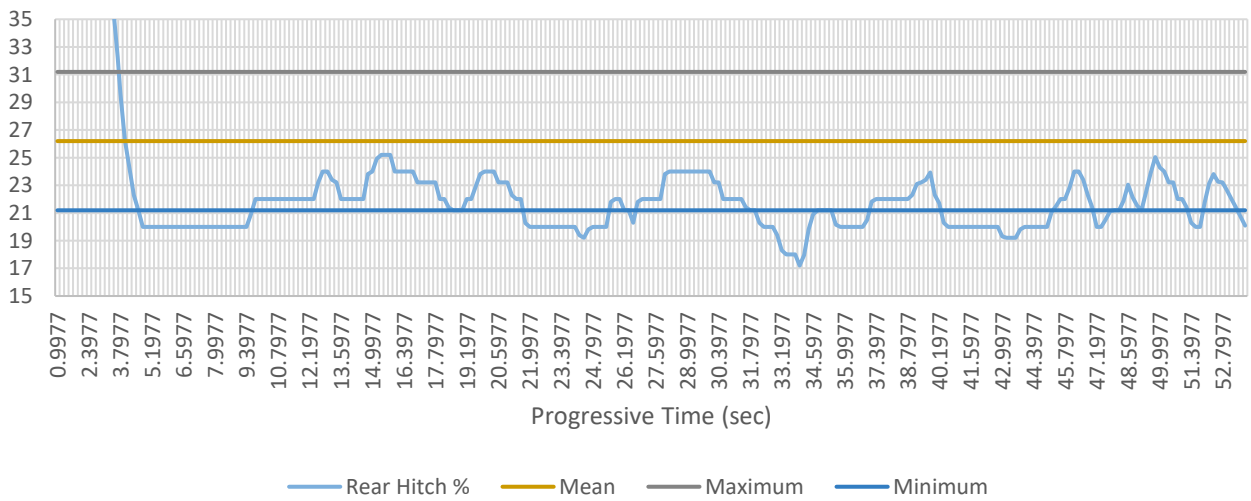




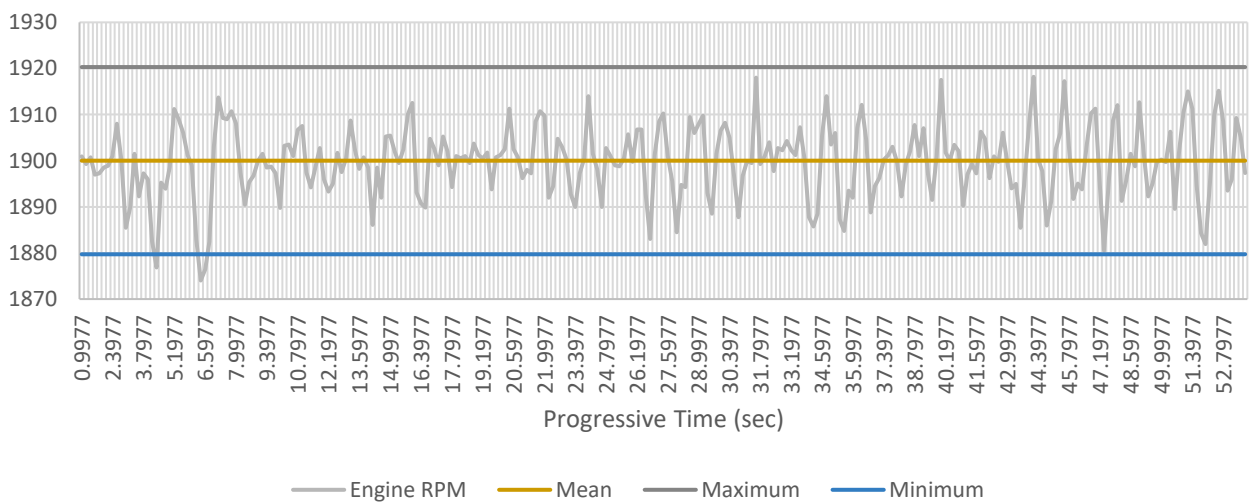
Coolant Temperature



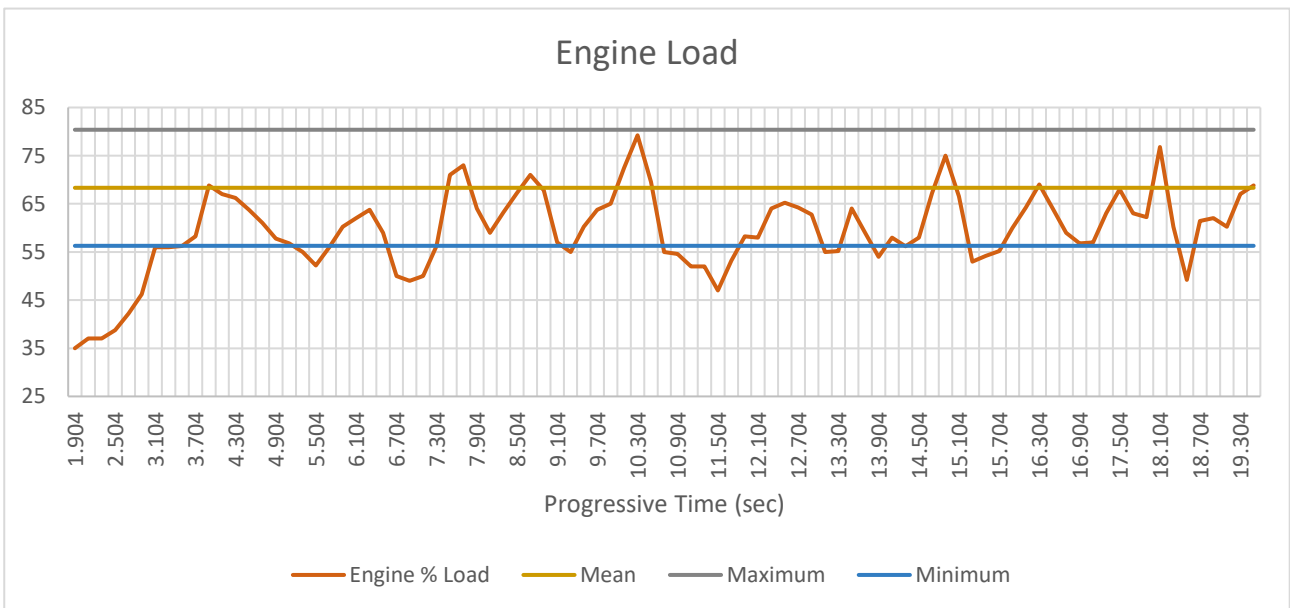
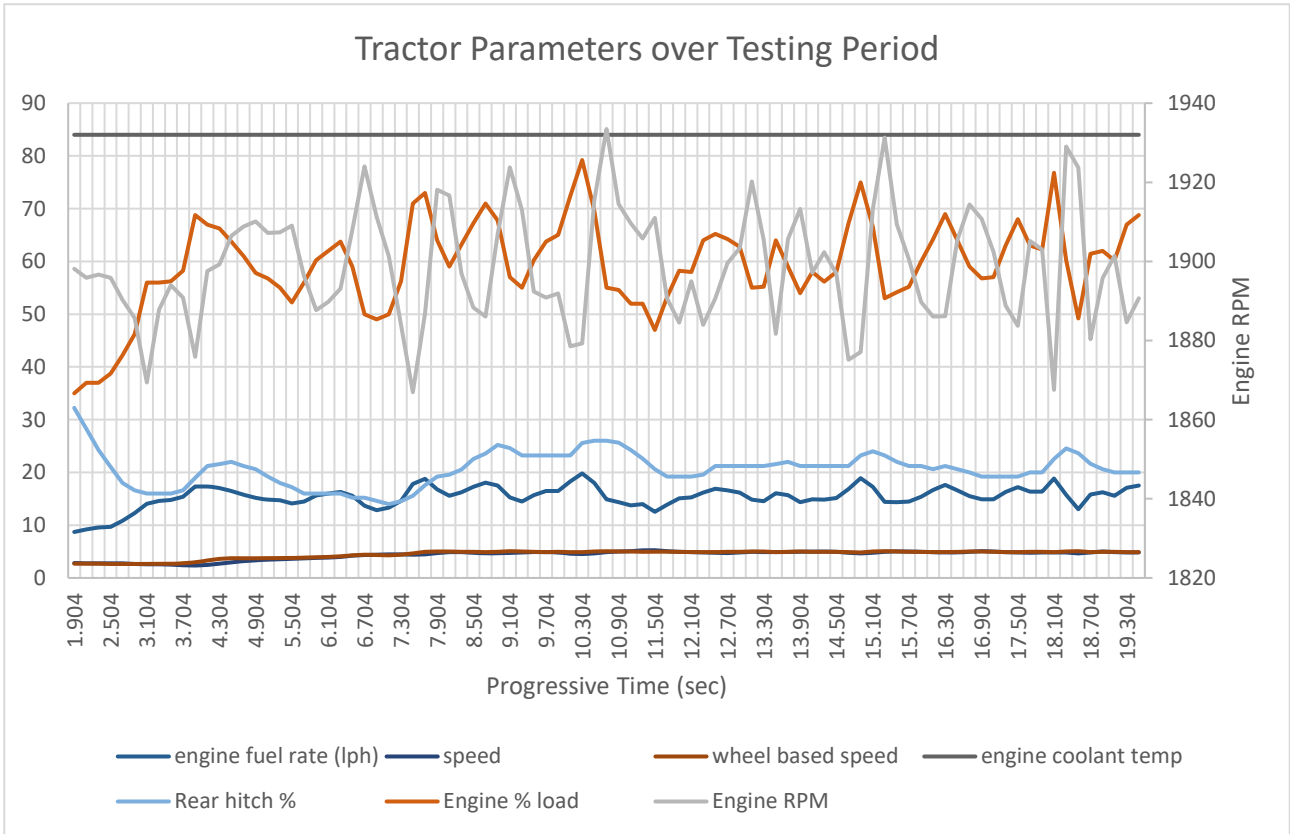
Rear Hitch %

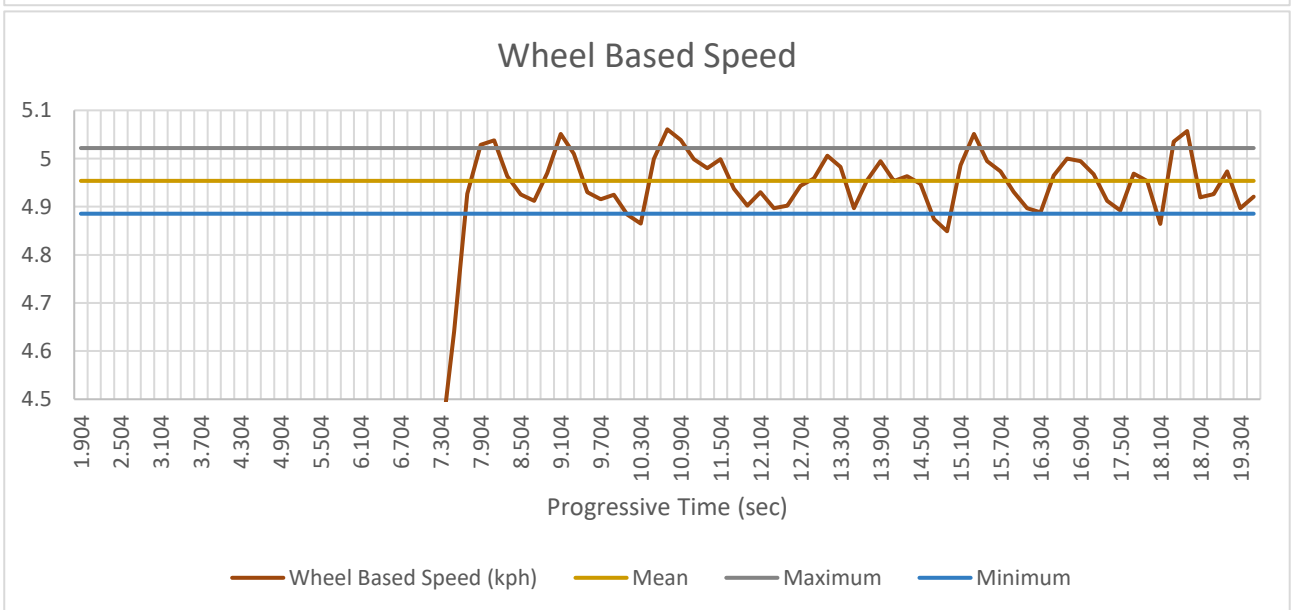
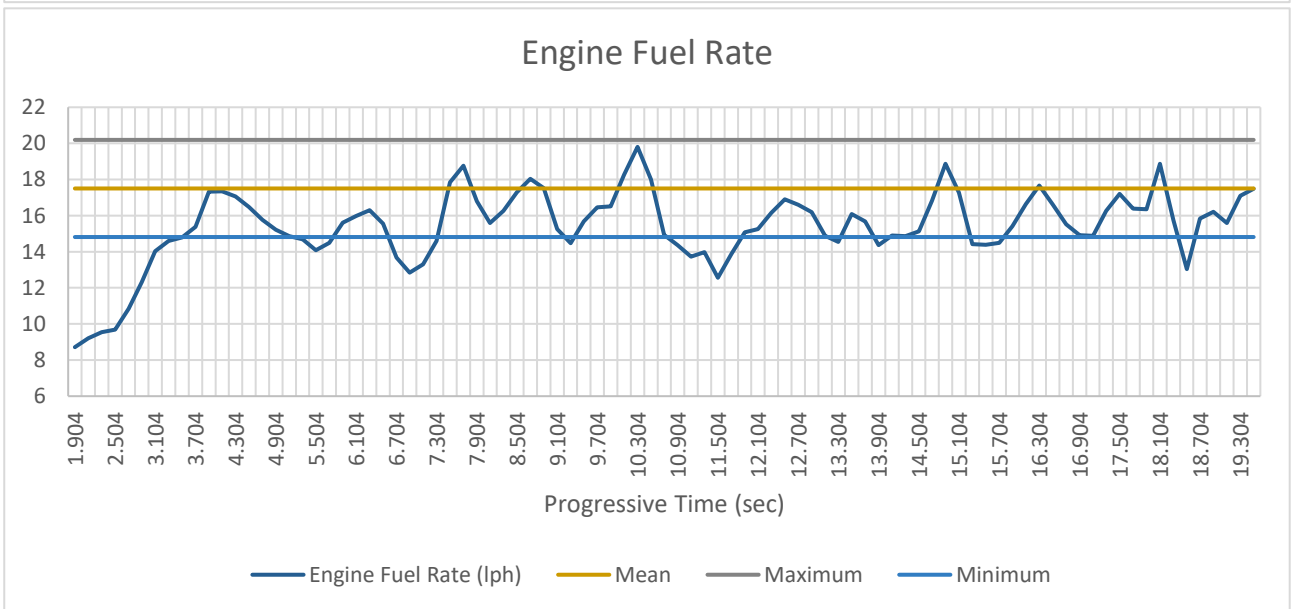
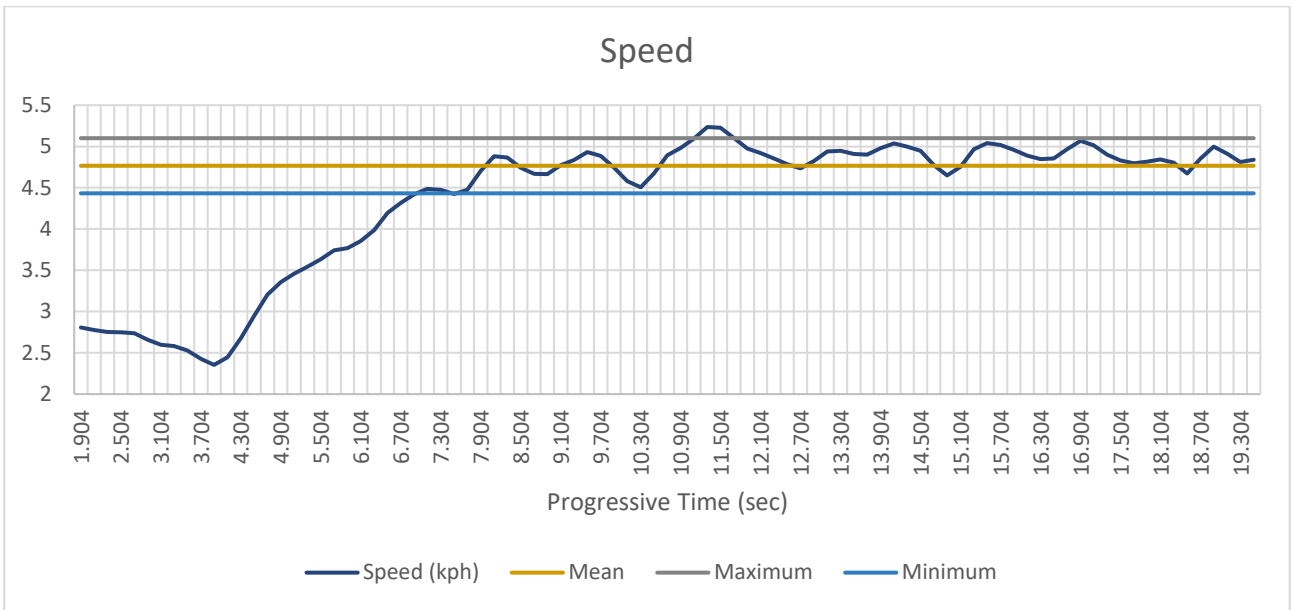


Engine RPM

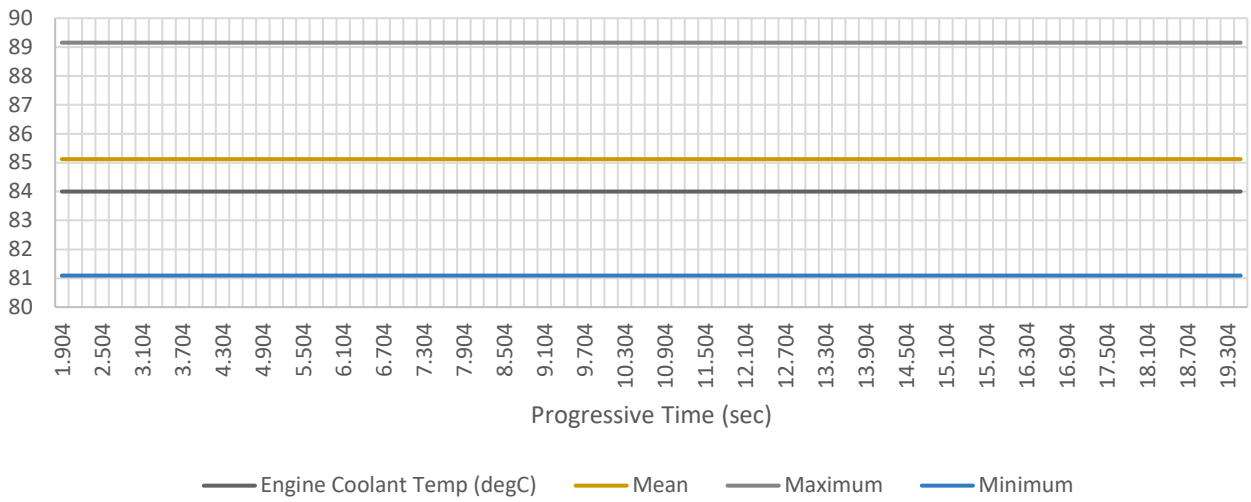


350mm 5kph – 2

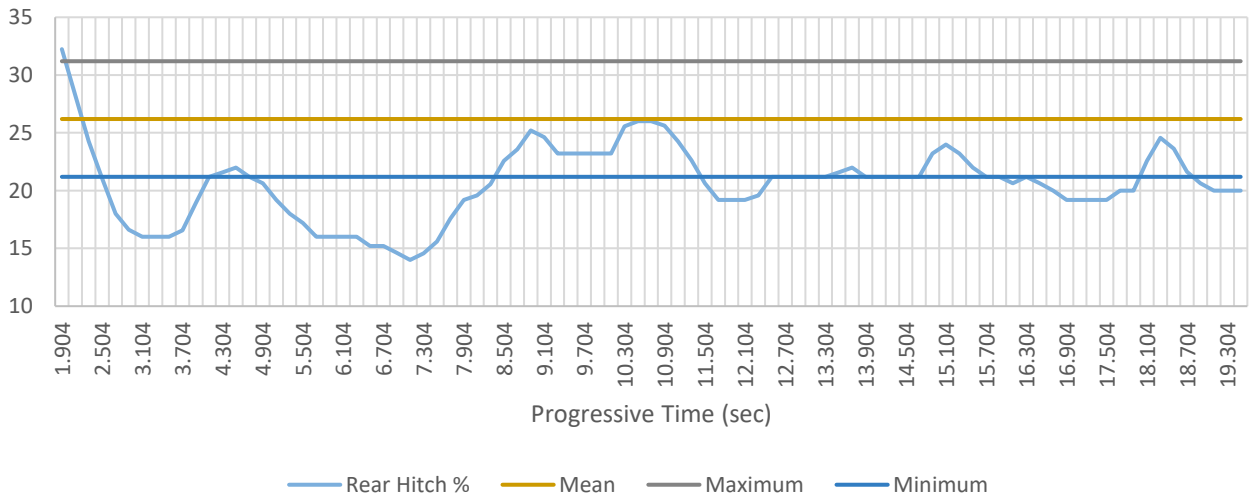




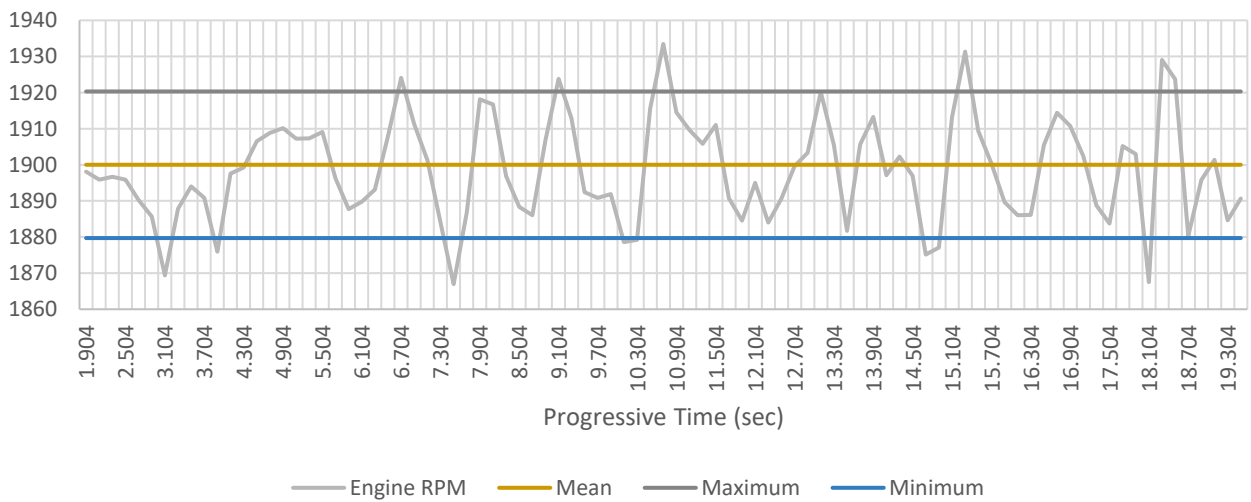
Coolant Temperature



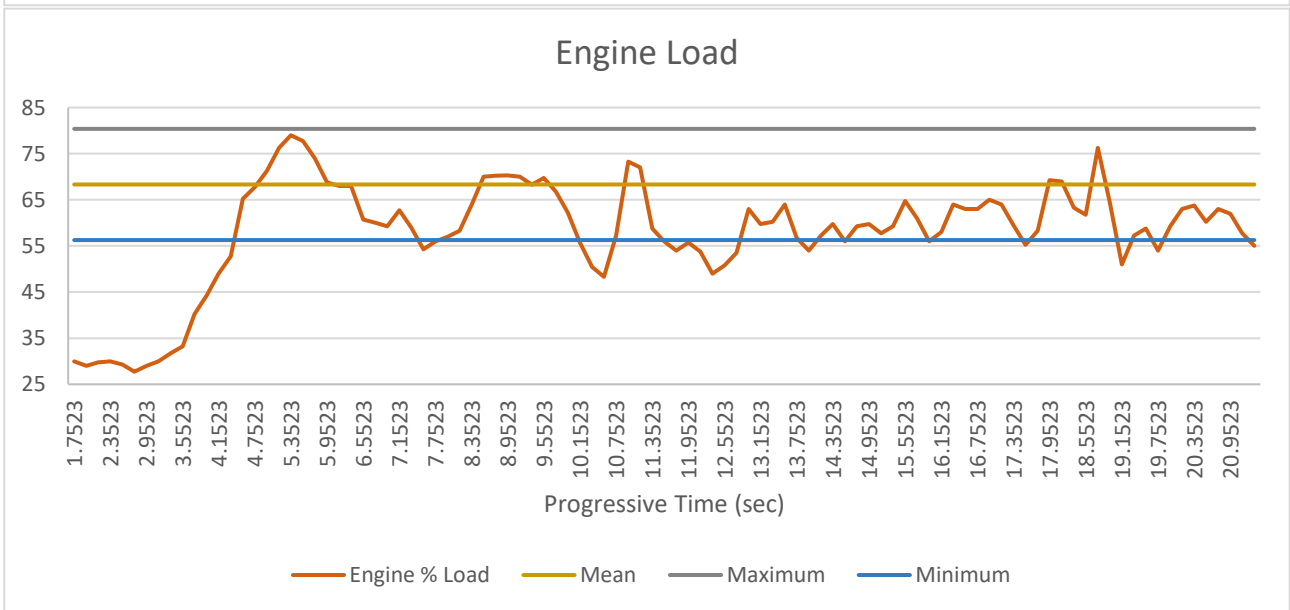
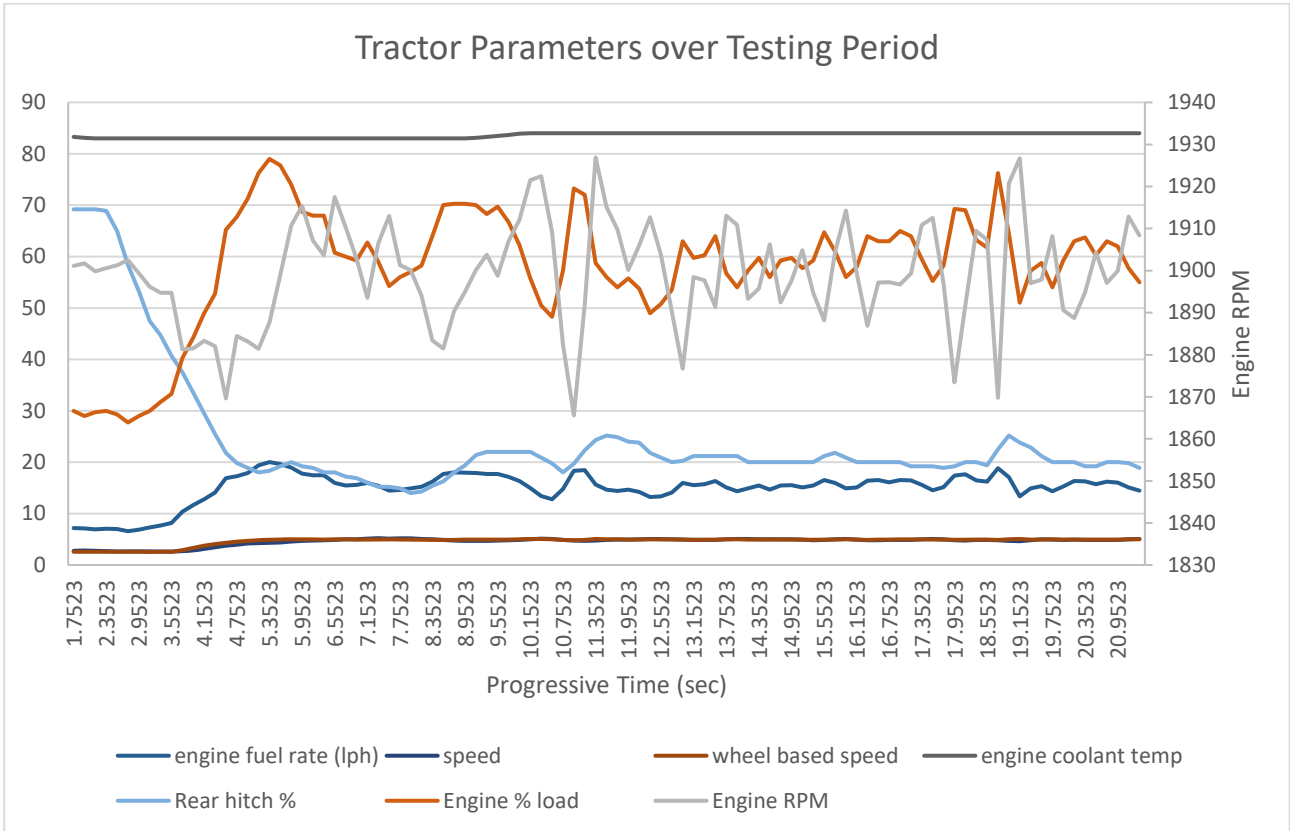
Rear Hitch %

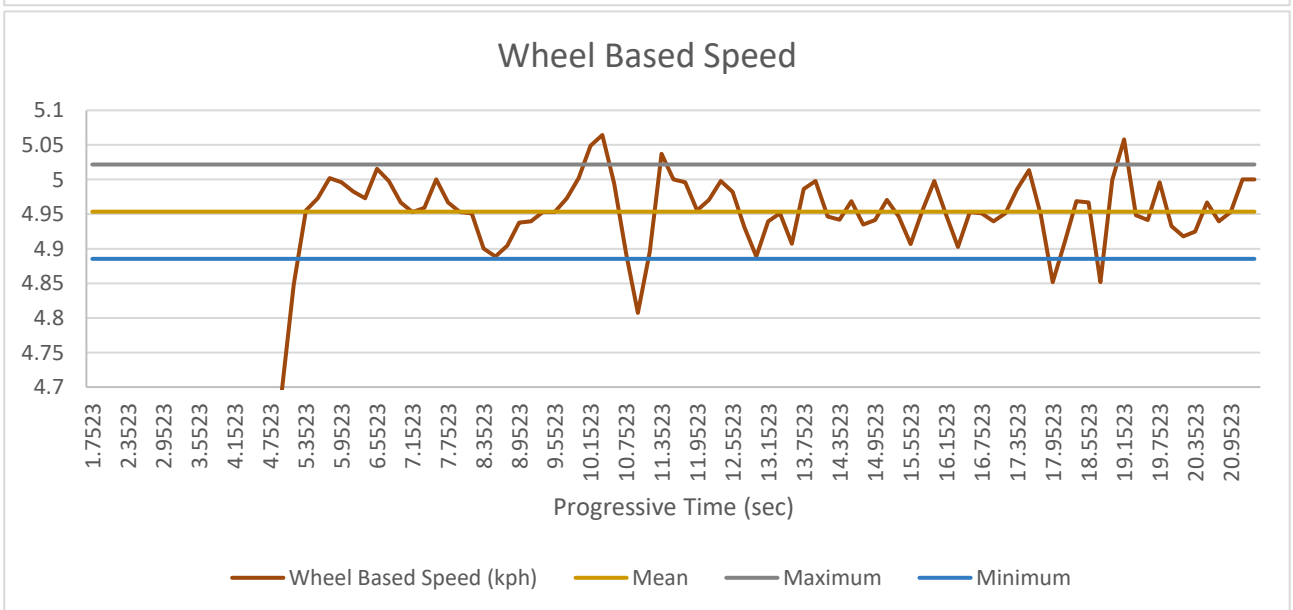
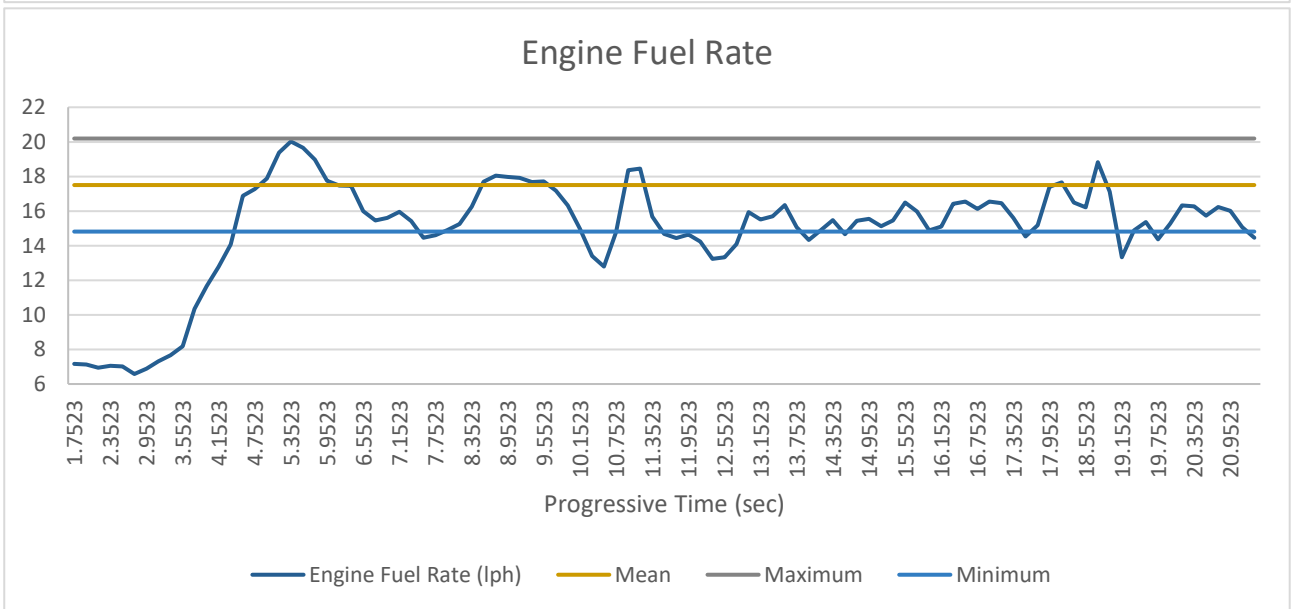
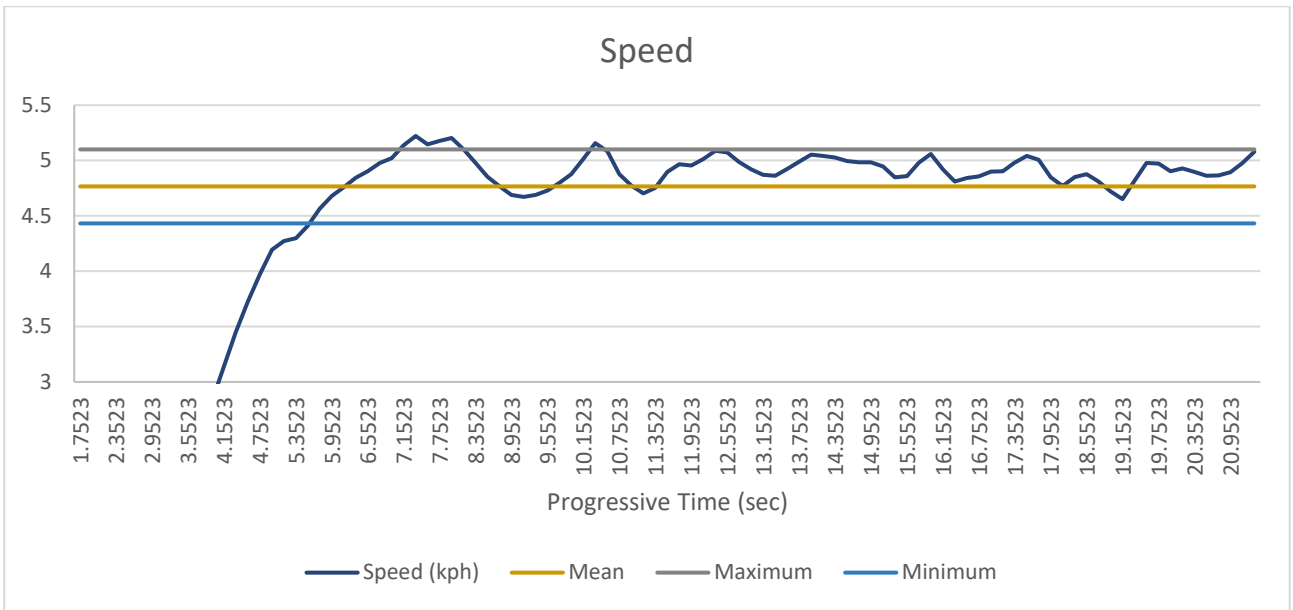


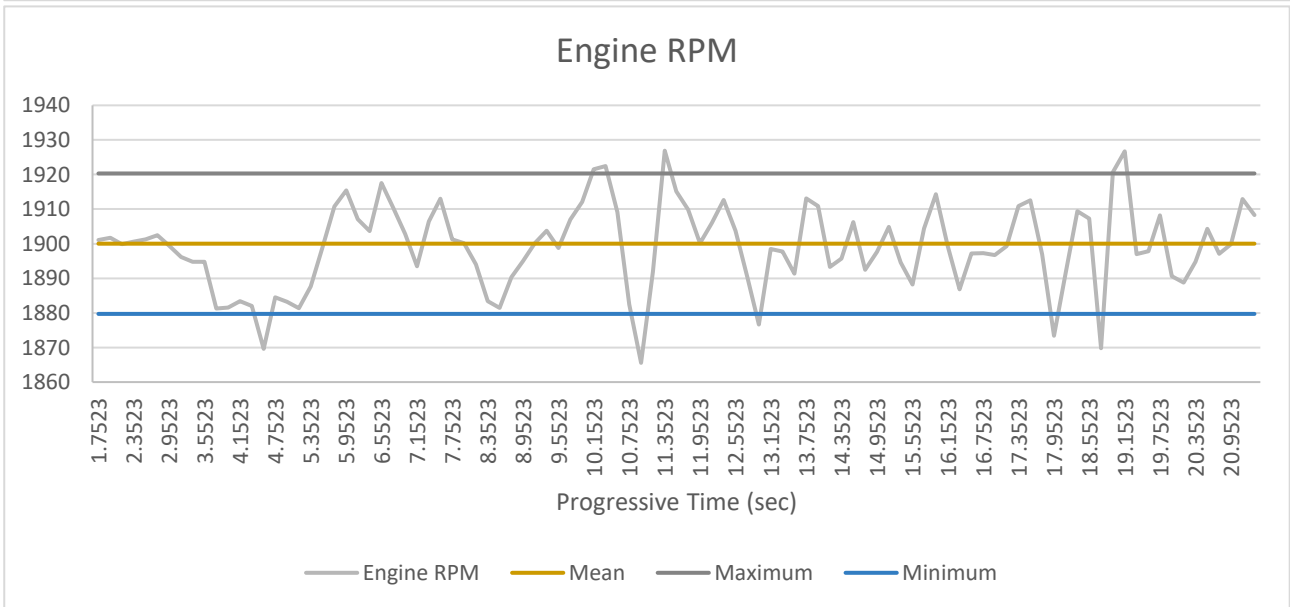
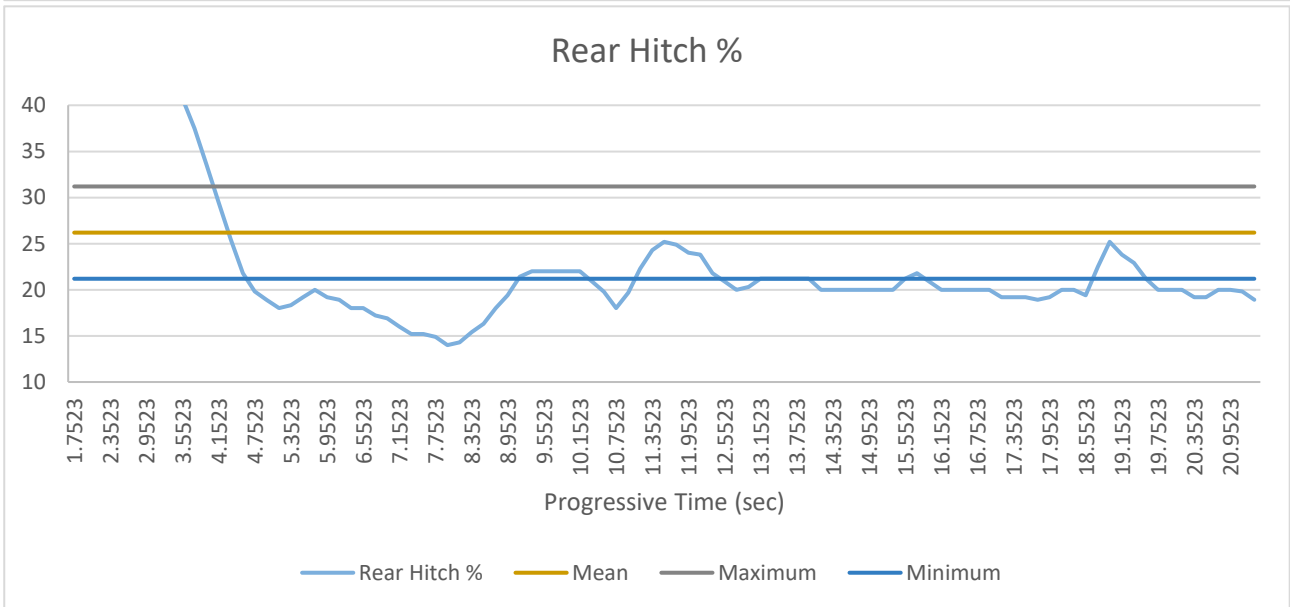
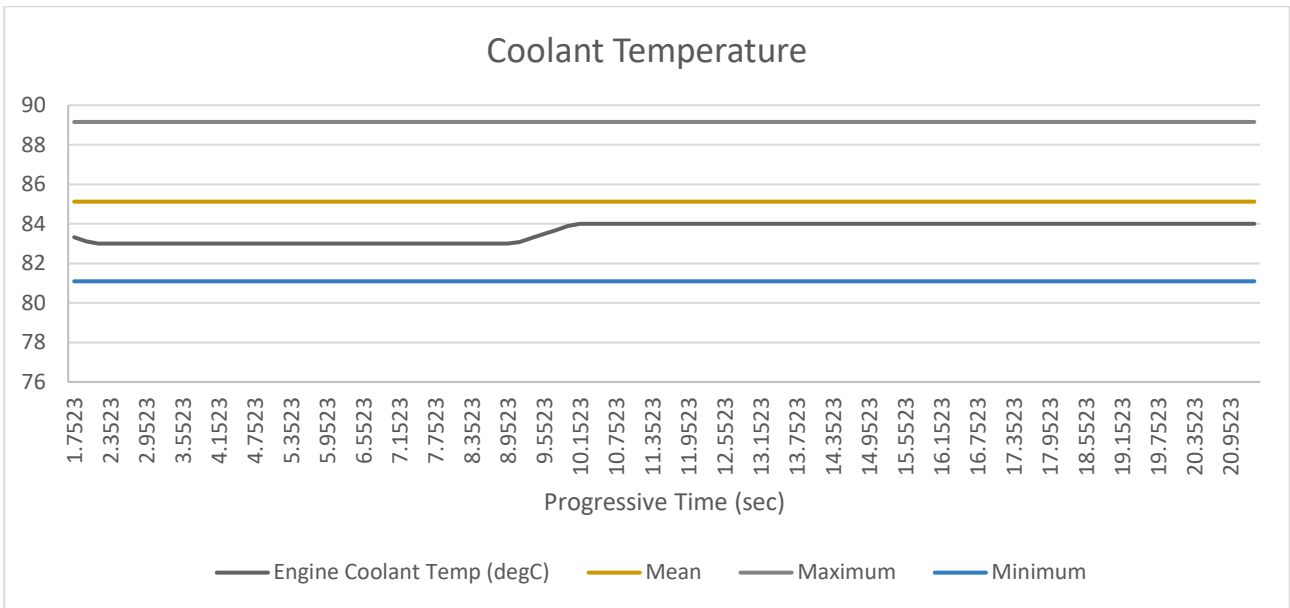
Engine RPM



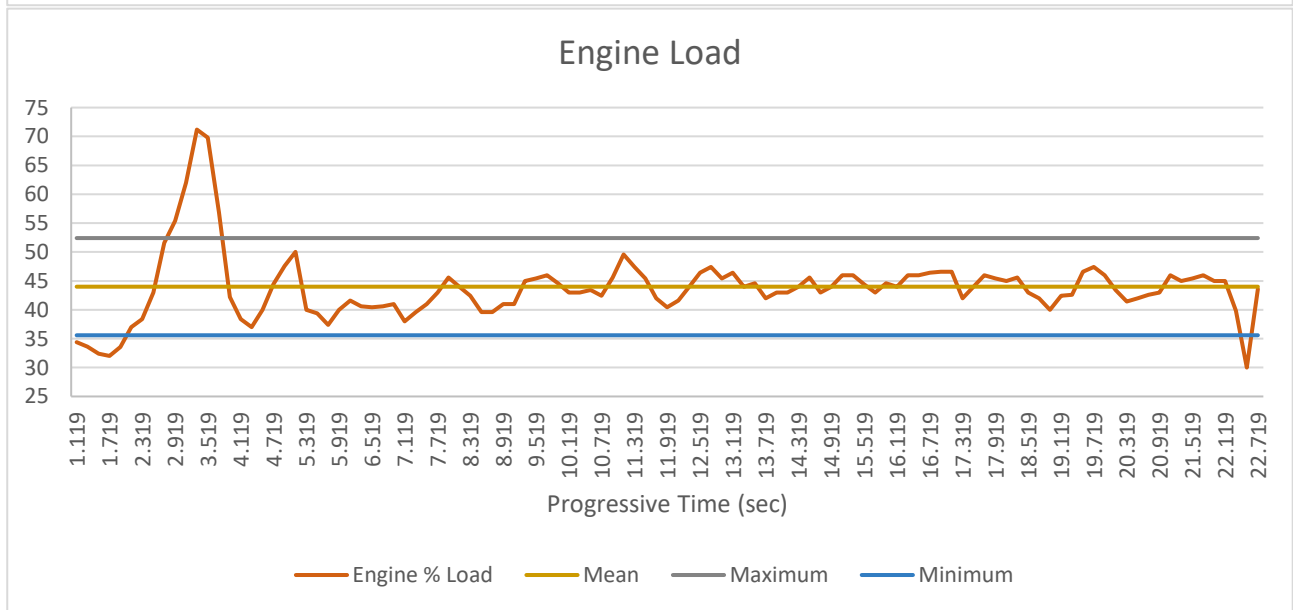
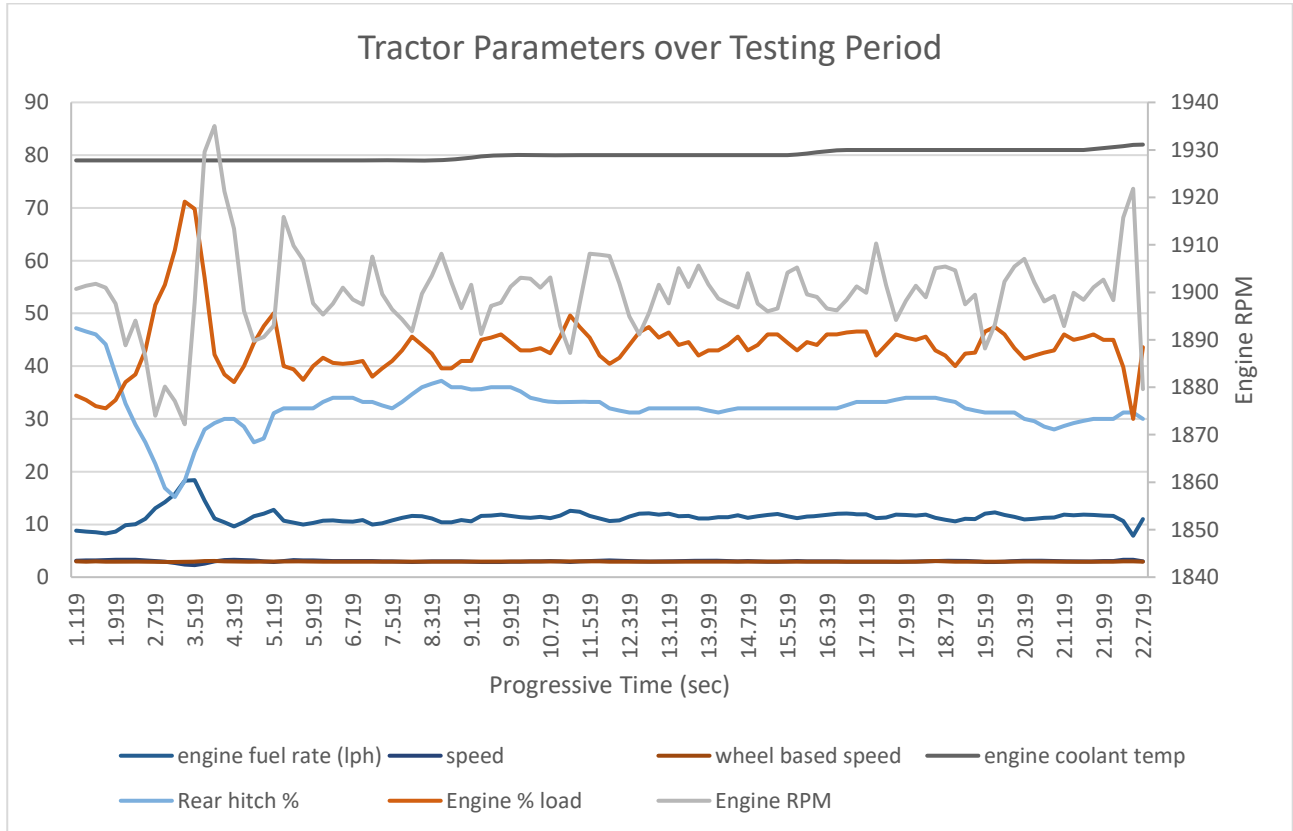
350mm – 5kph – half cut pin

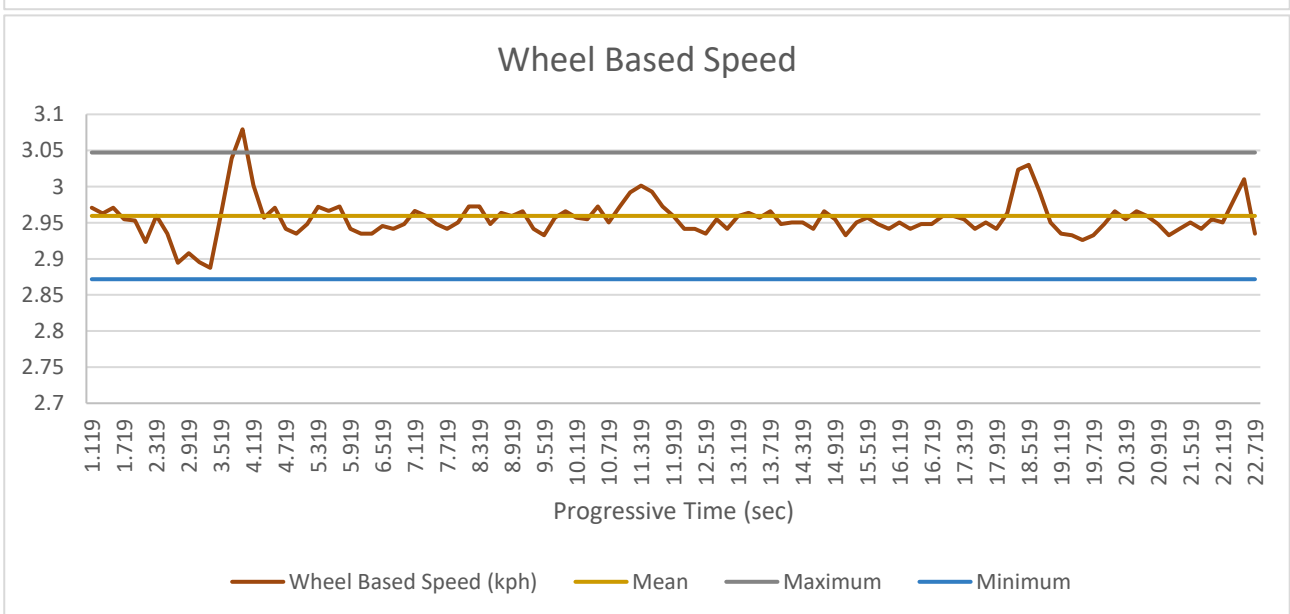
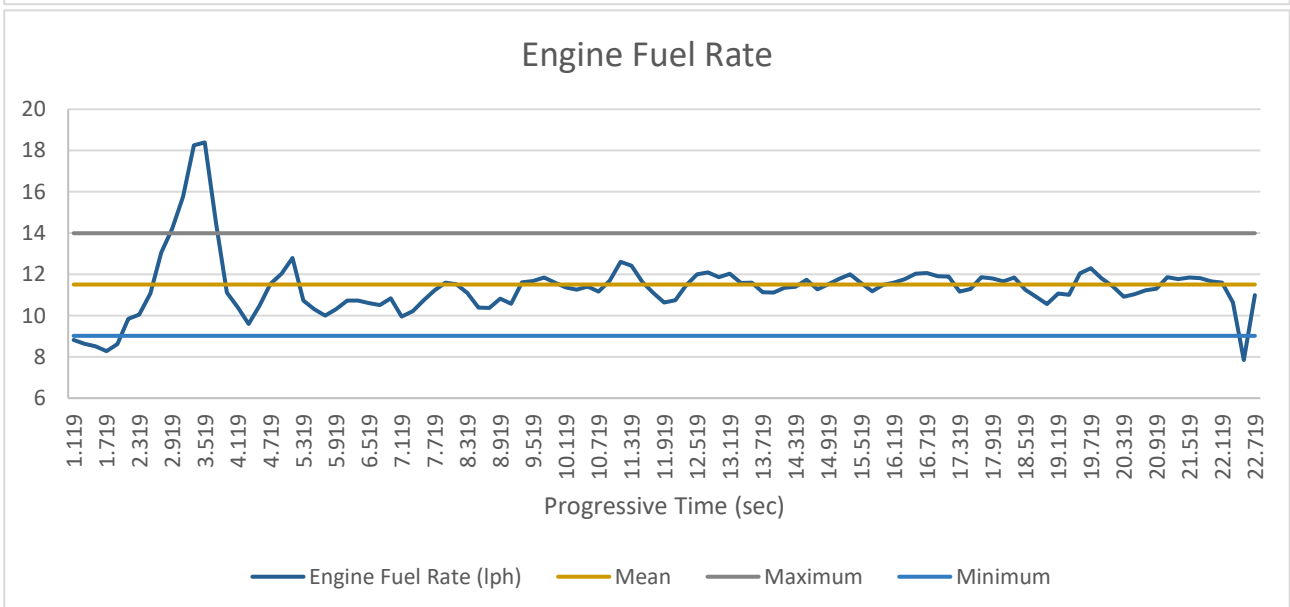
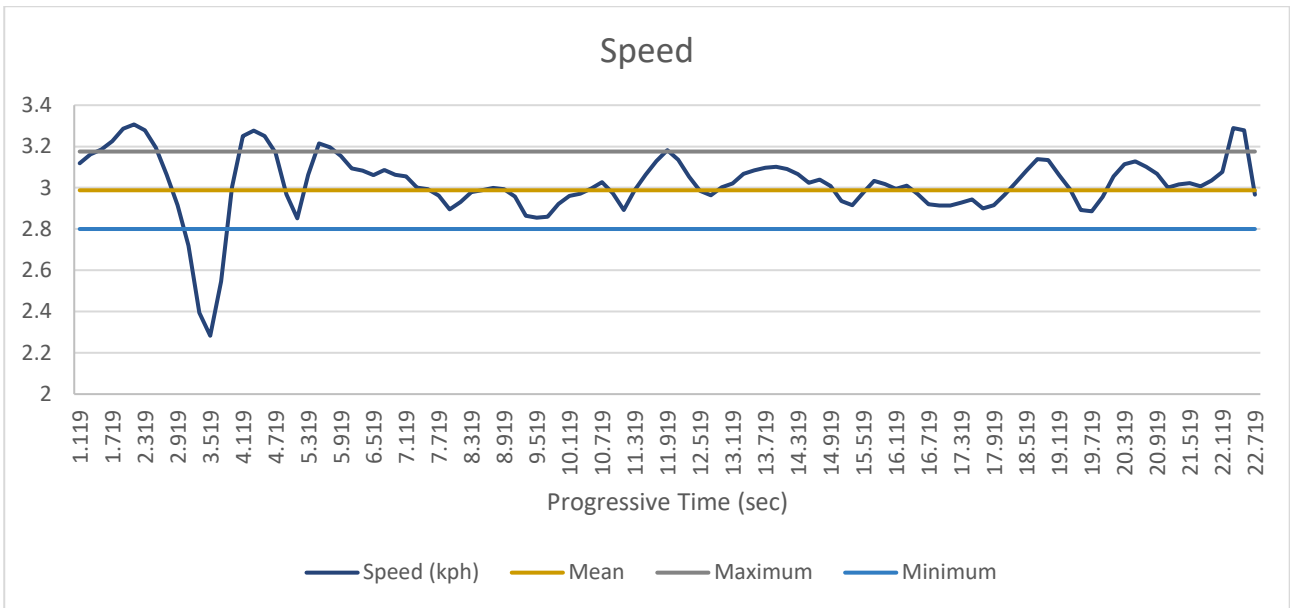


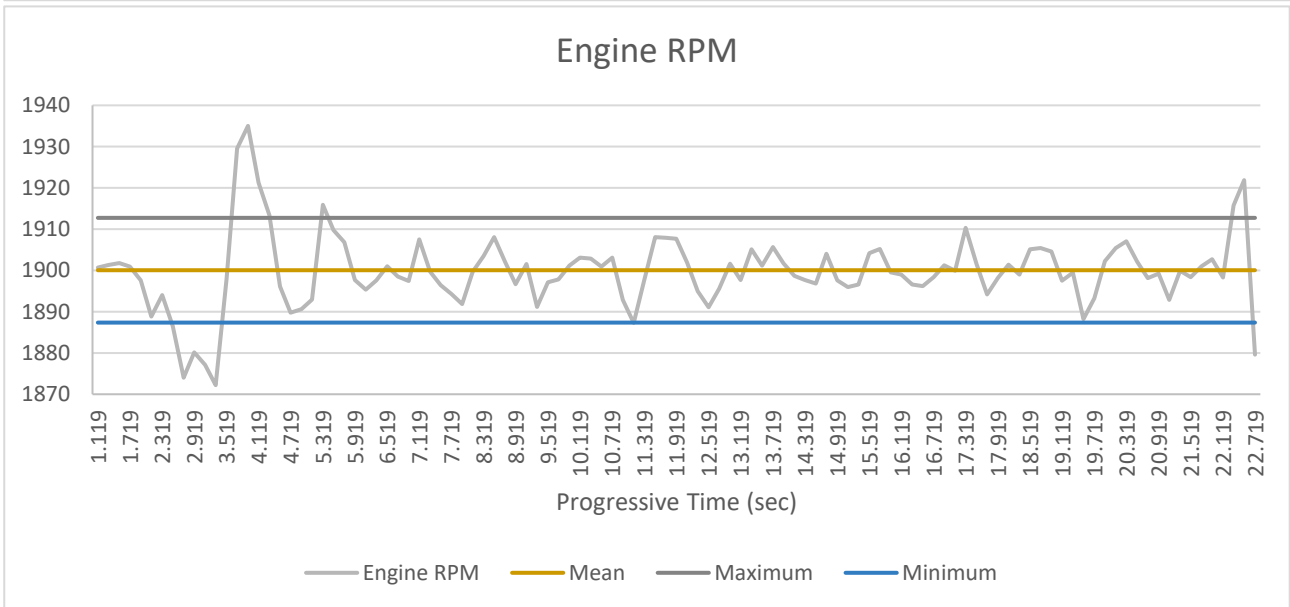
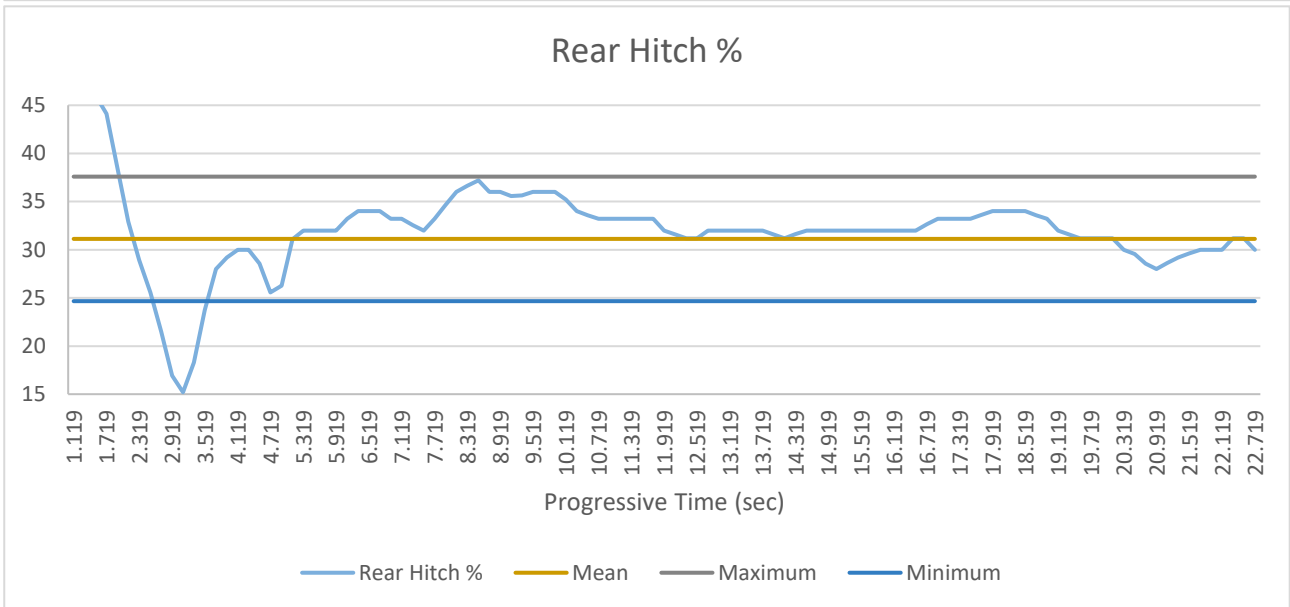
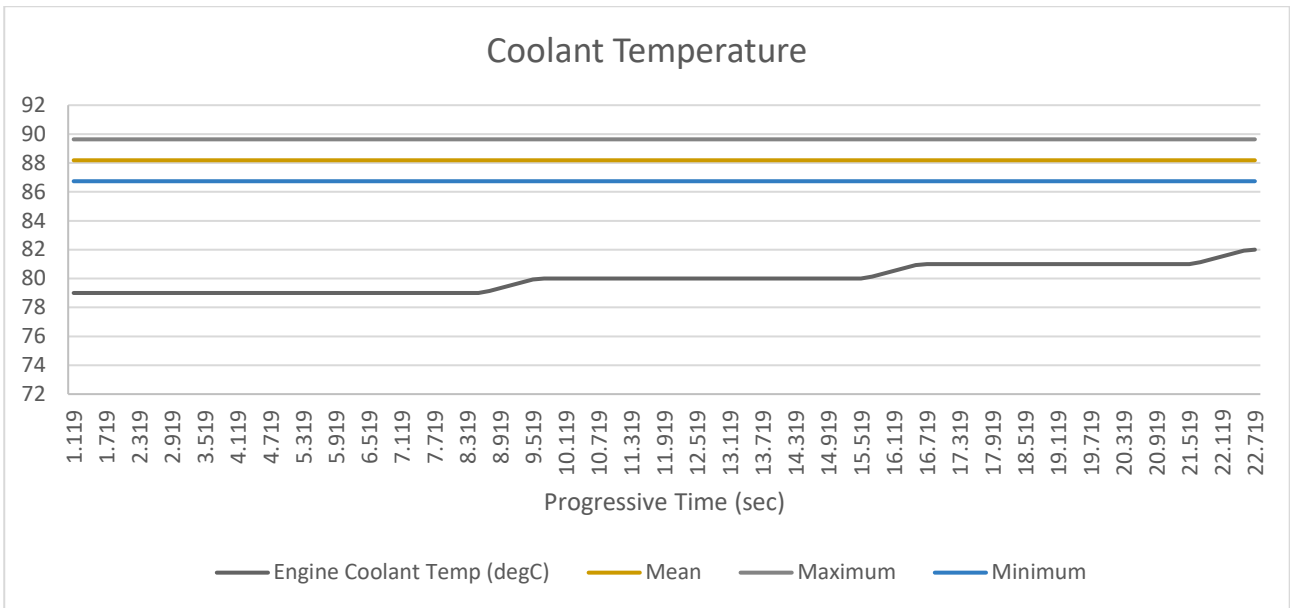




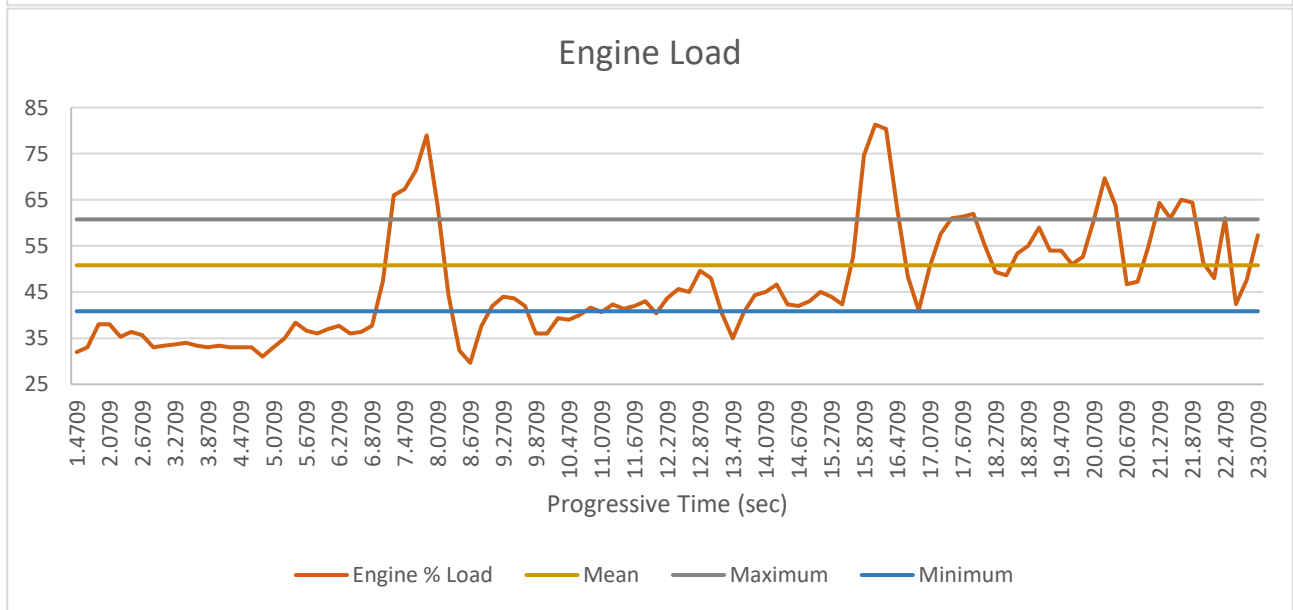
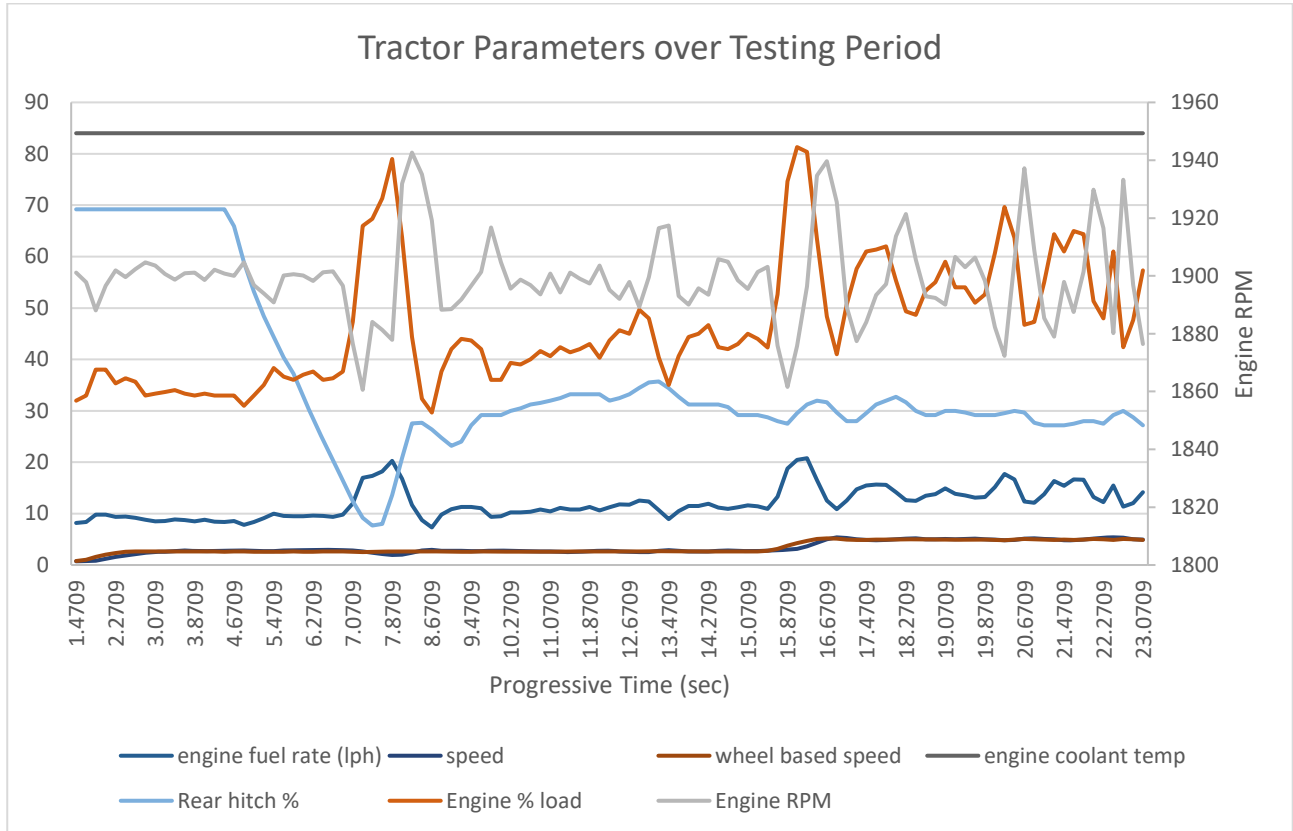
300mm – 3kph

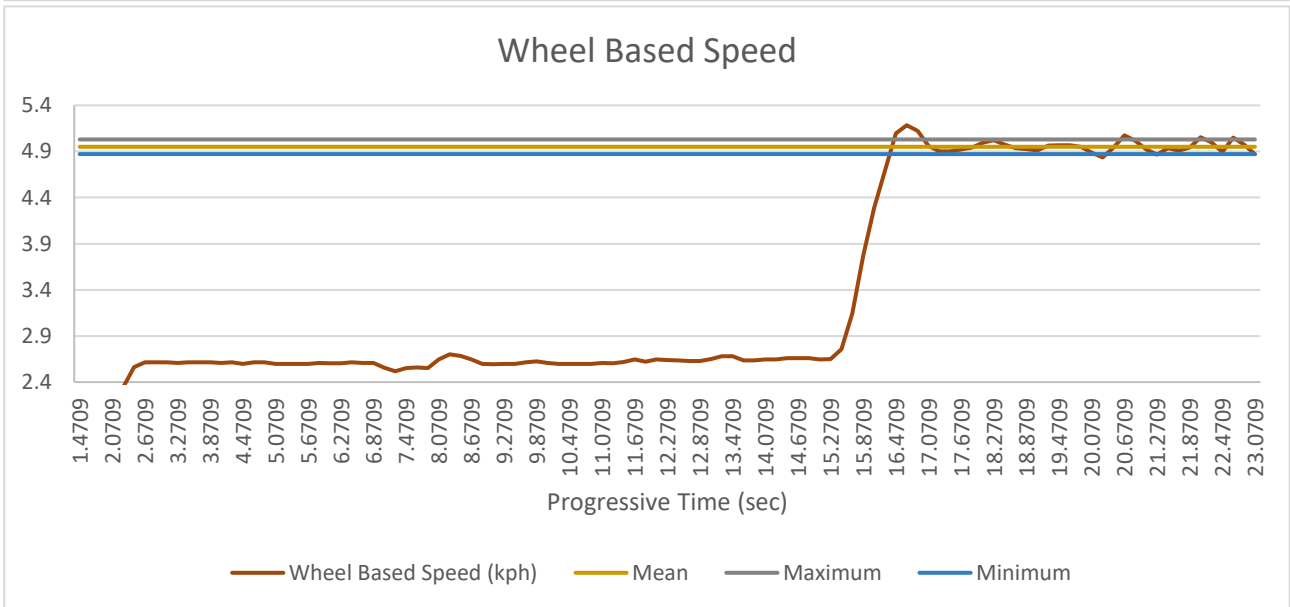
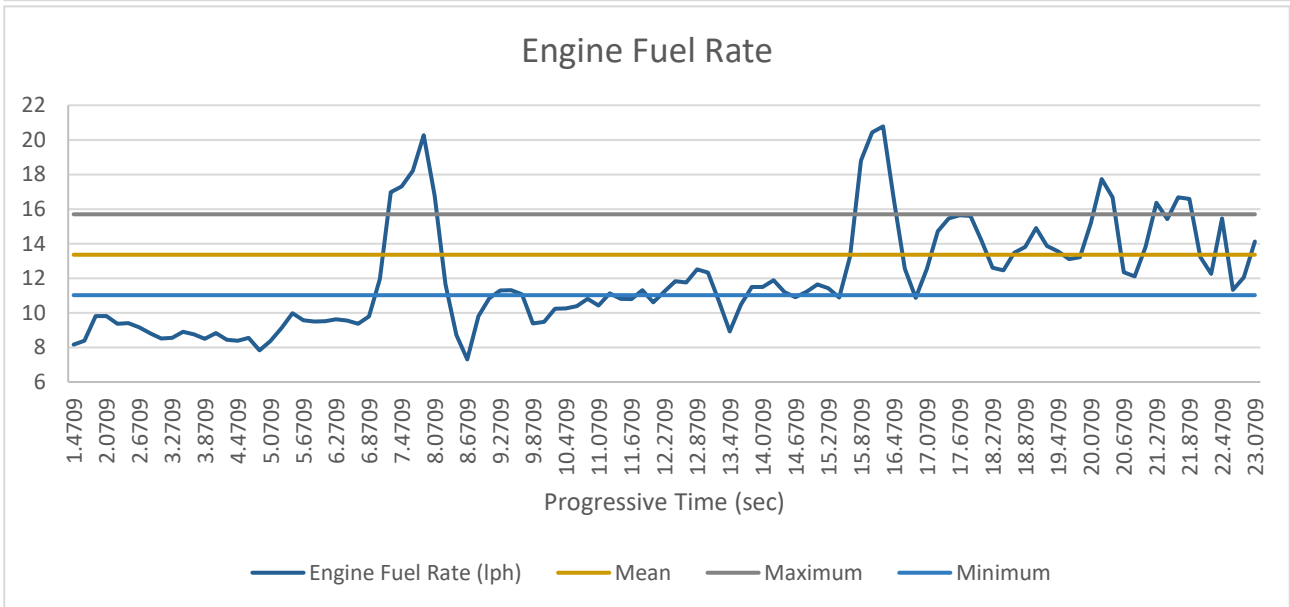
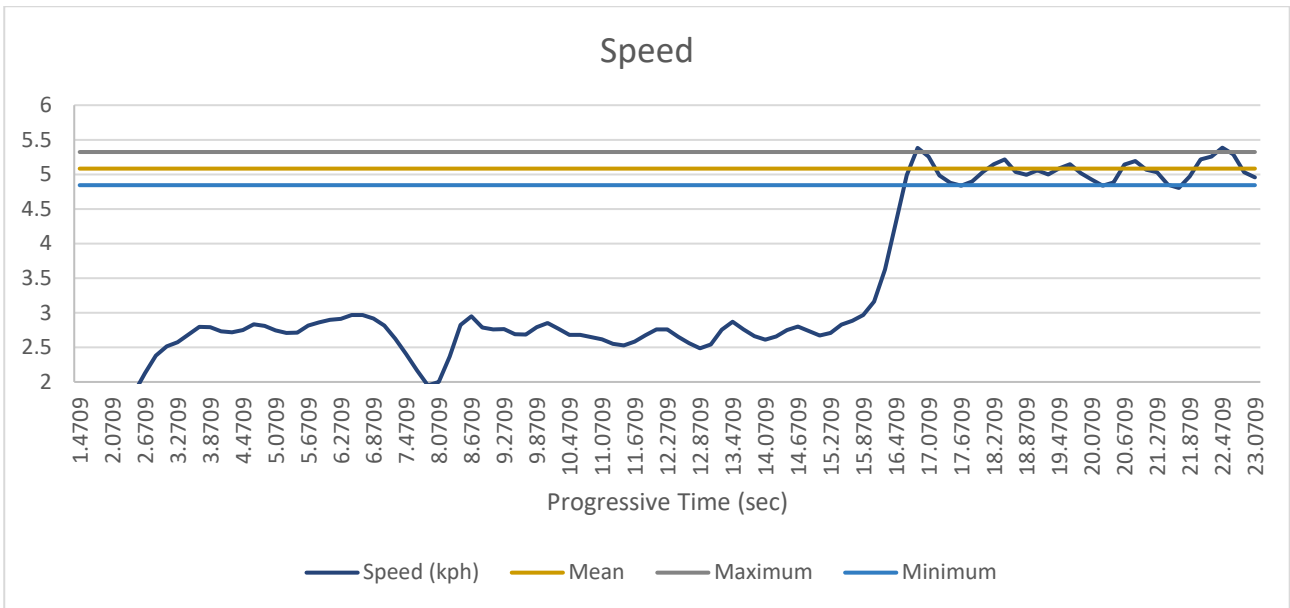


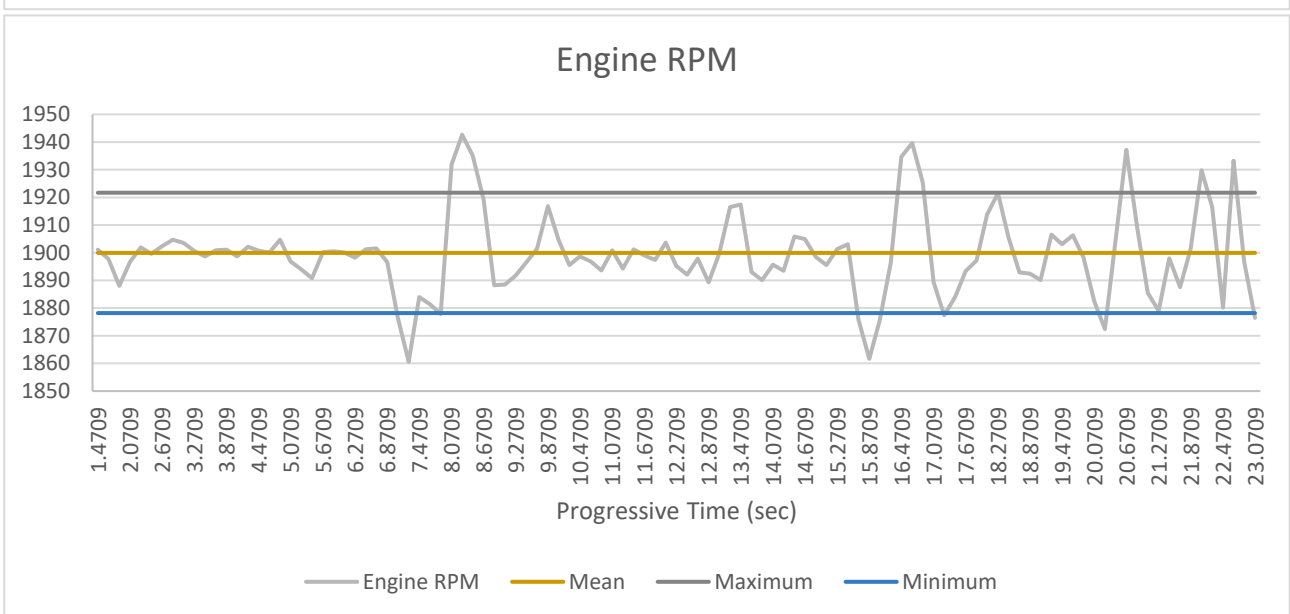
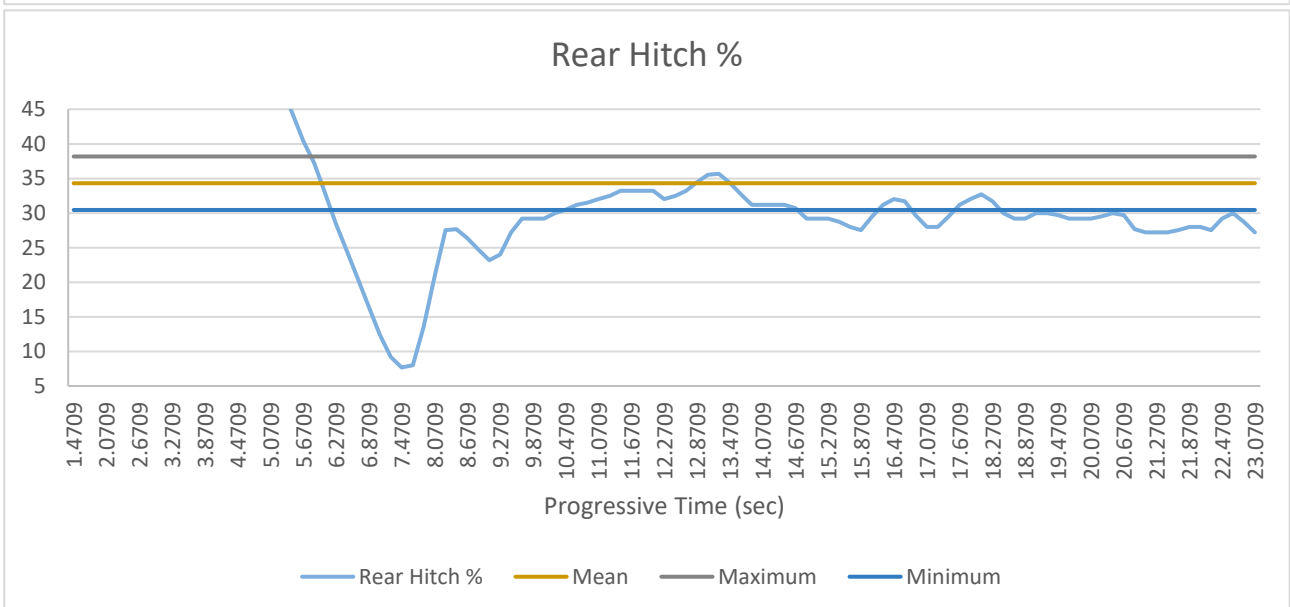
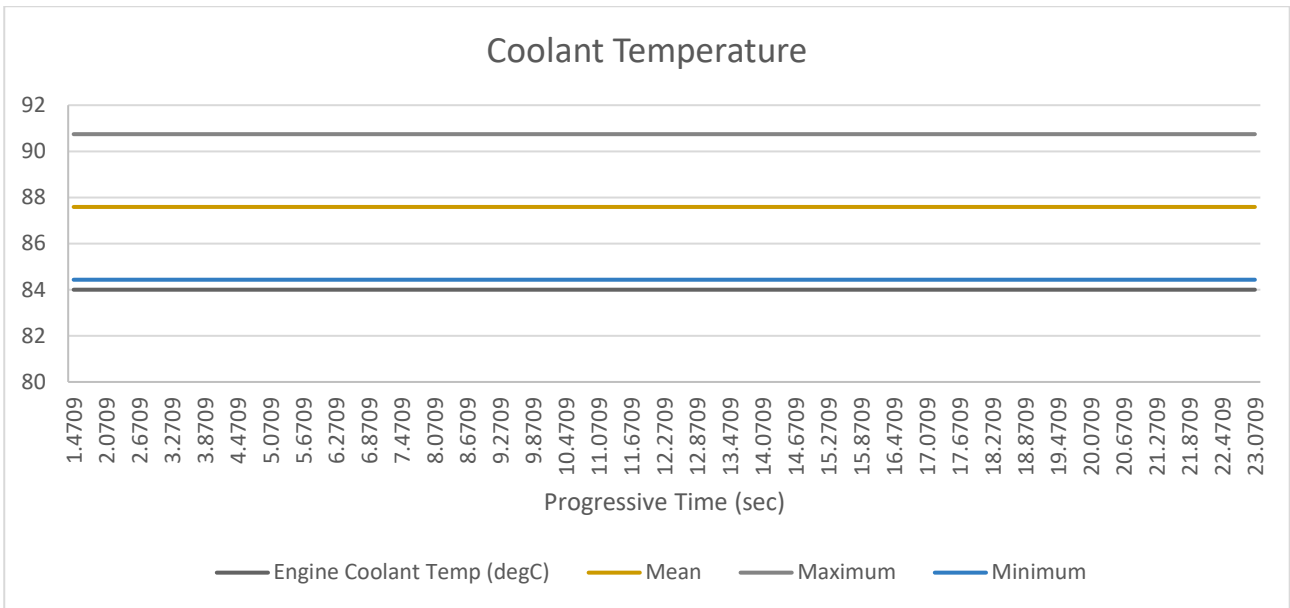




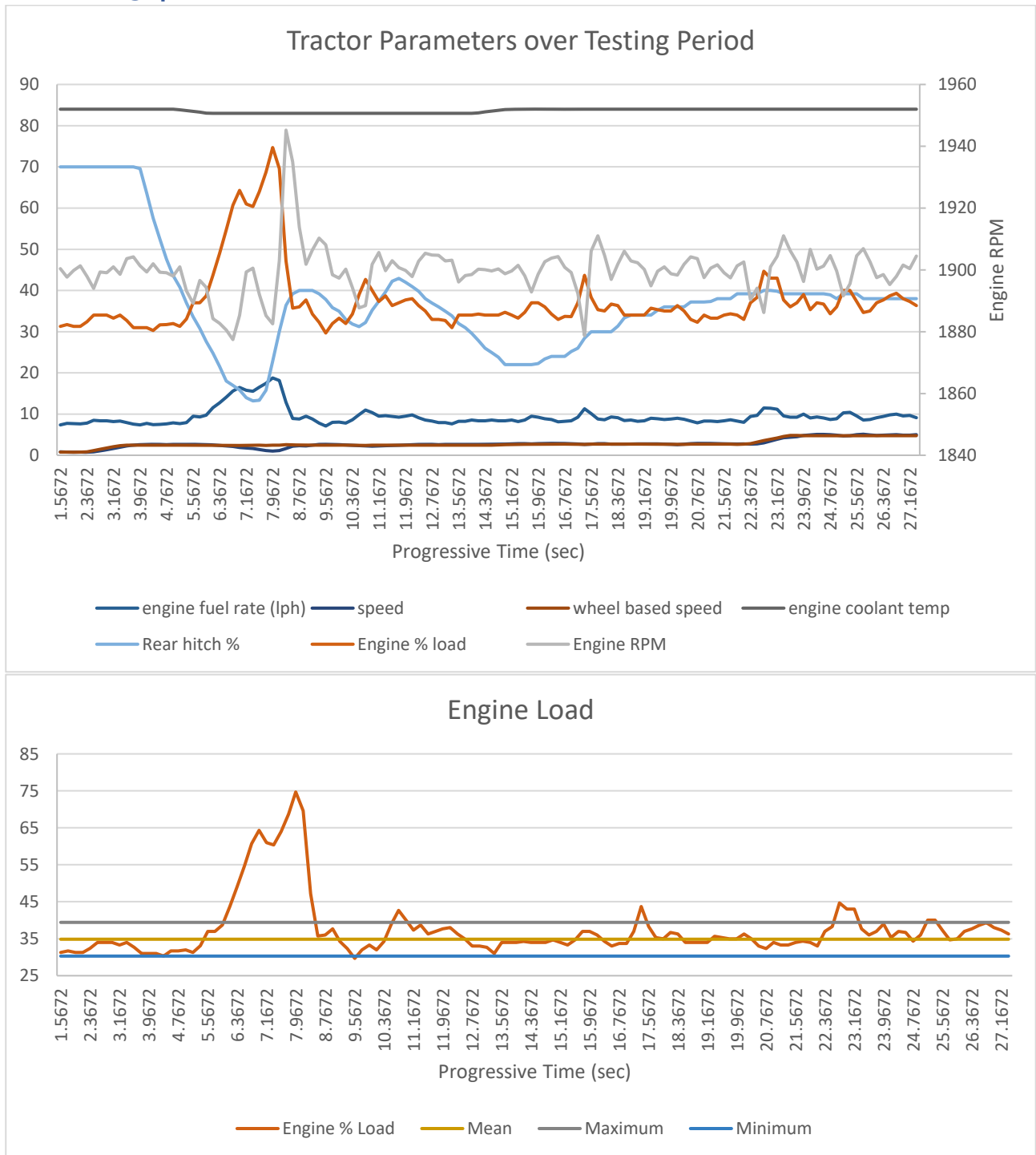
300mm – 5kph

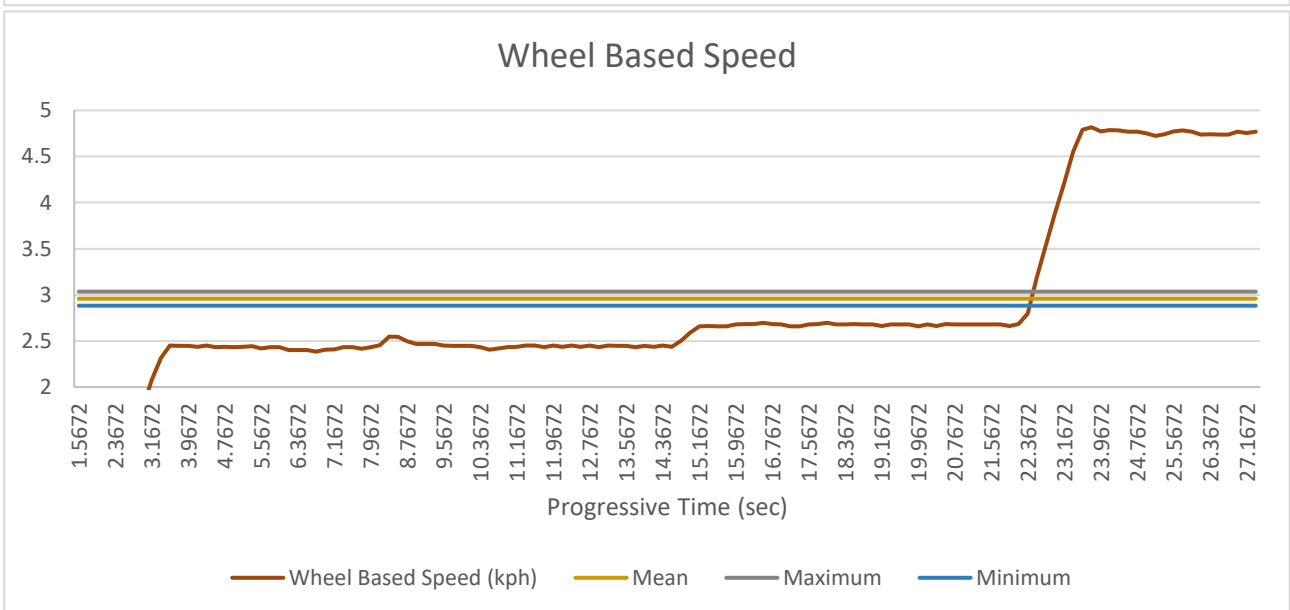
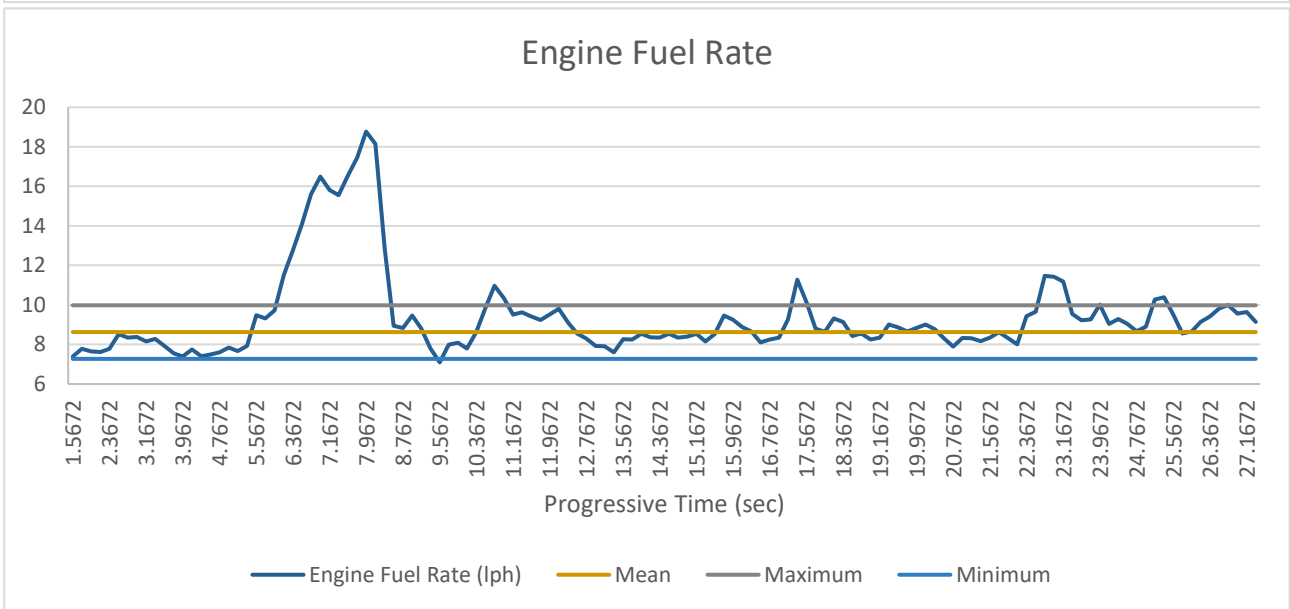
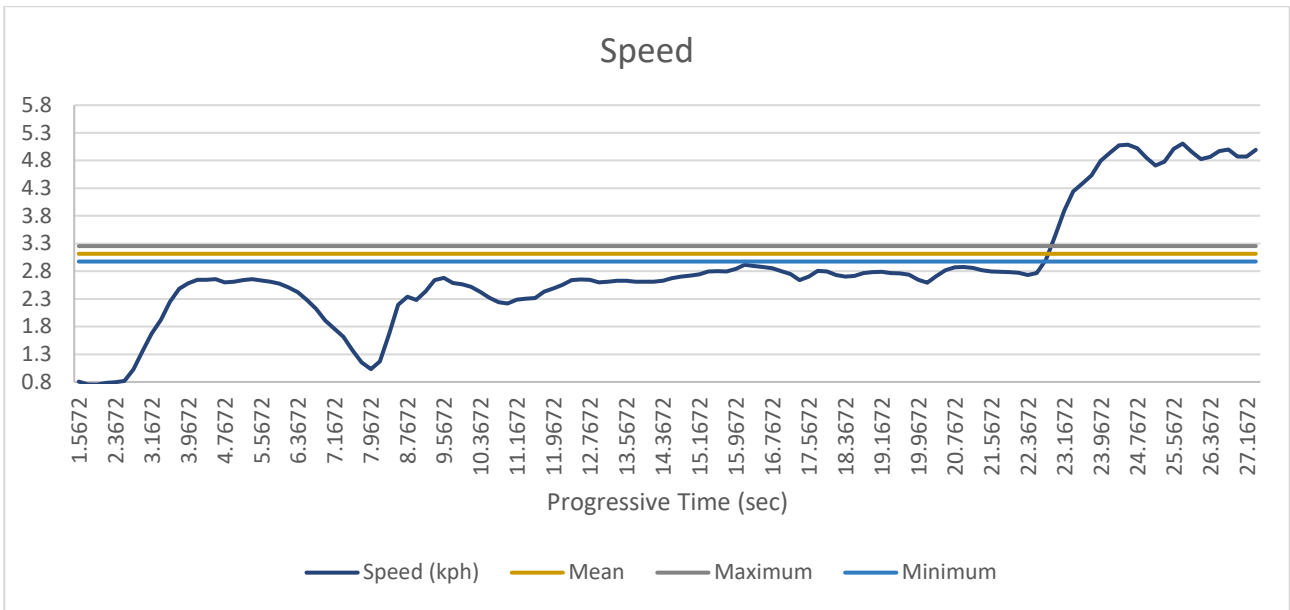


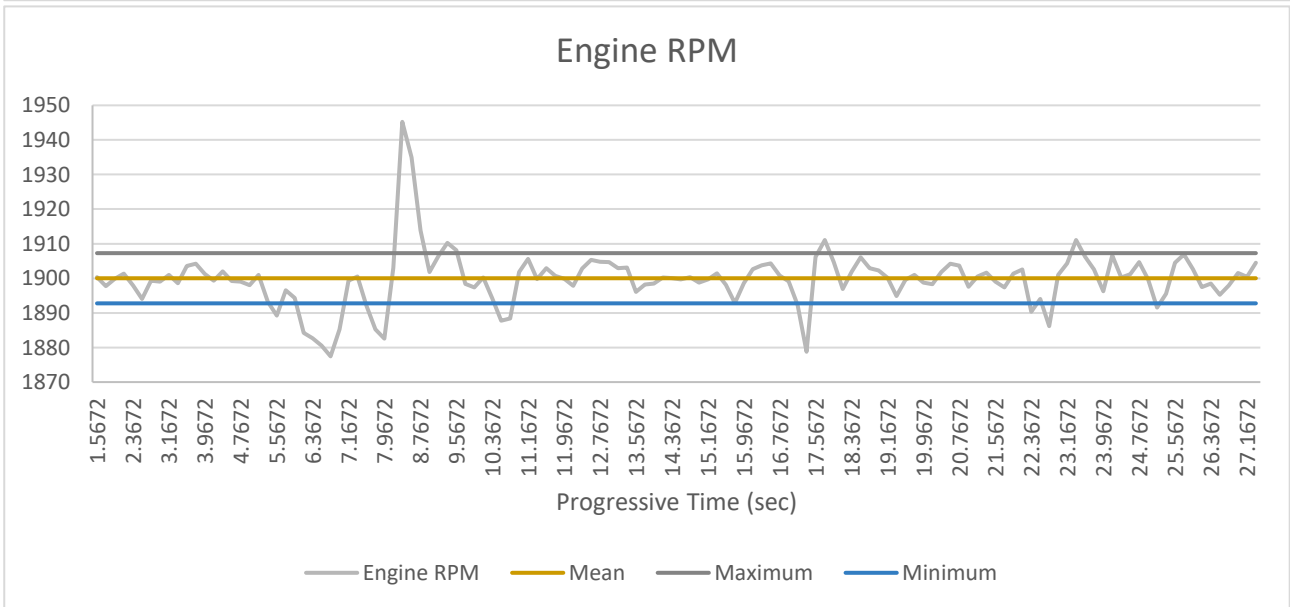
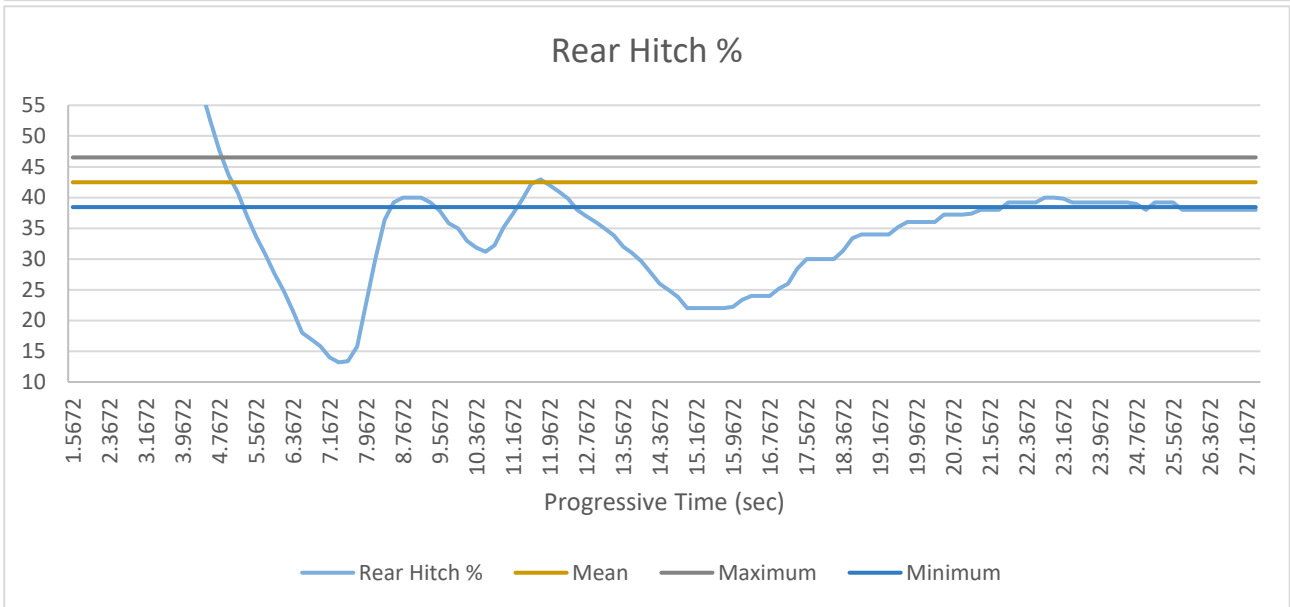
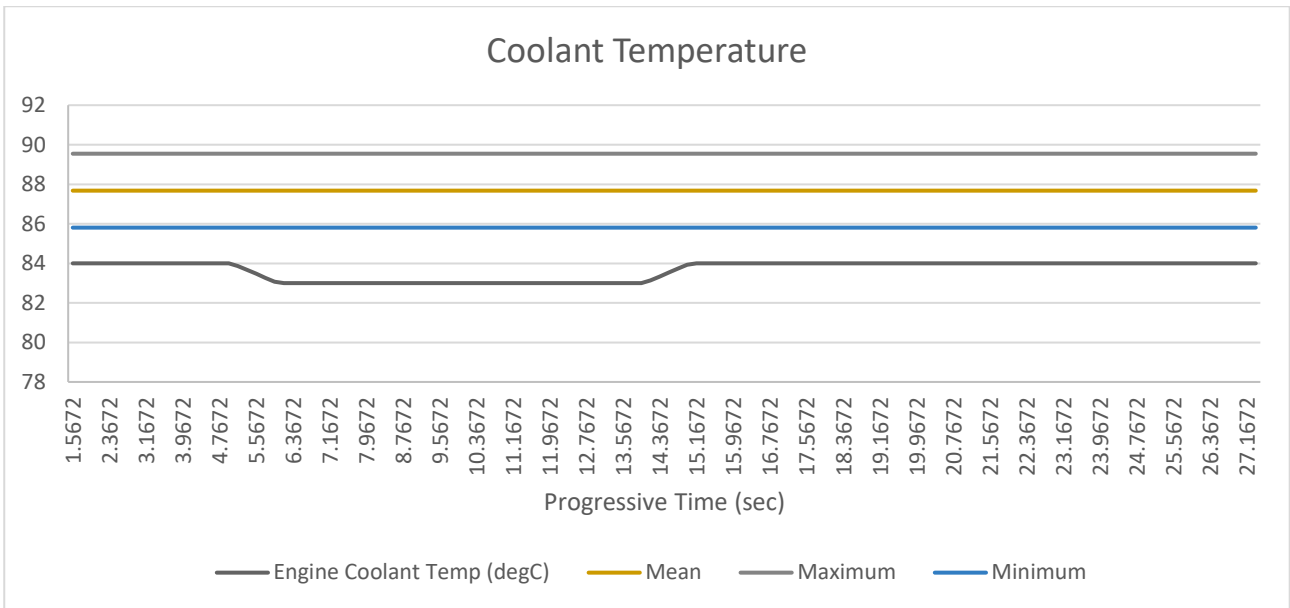




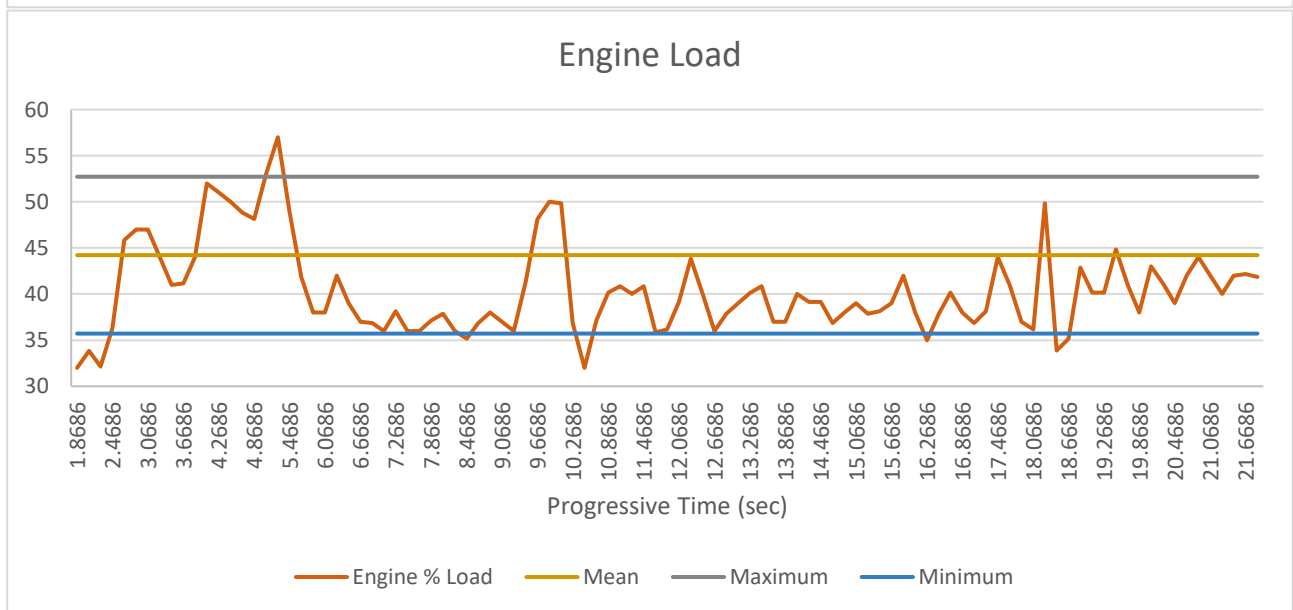
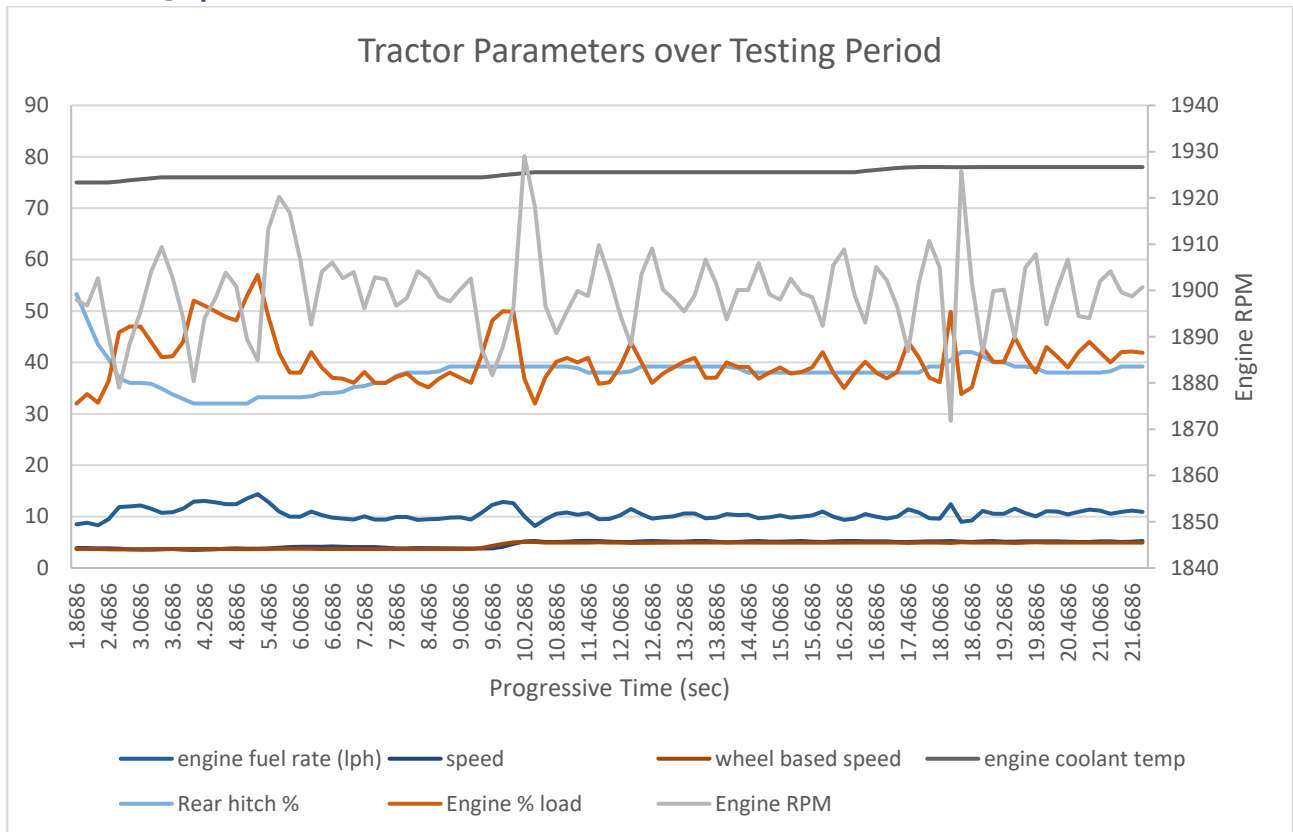
200mm – 3kph

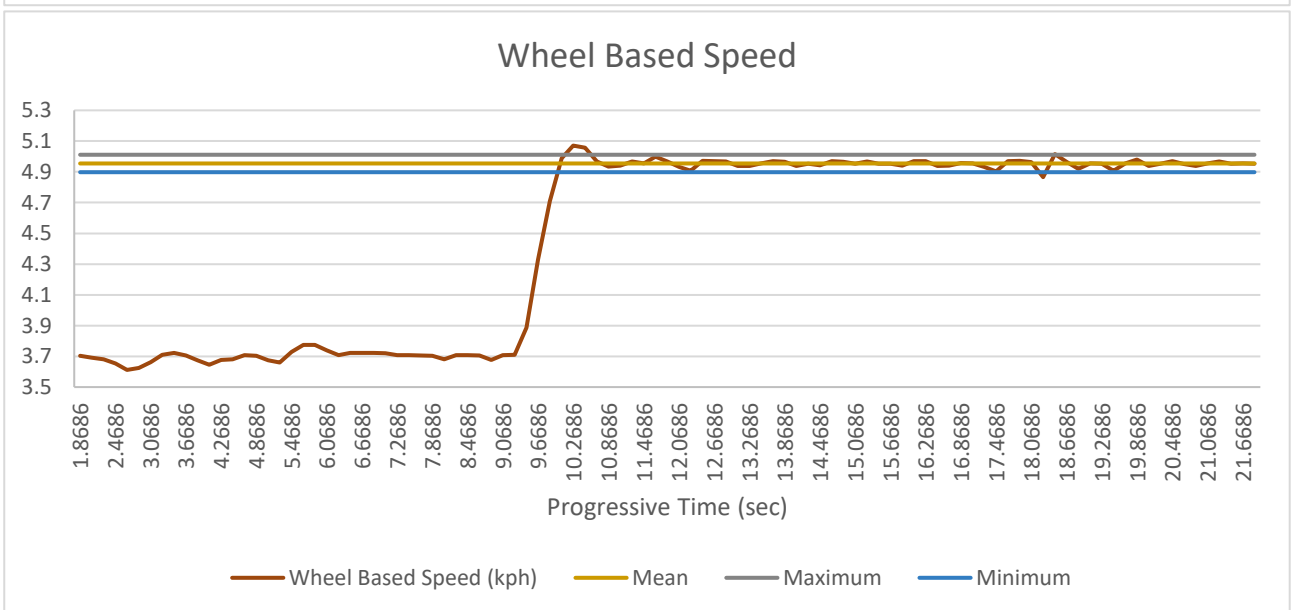
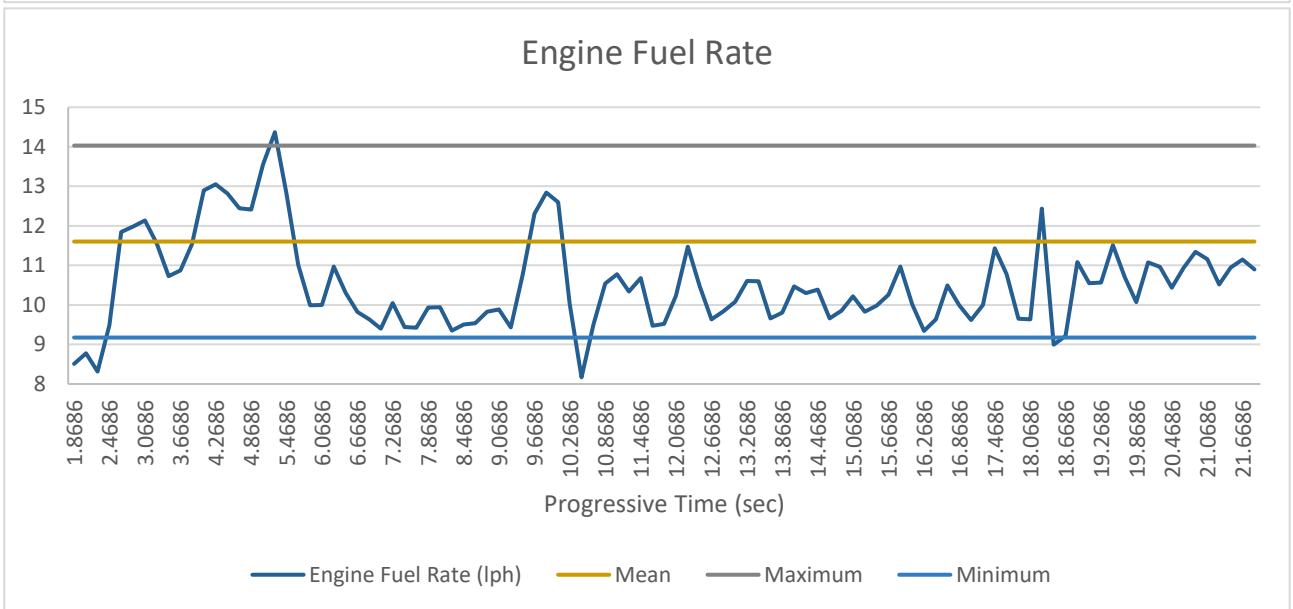
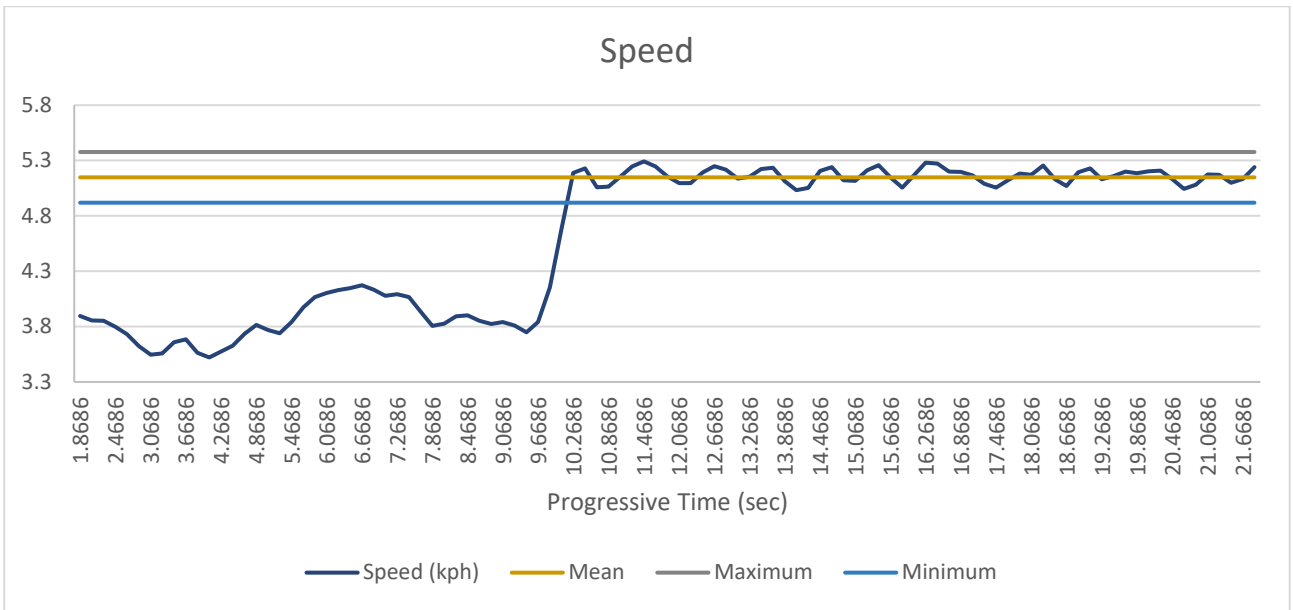


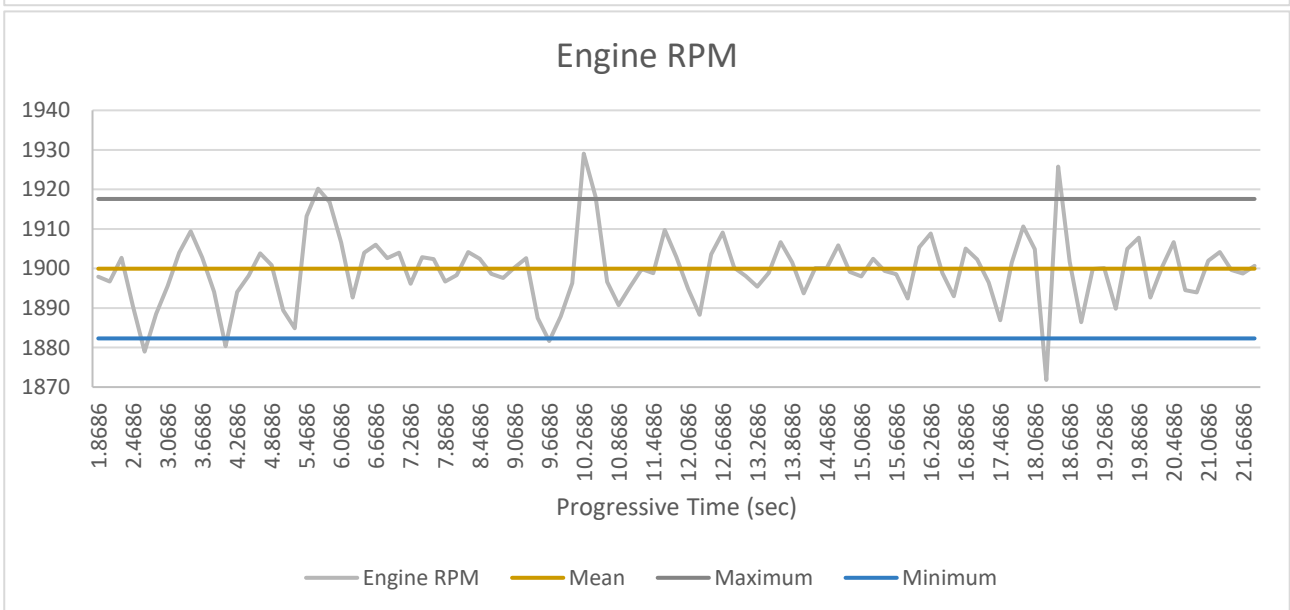
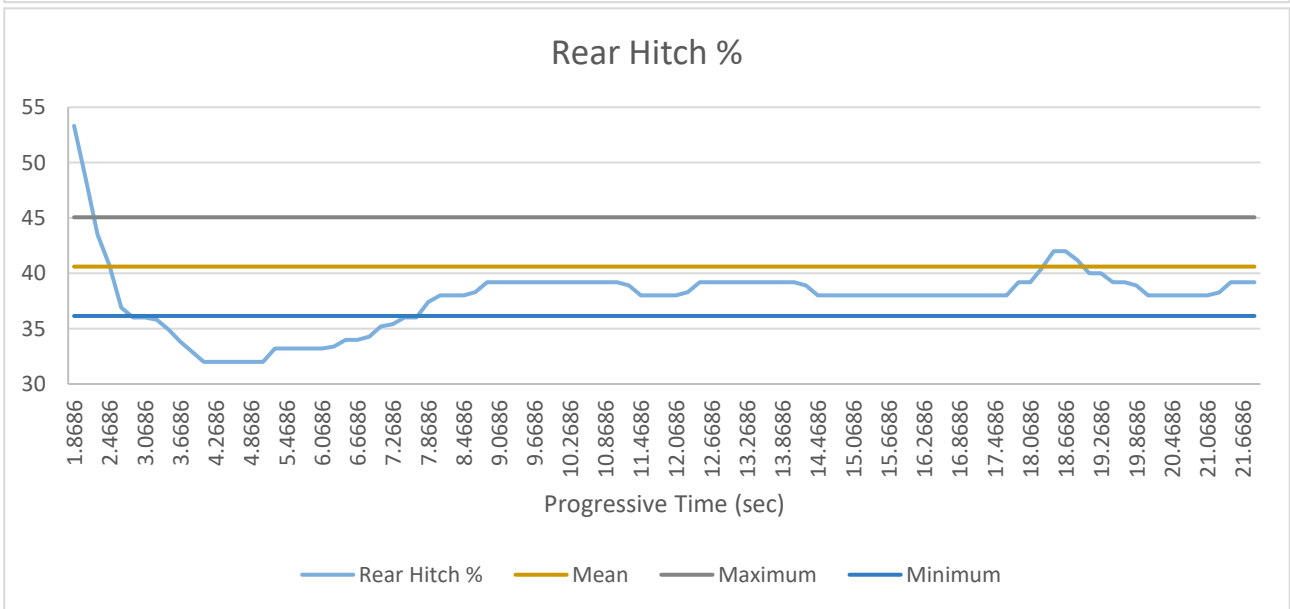
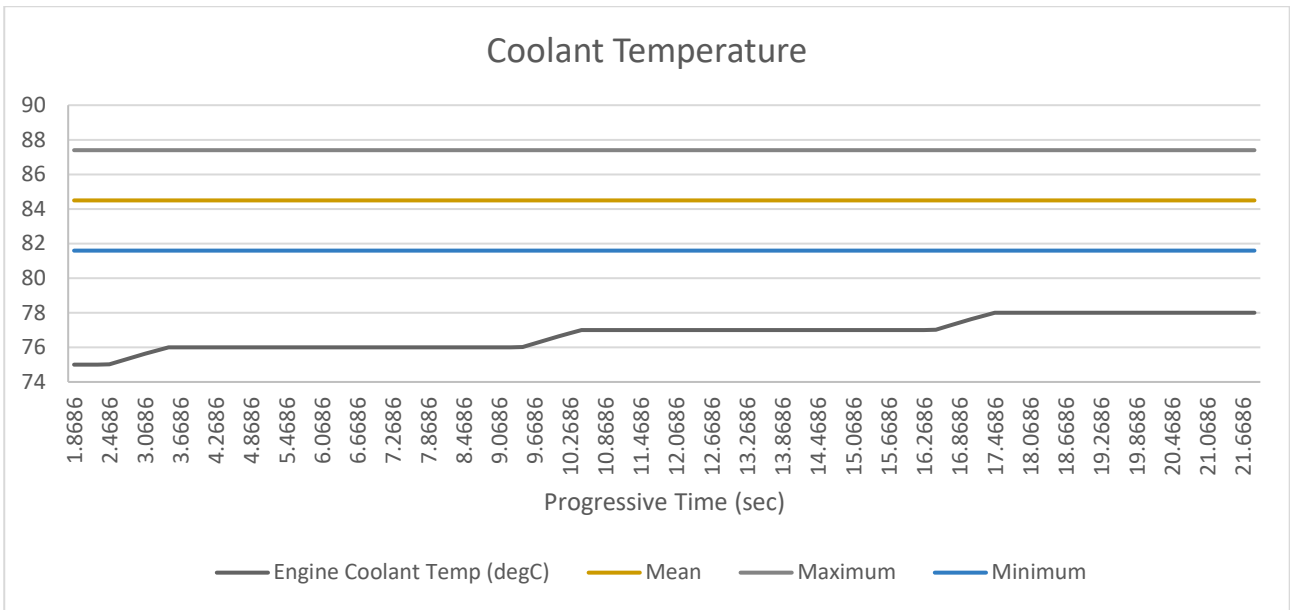




200mm – 5kph

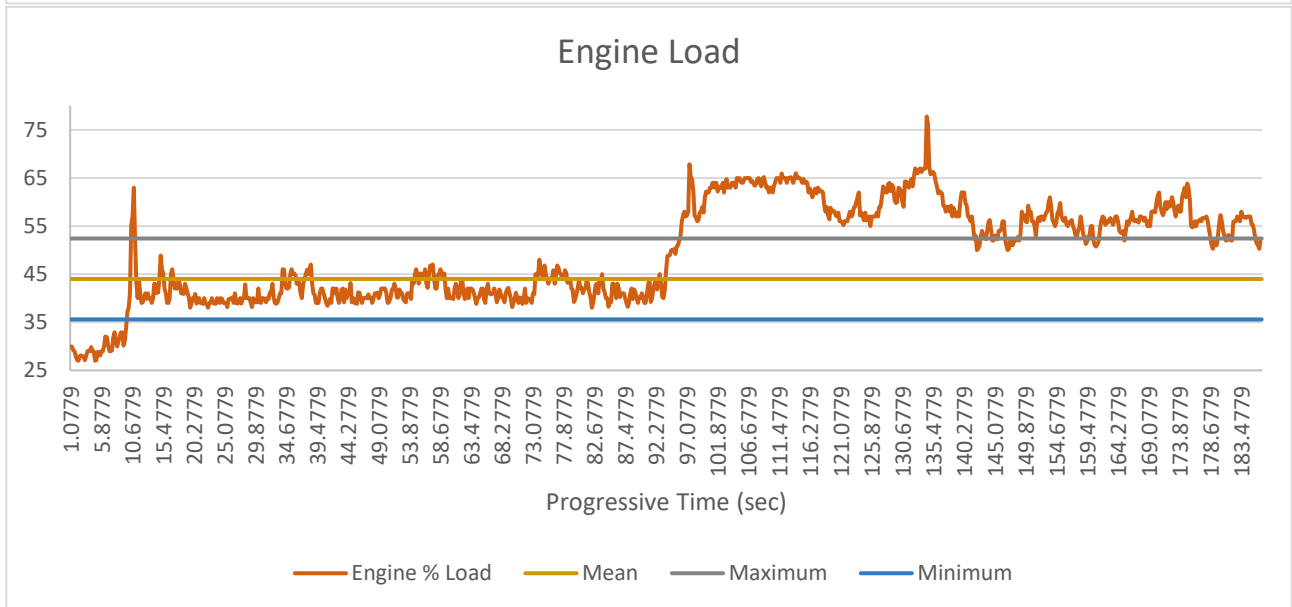
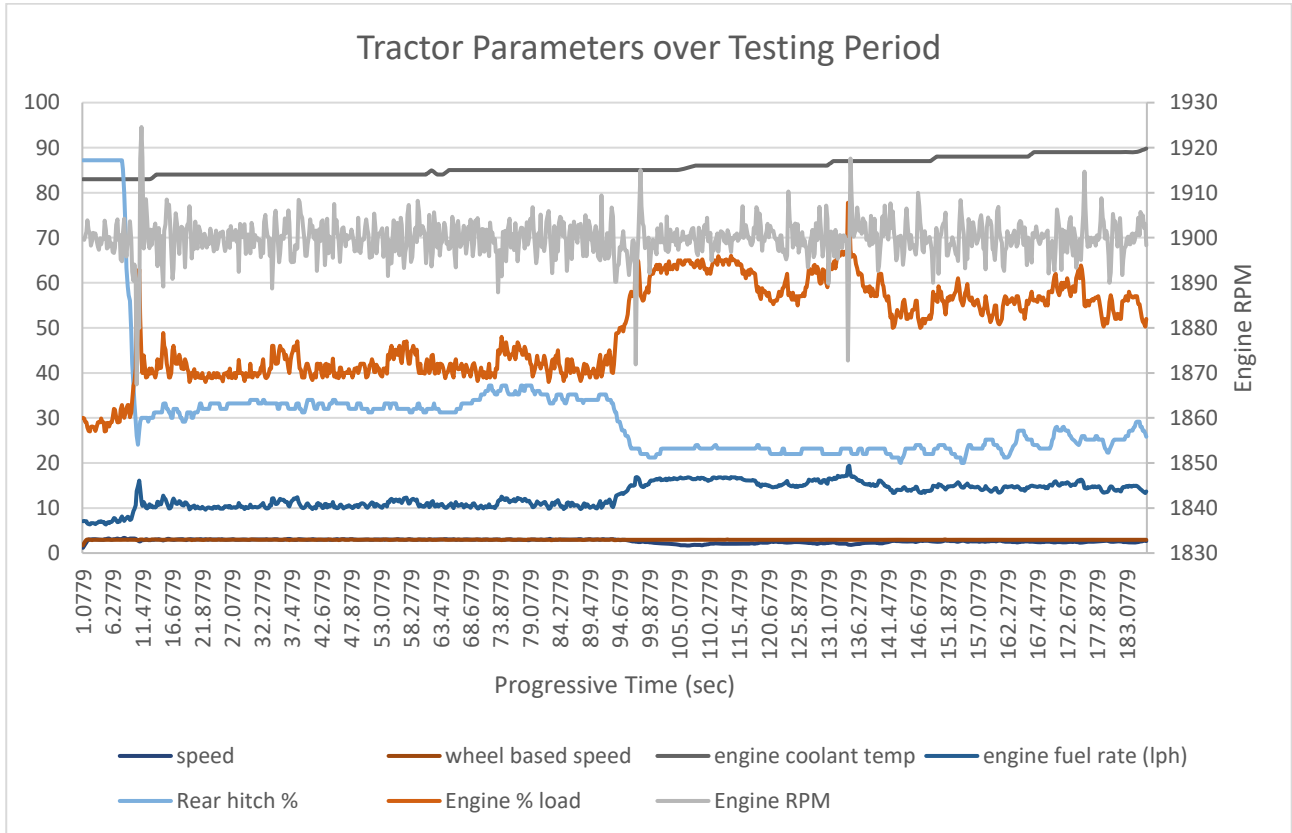


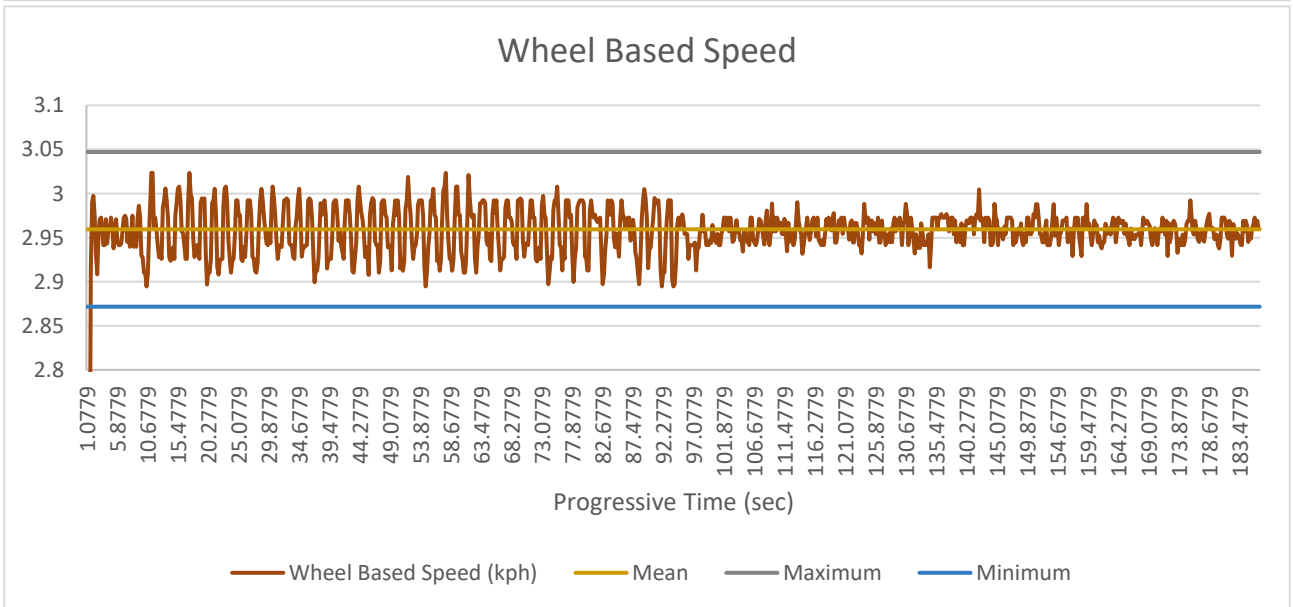
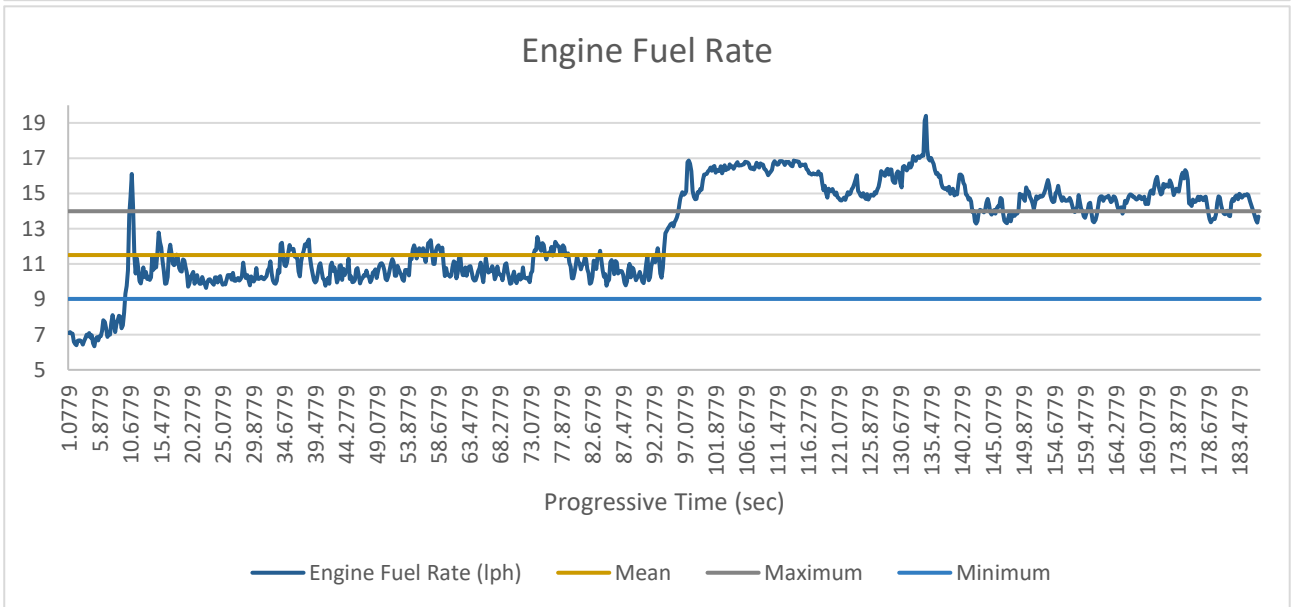
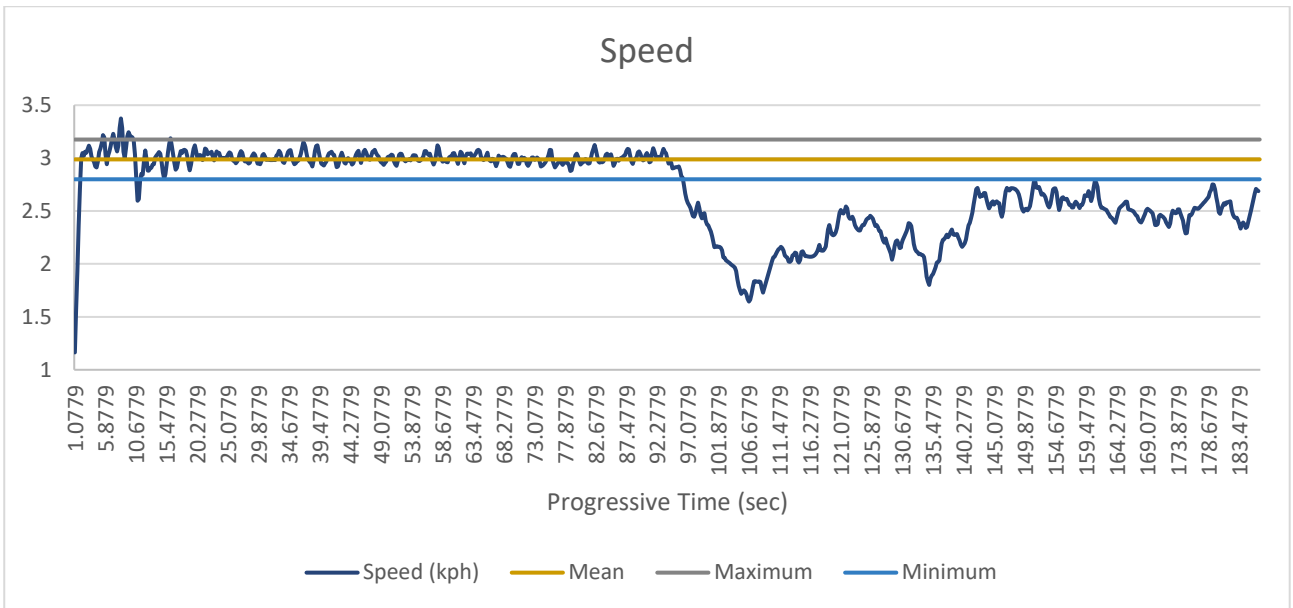


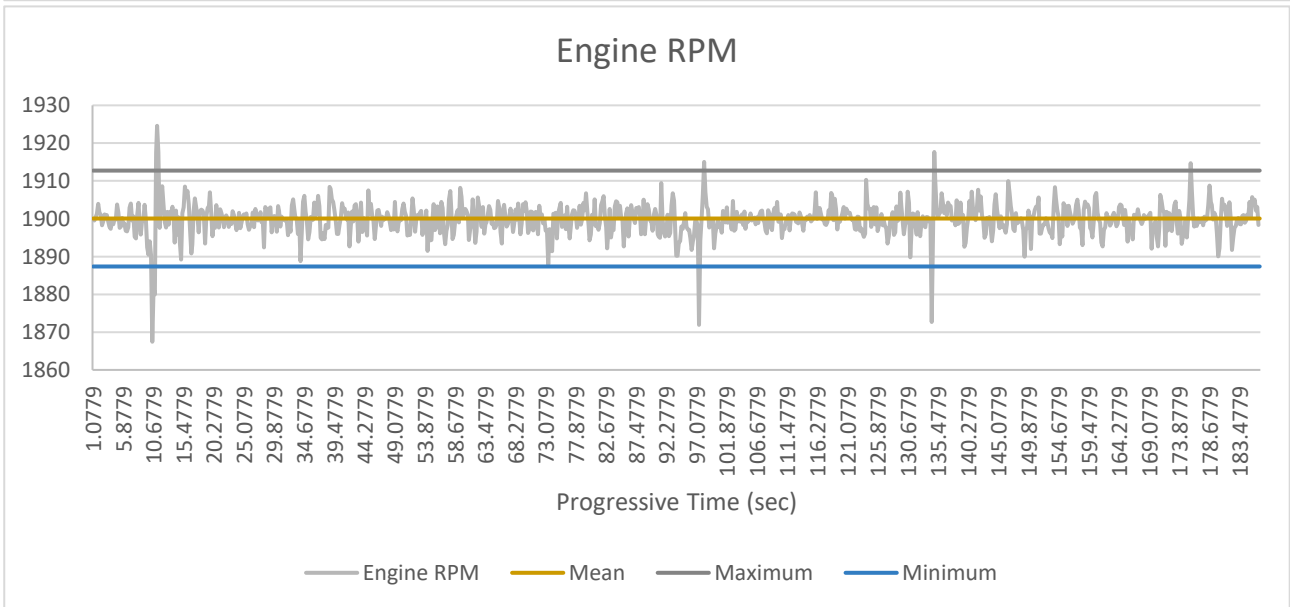
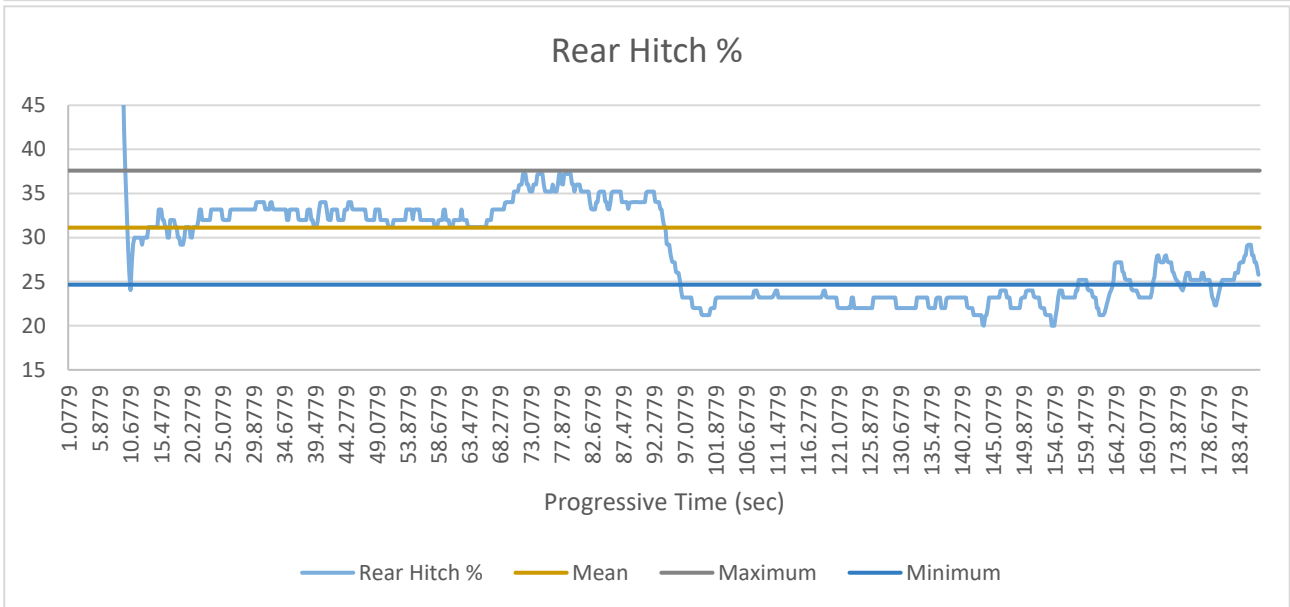
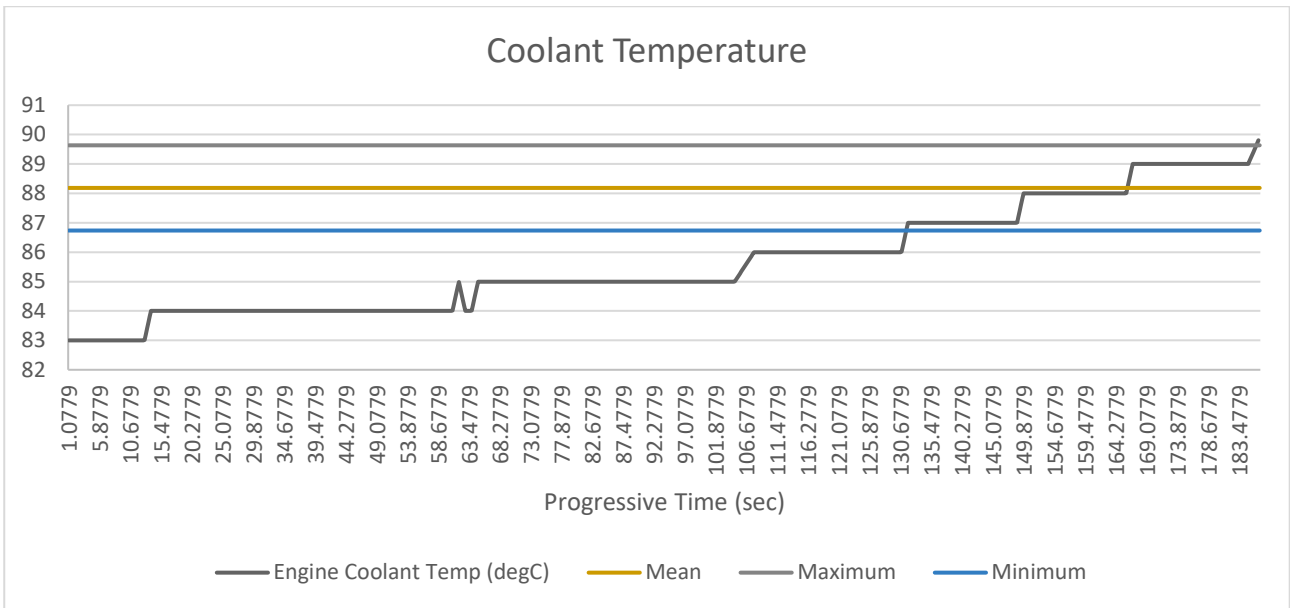


Appendix H – 3PL Deep Ripper – Ripper digging in too far data

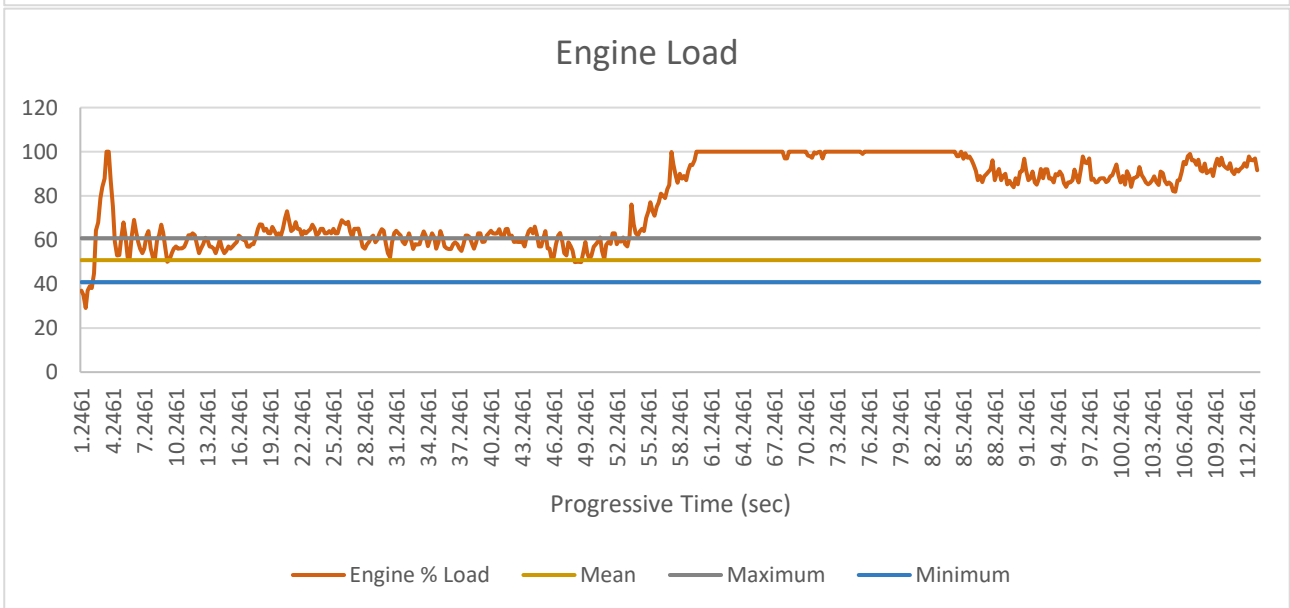
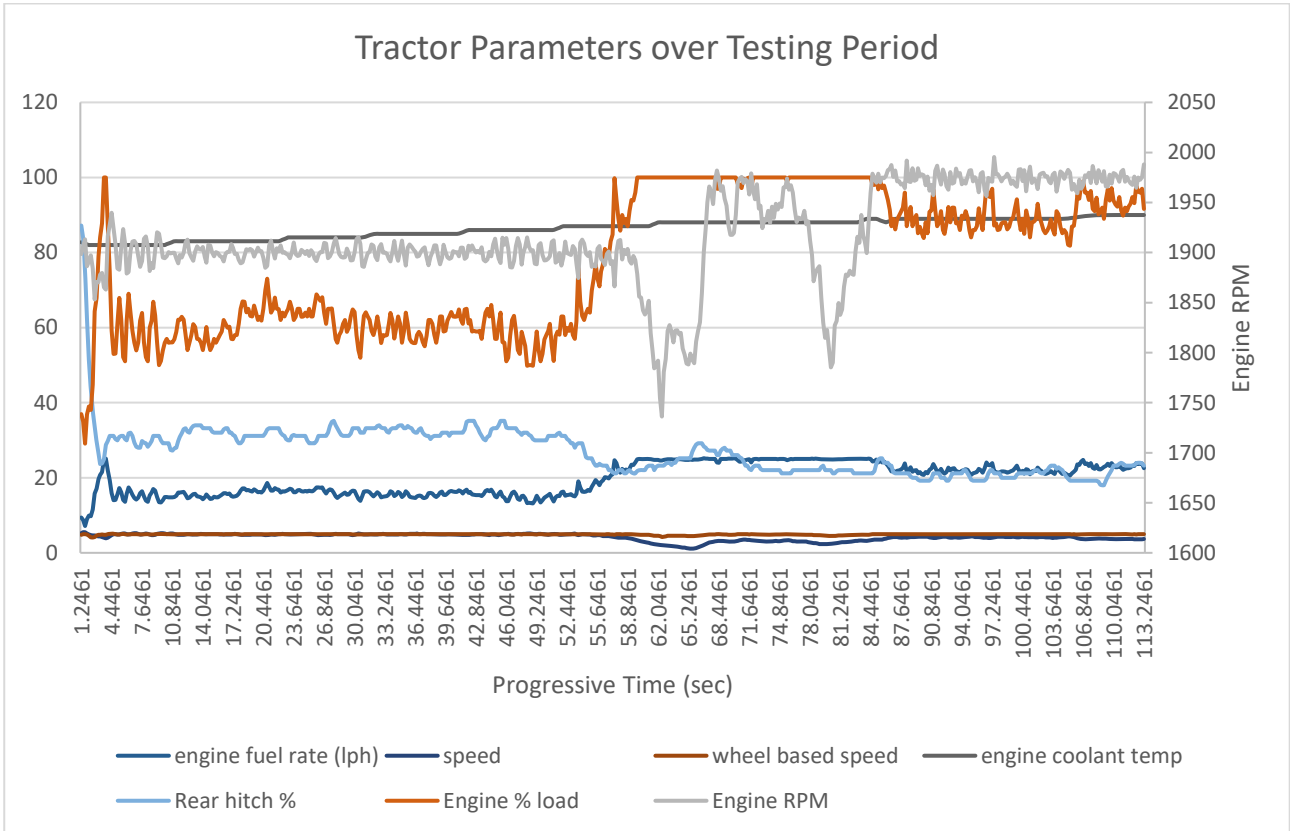
300mm – 3kph

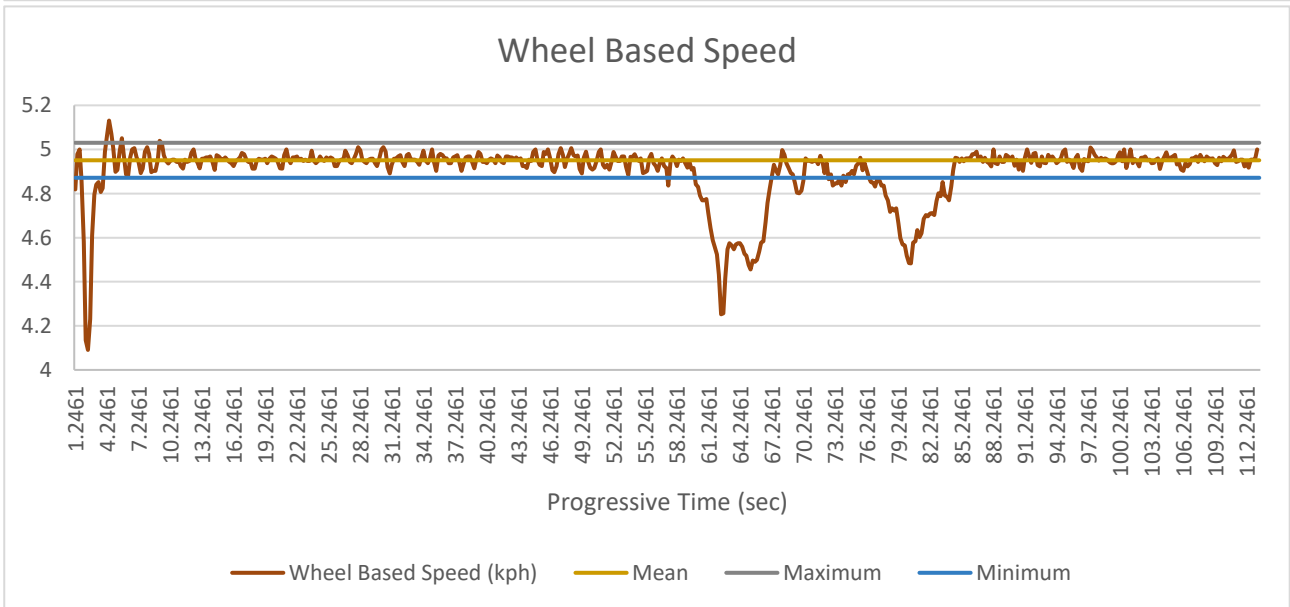
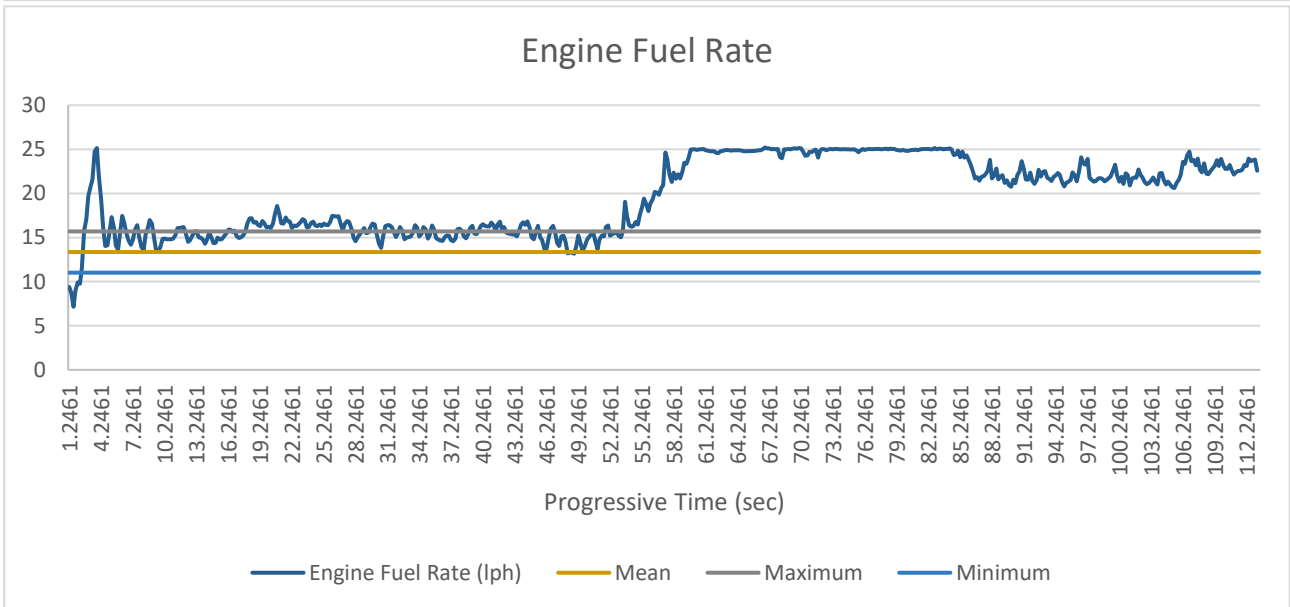
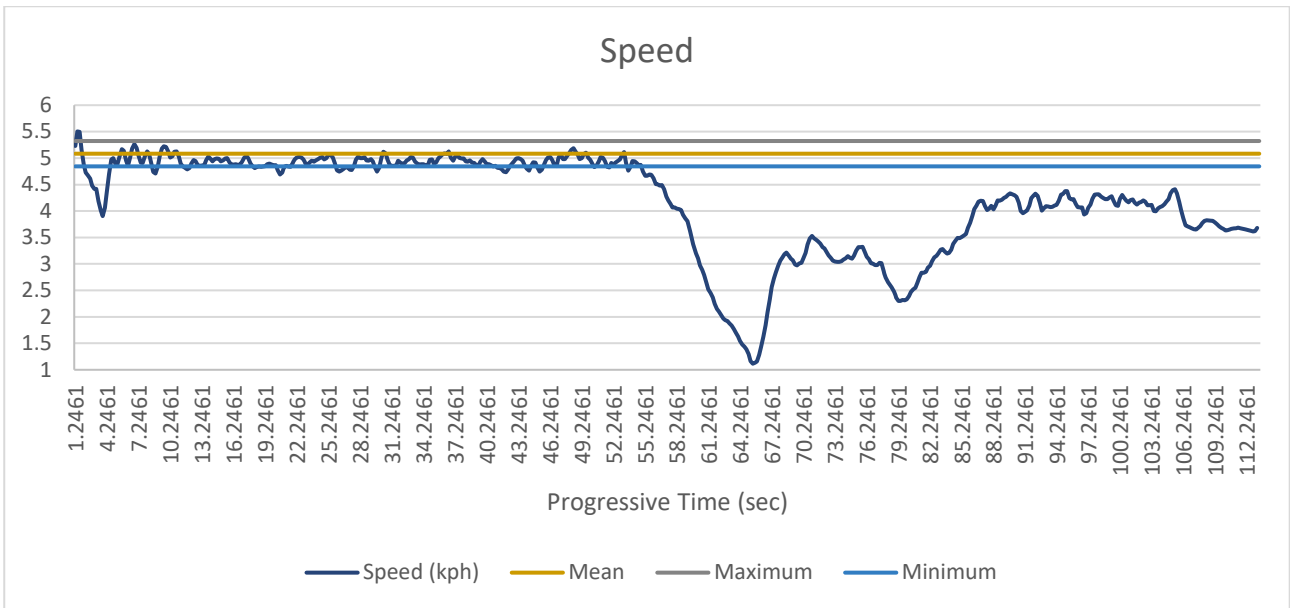


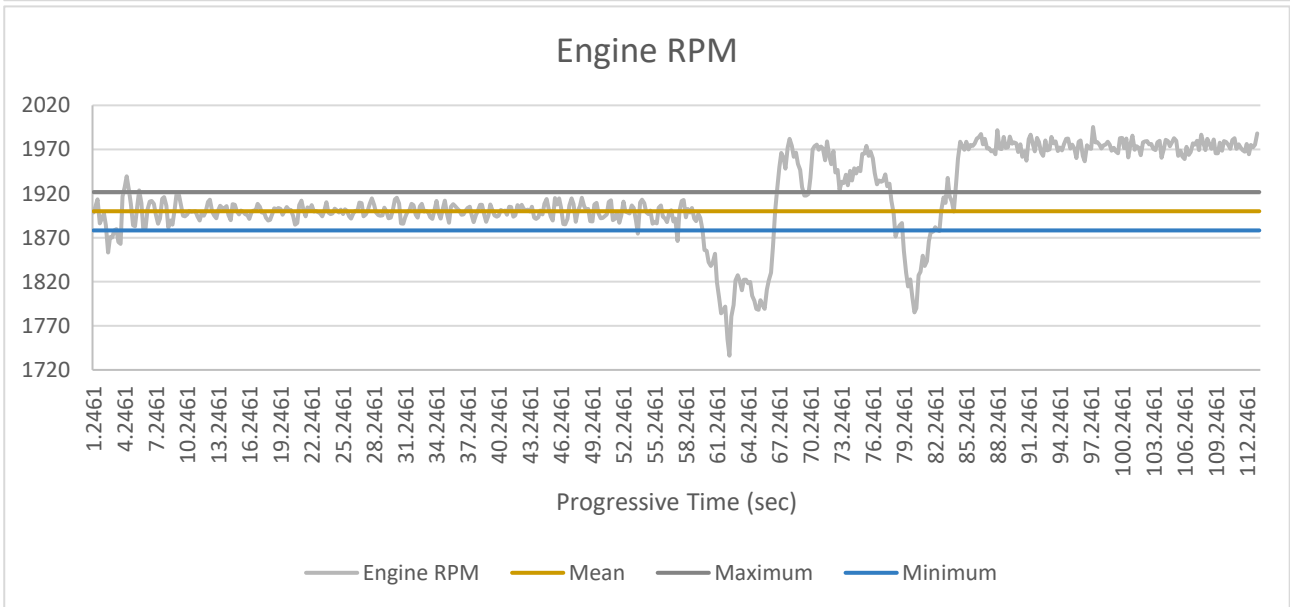
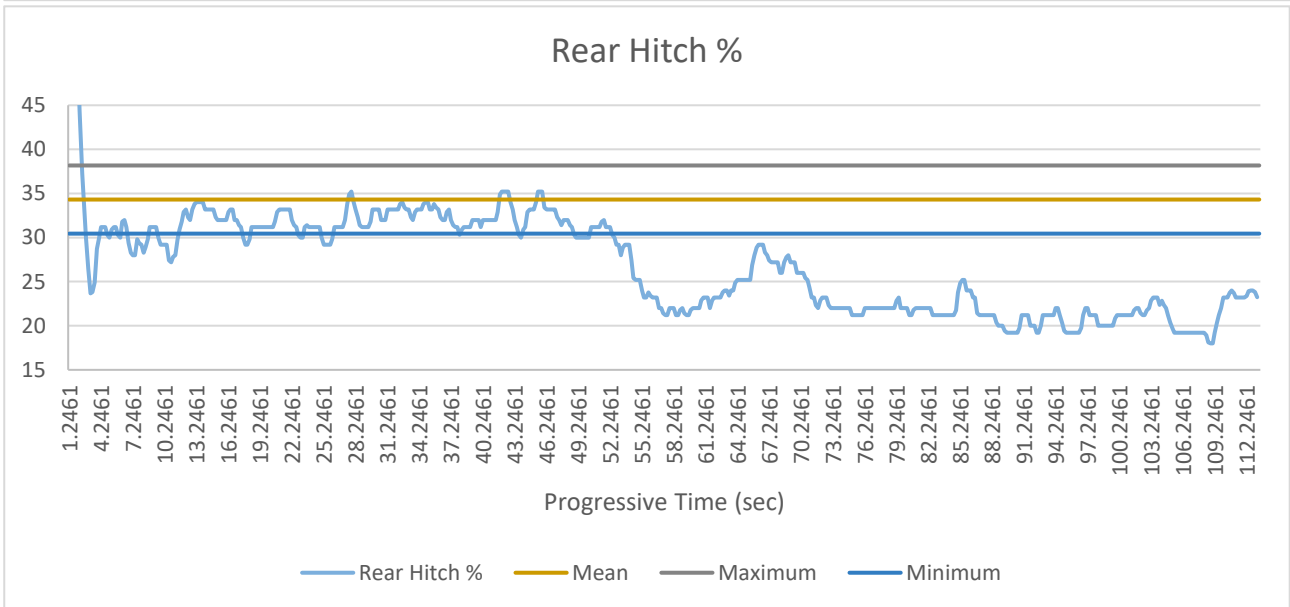
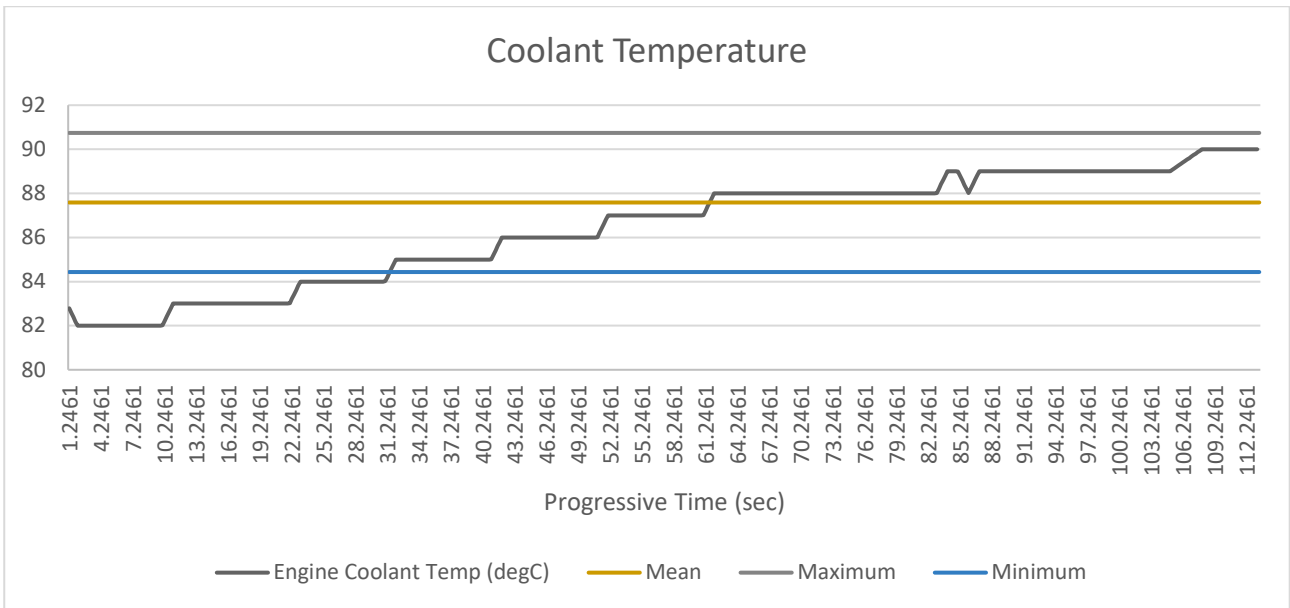




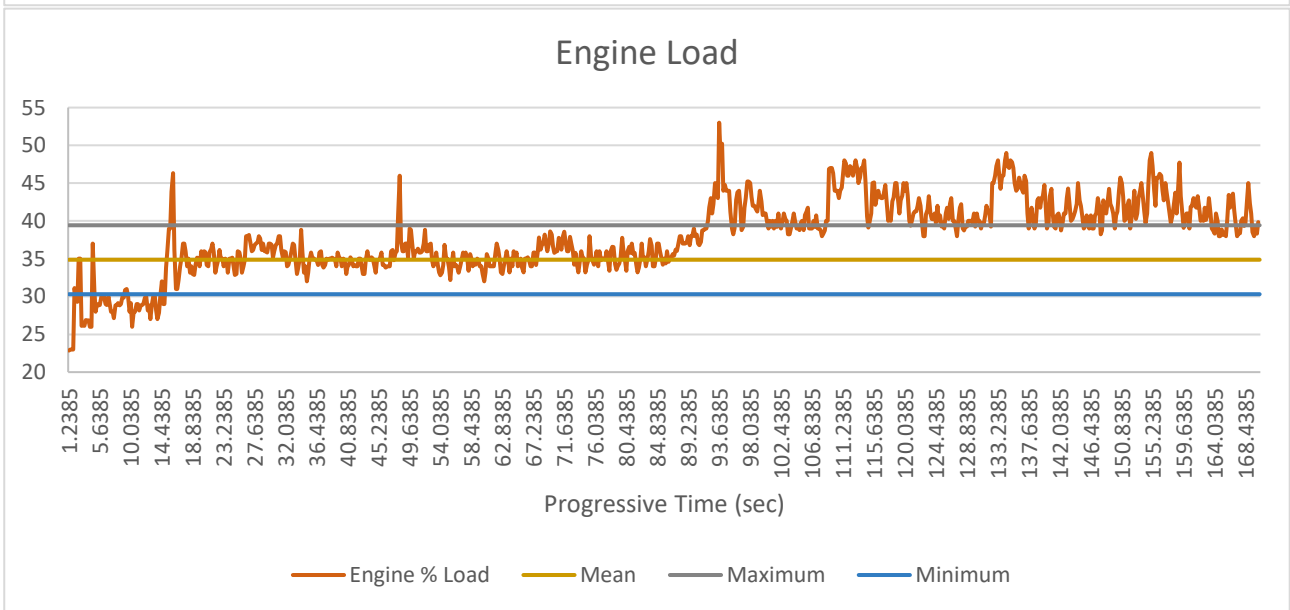
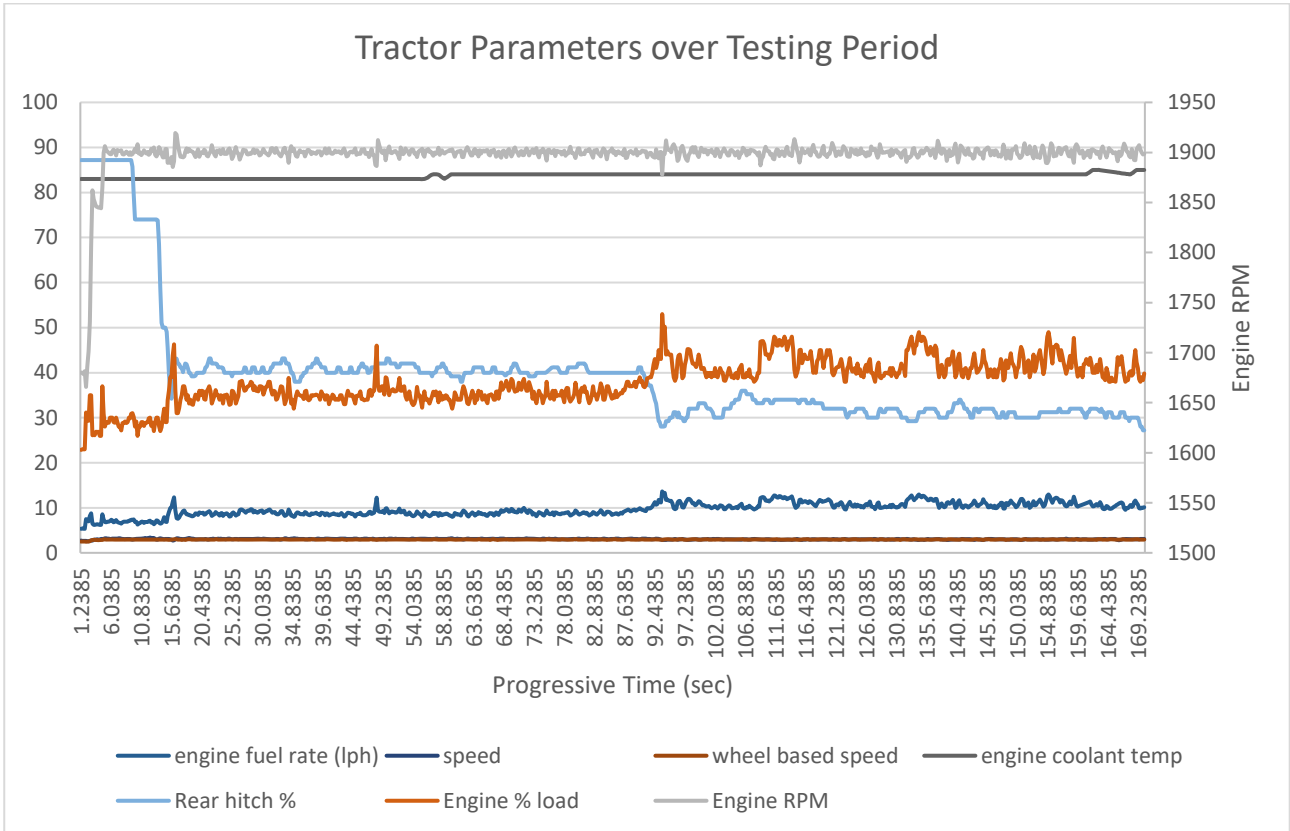
300mm – 5kph

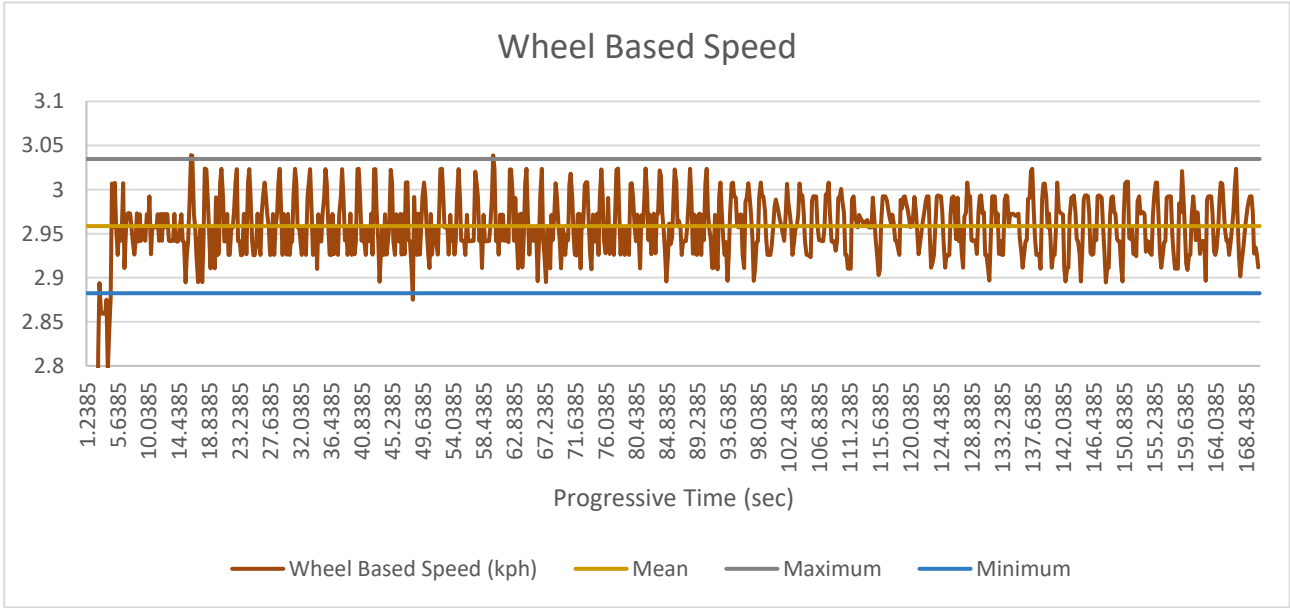
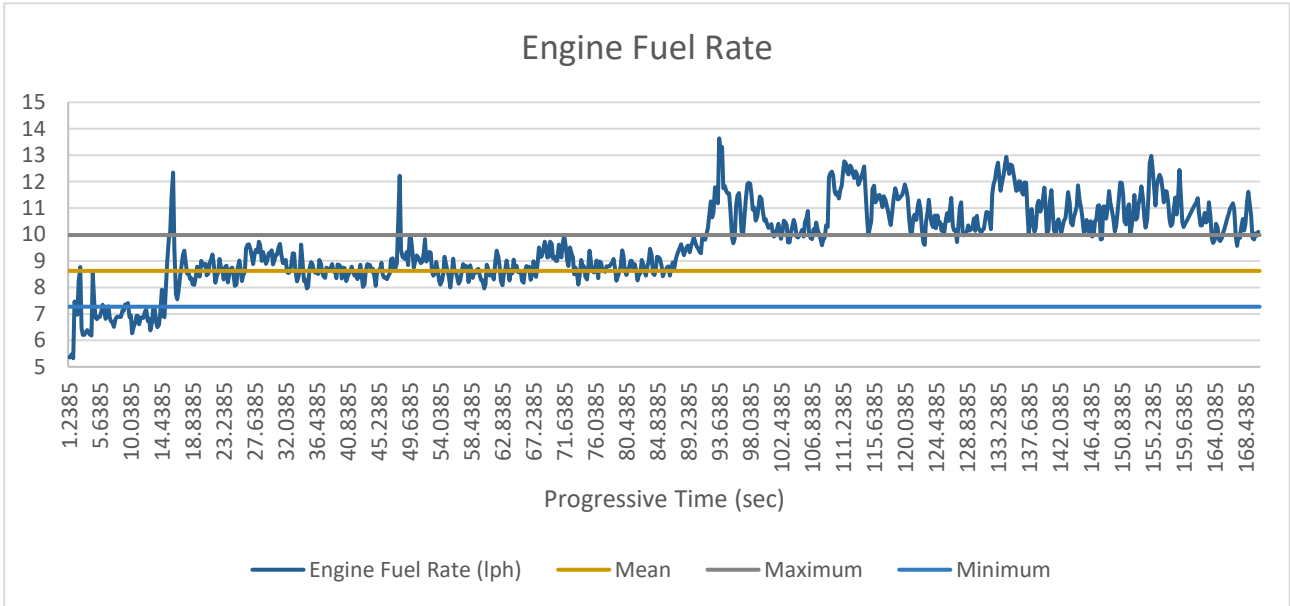
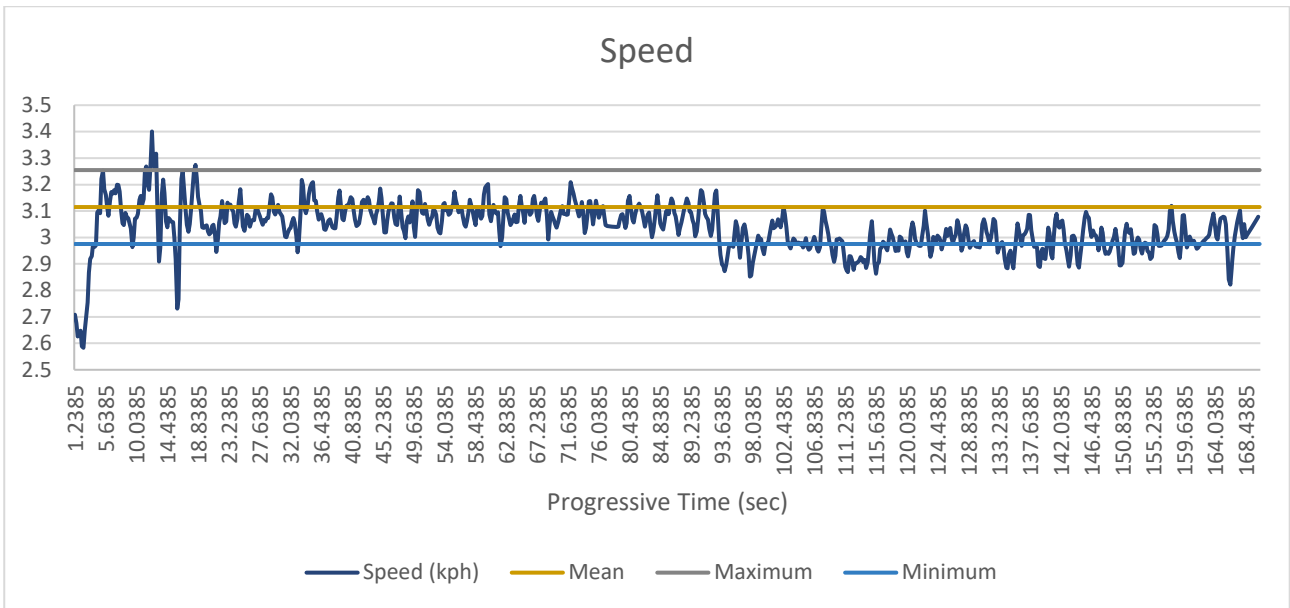


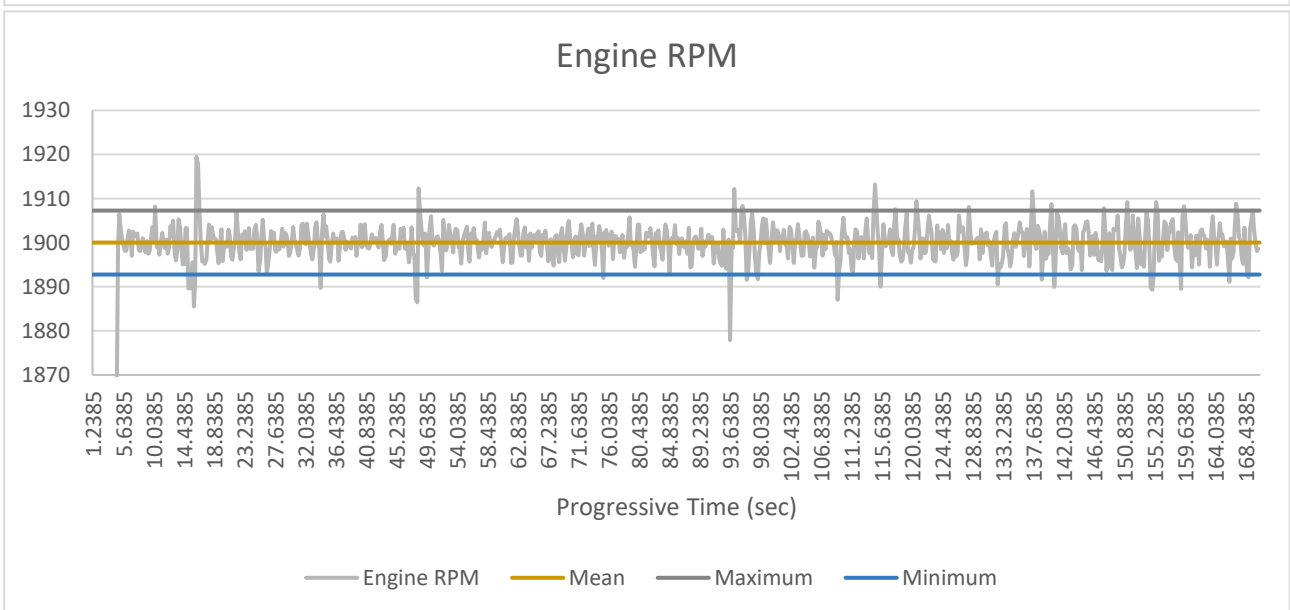
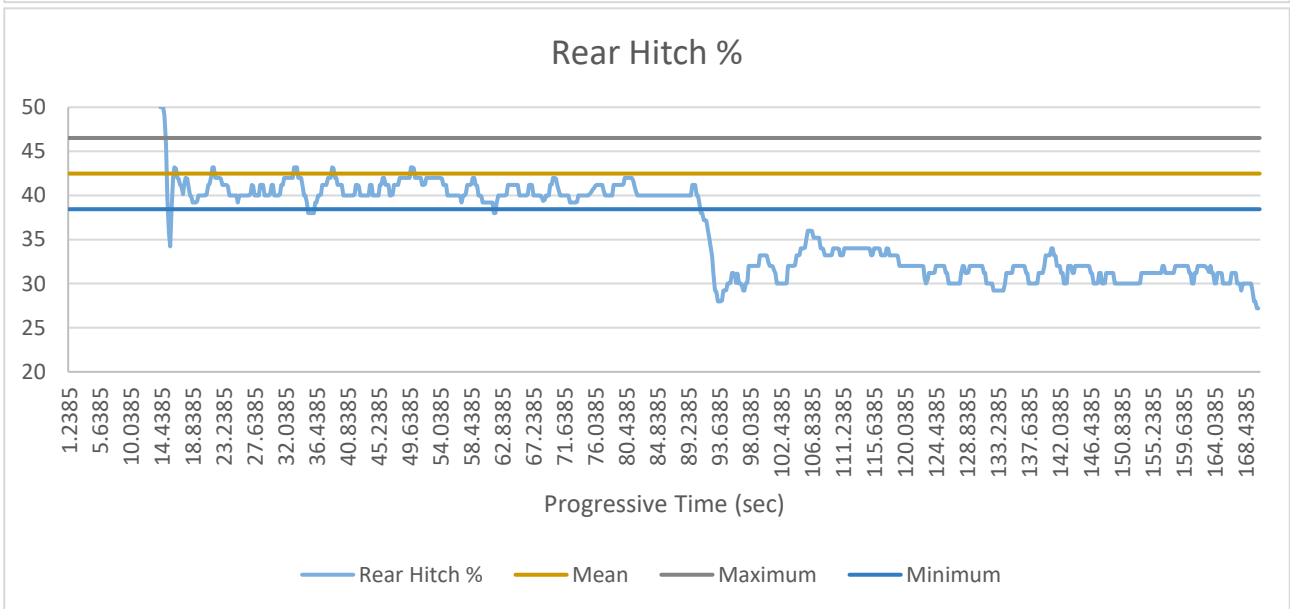
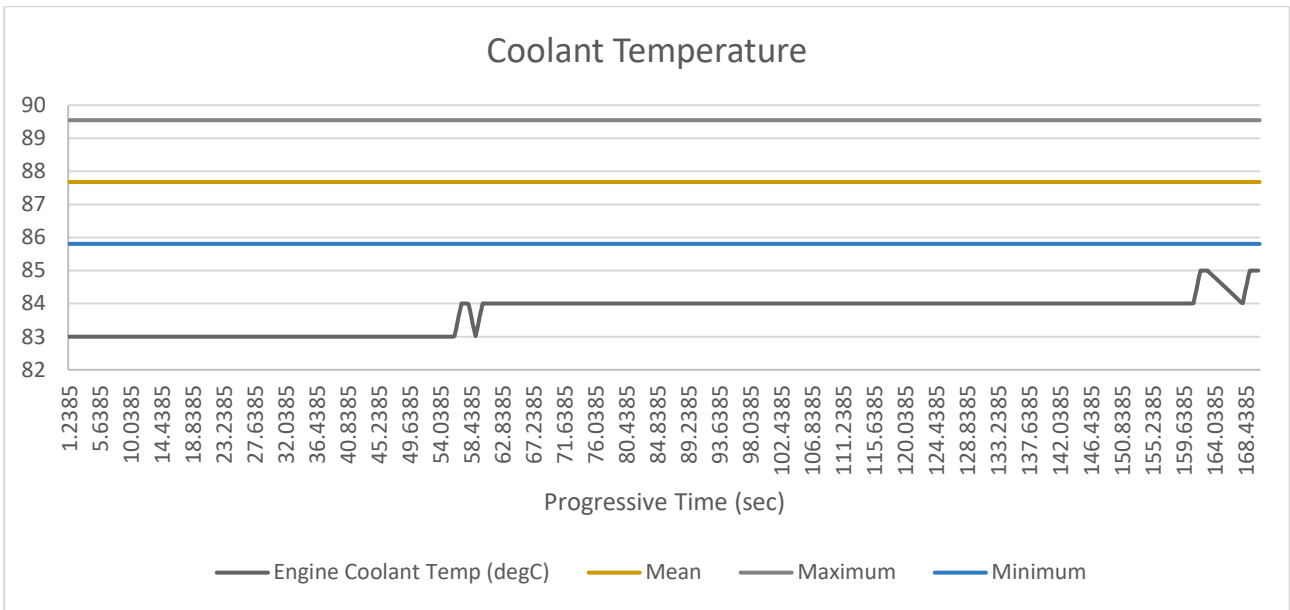




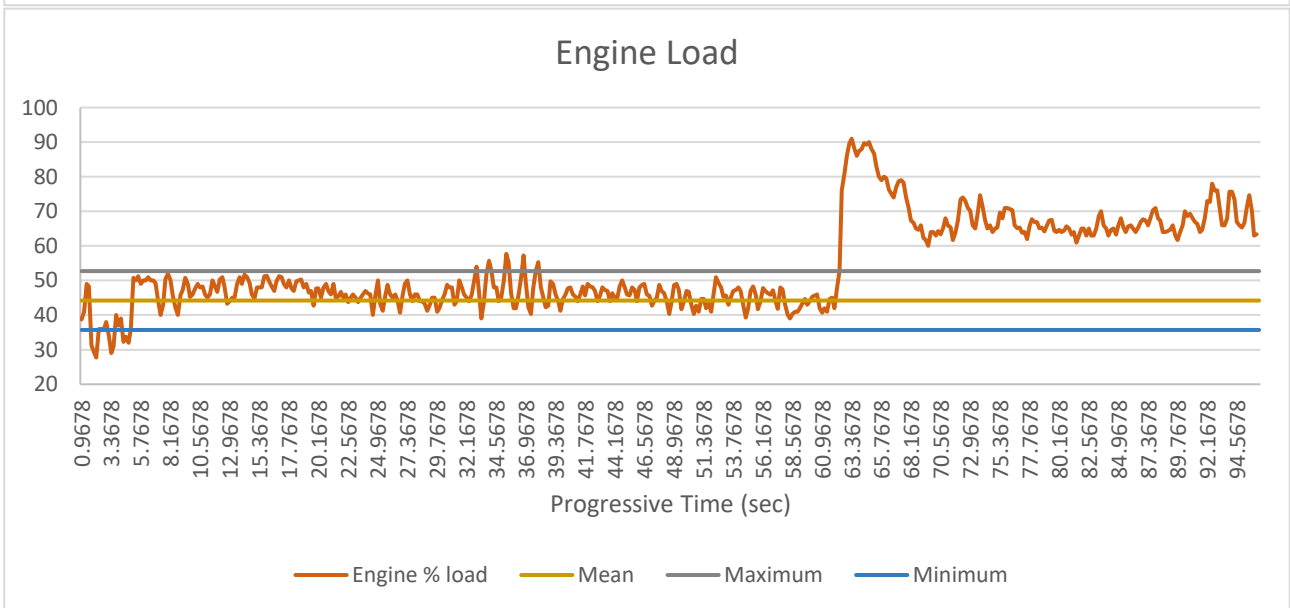
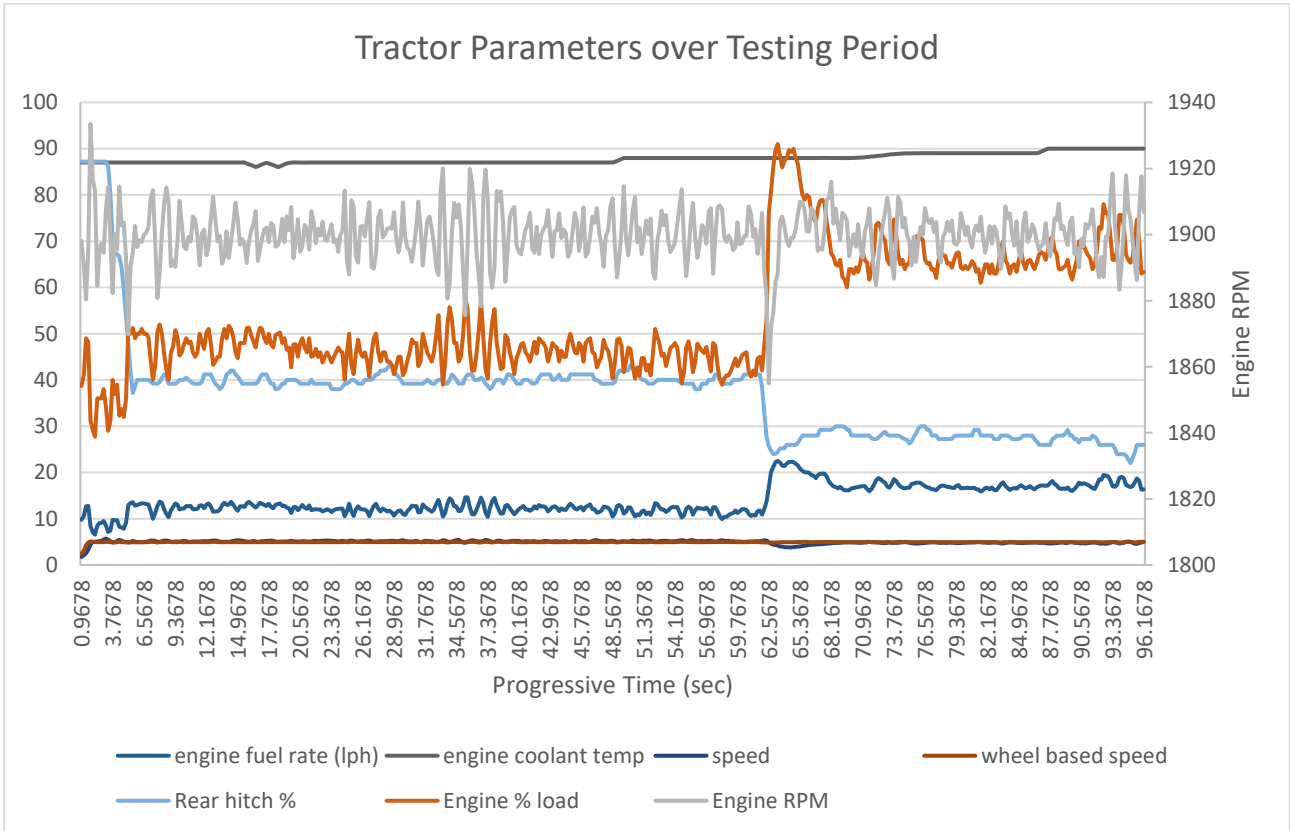
200mm – 3kph

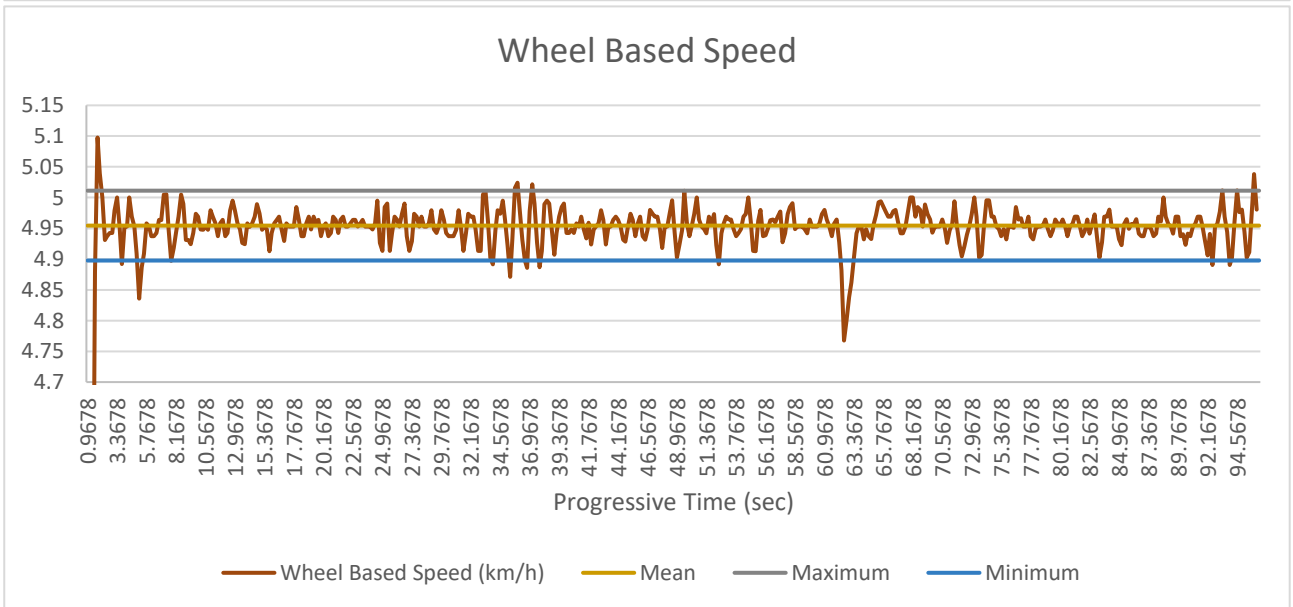
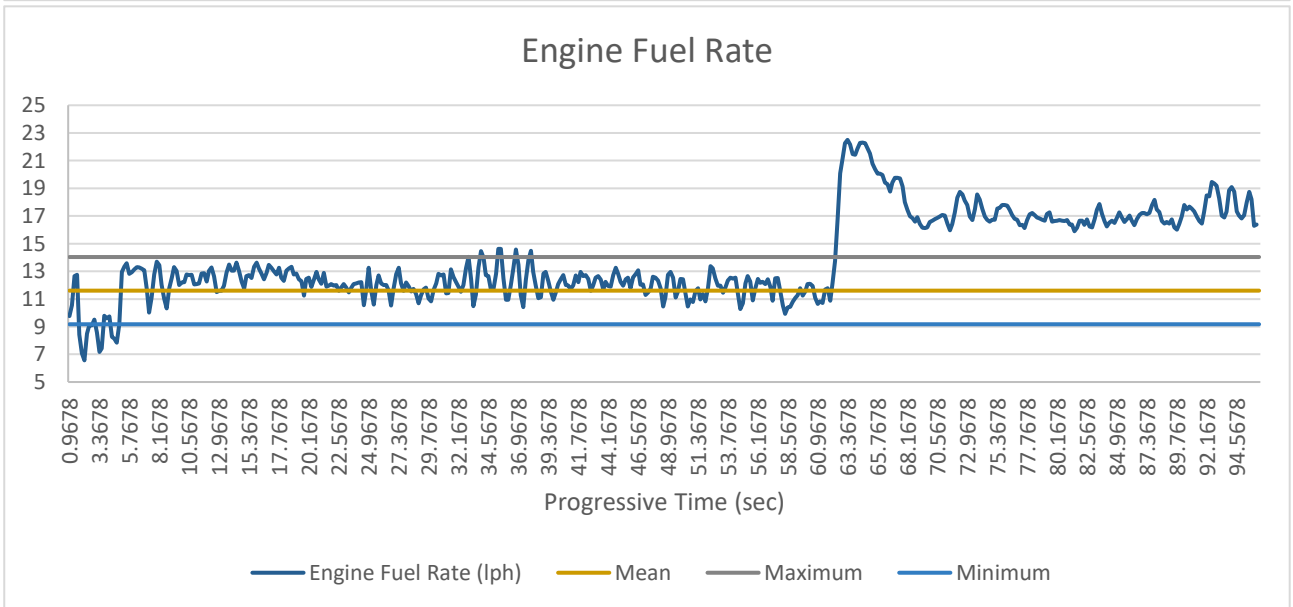
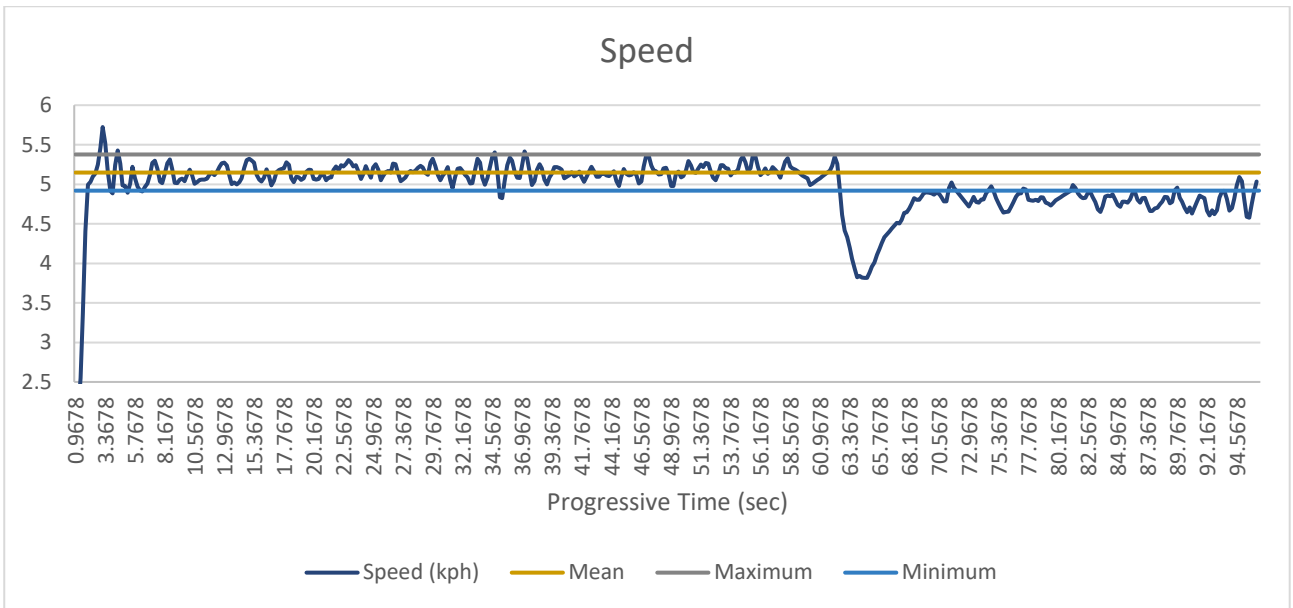


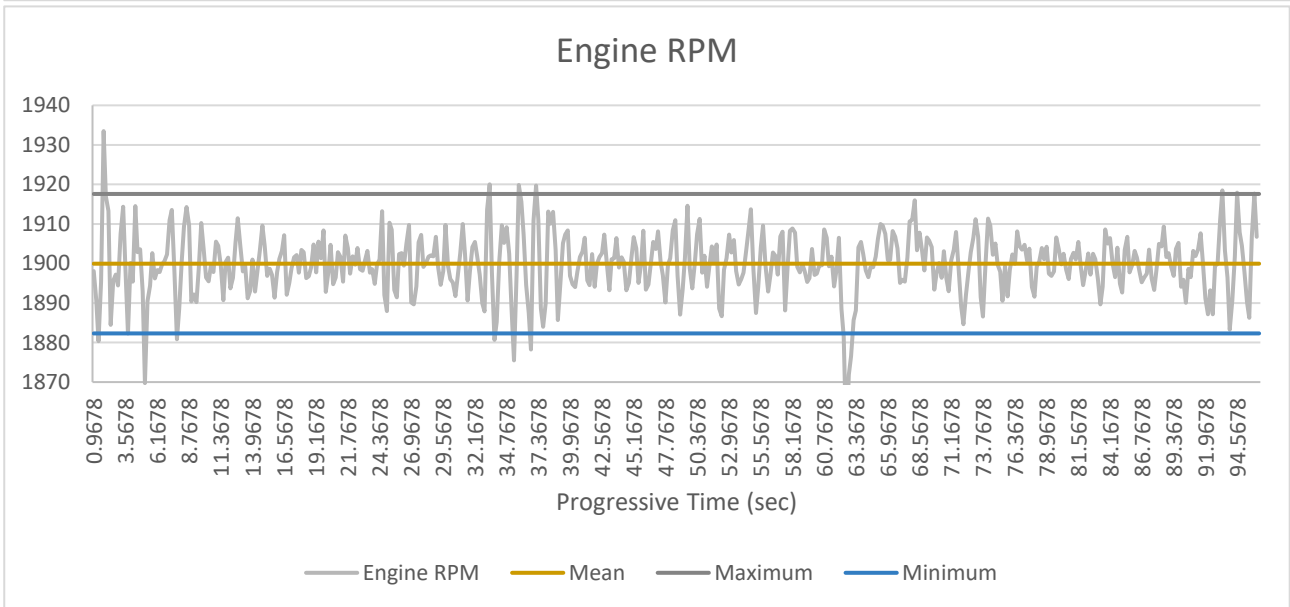
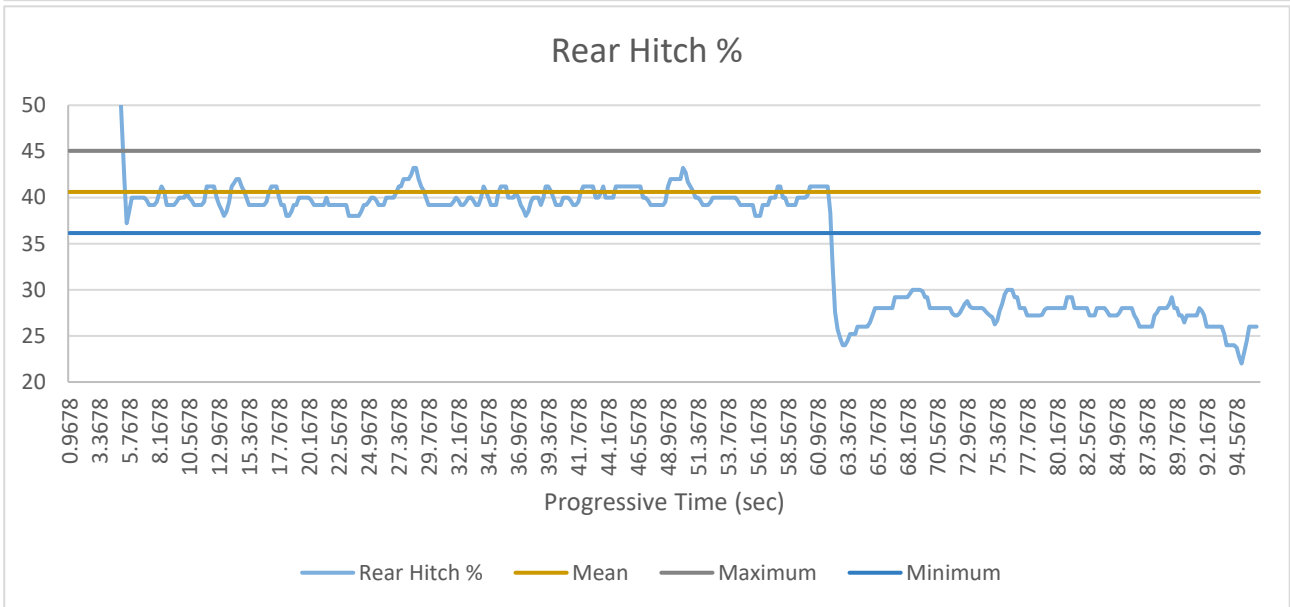
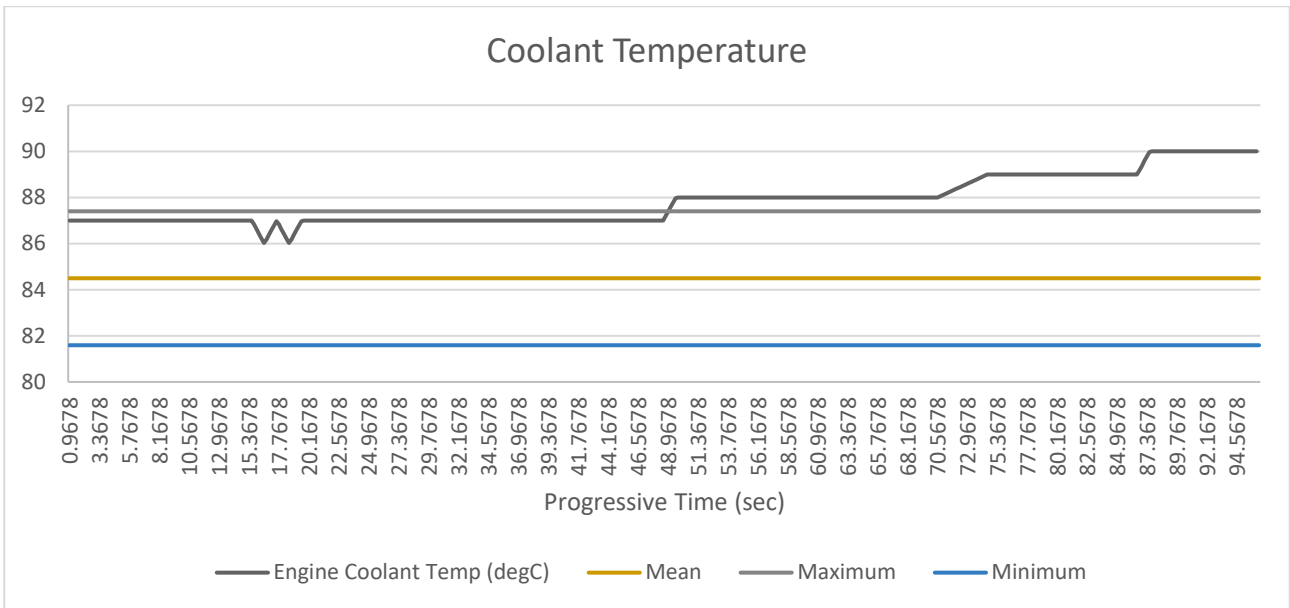




200mm – 5kph

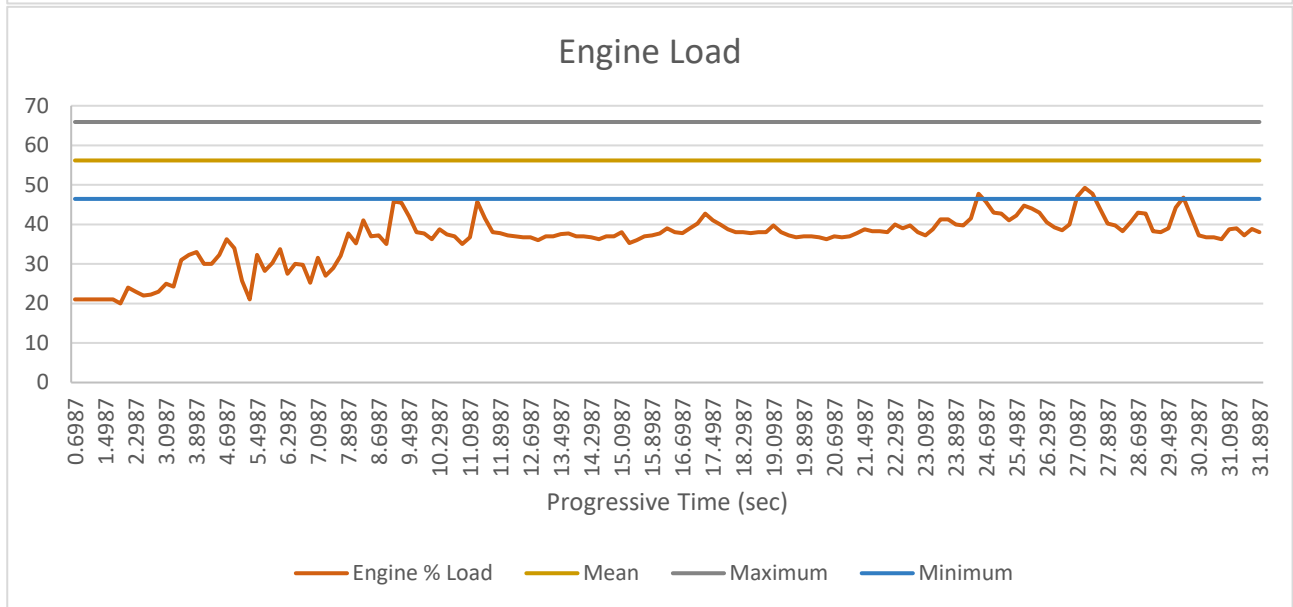
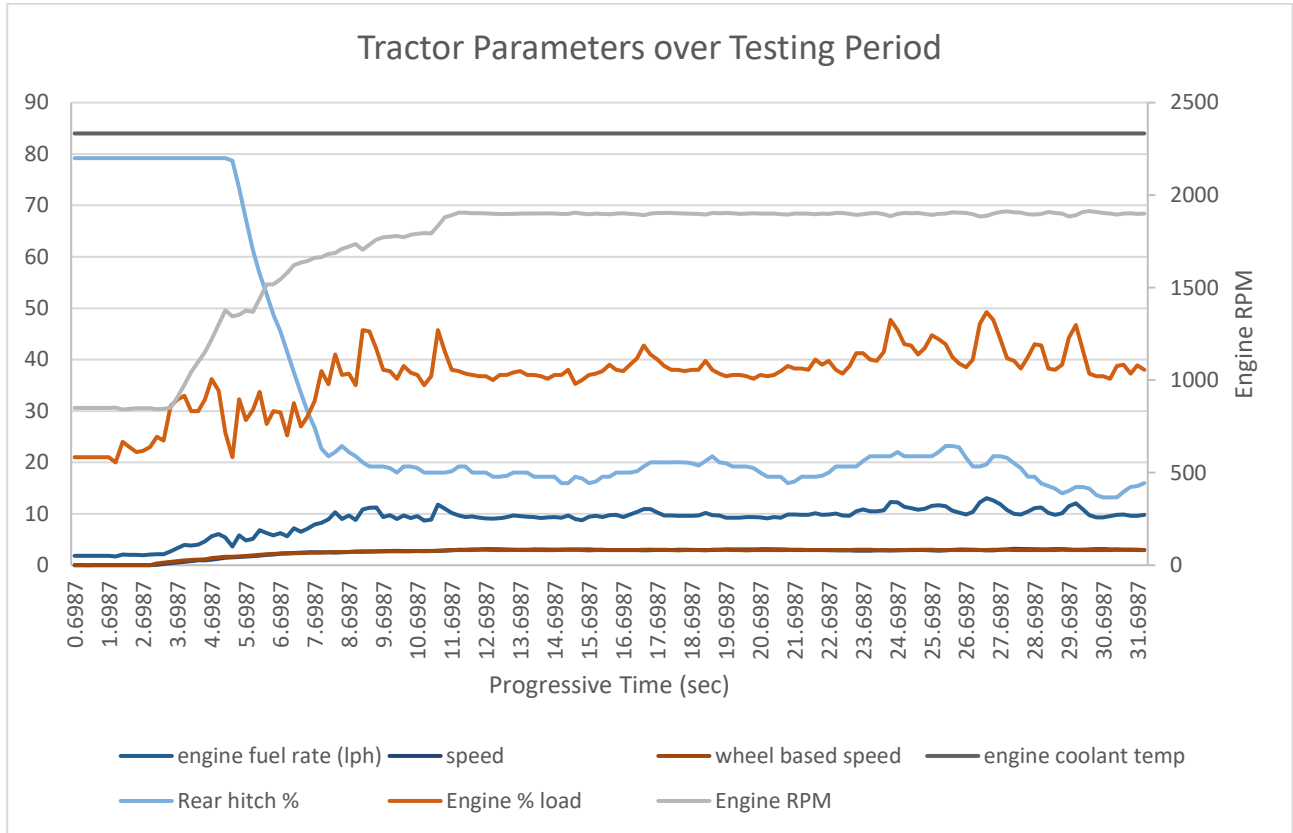


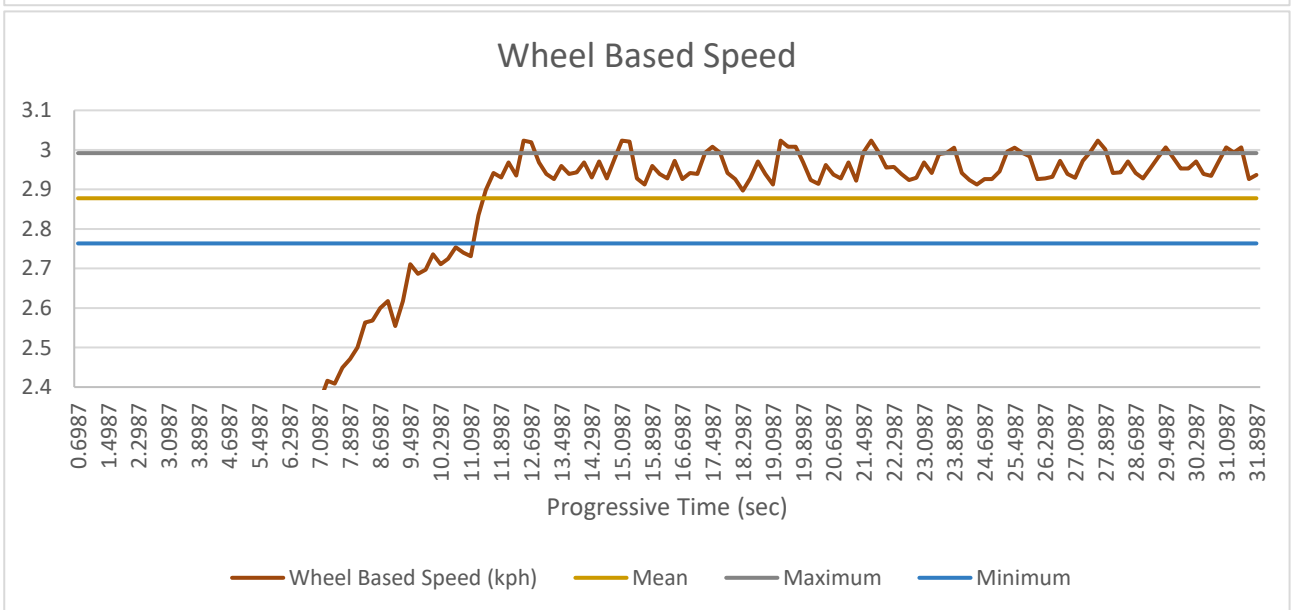
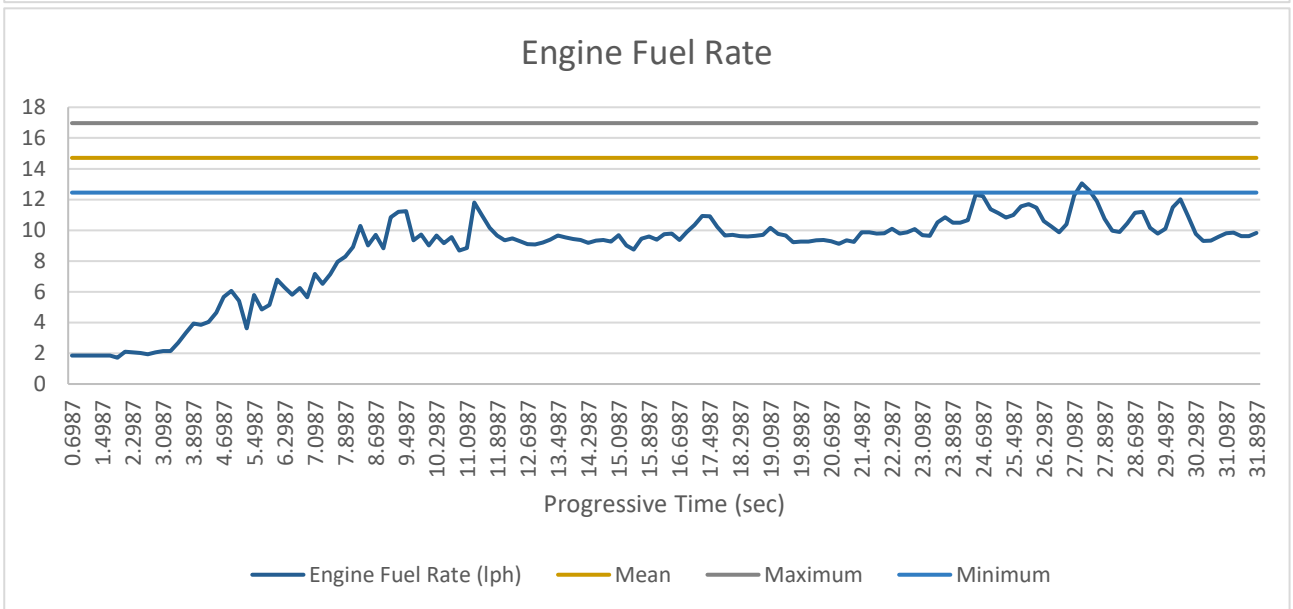
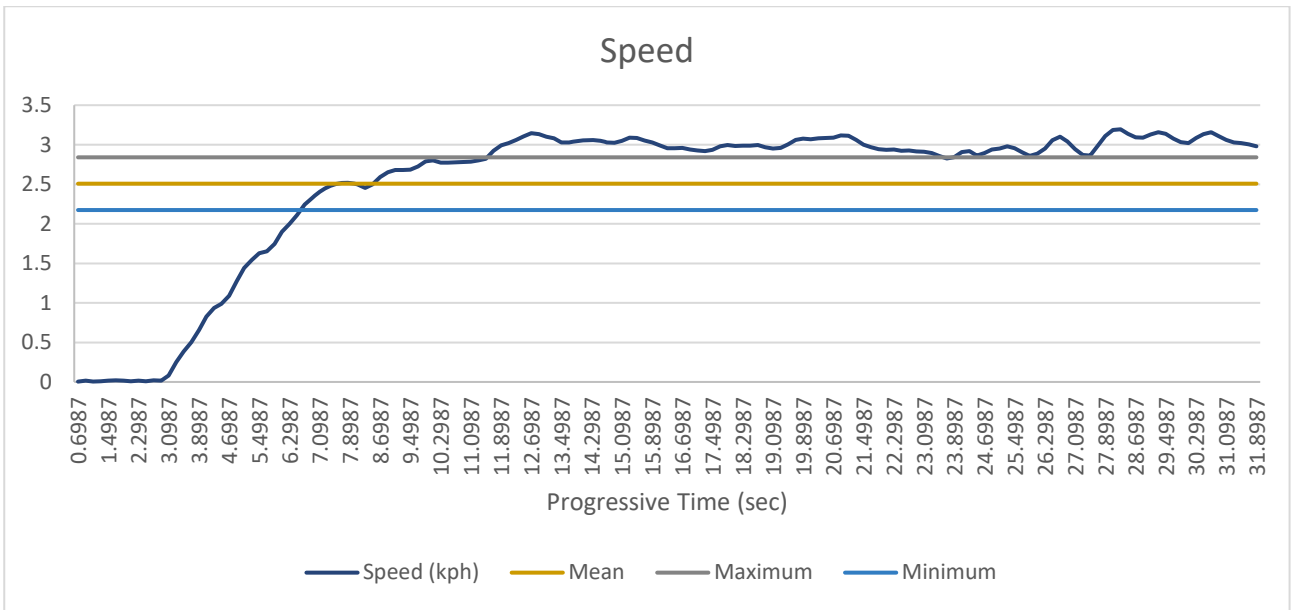


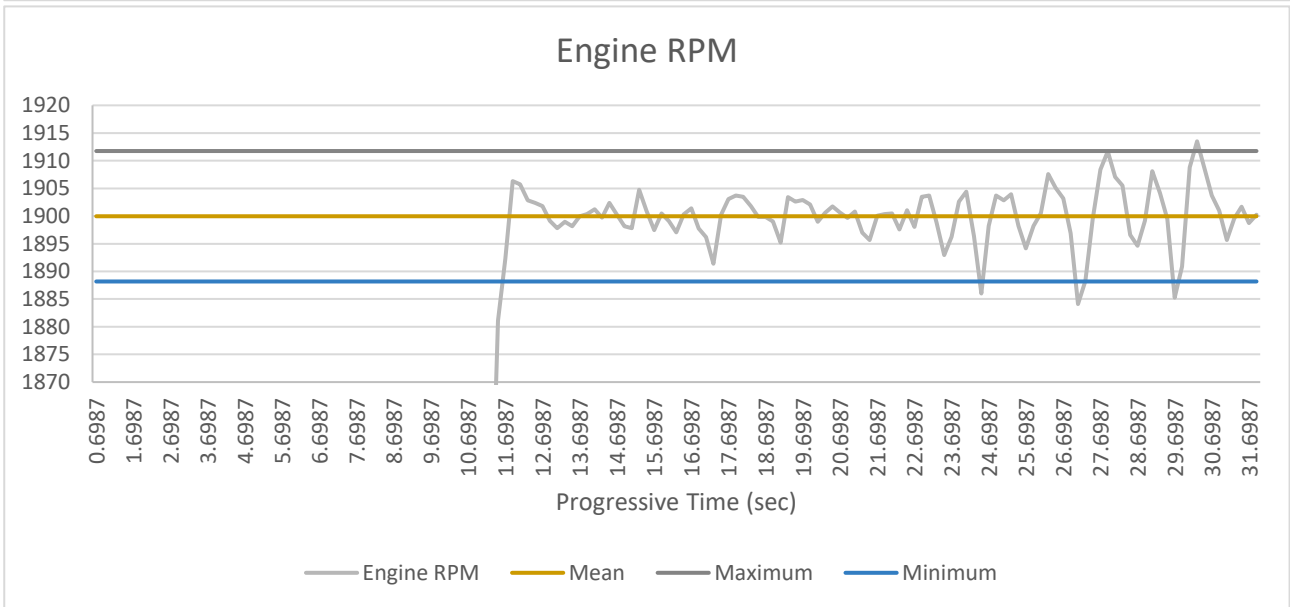
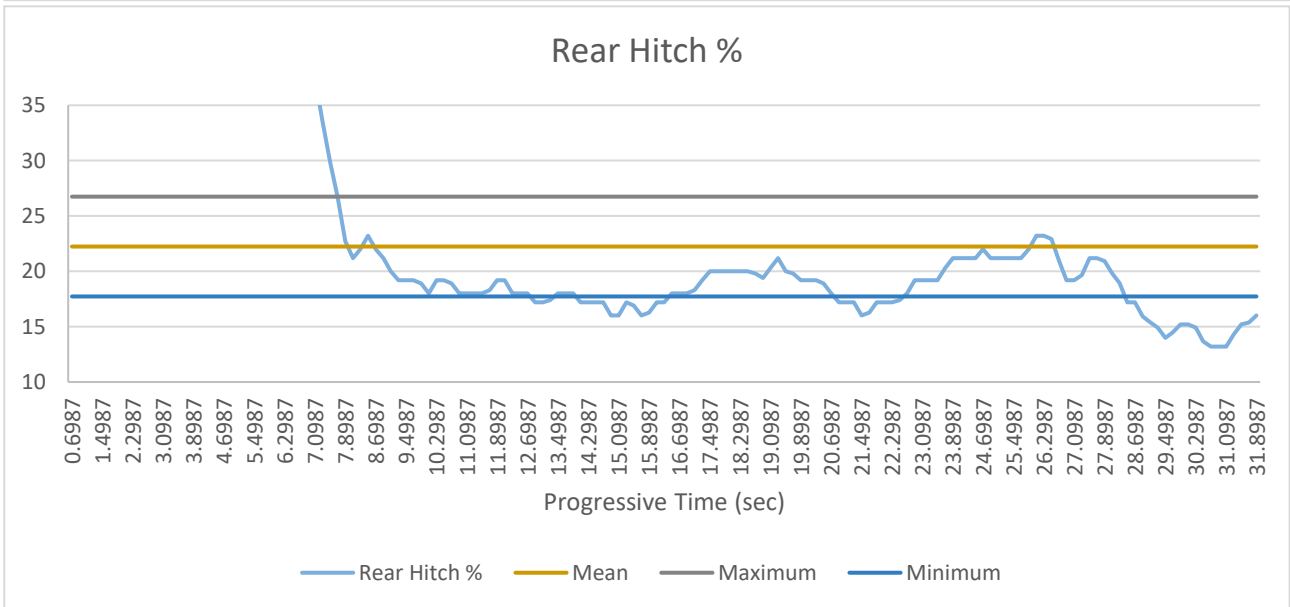
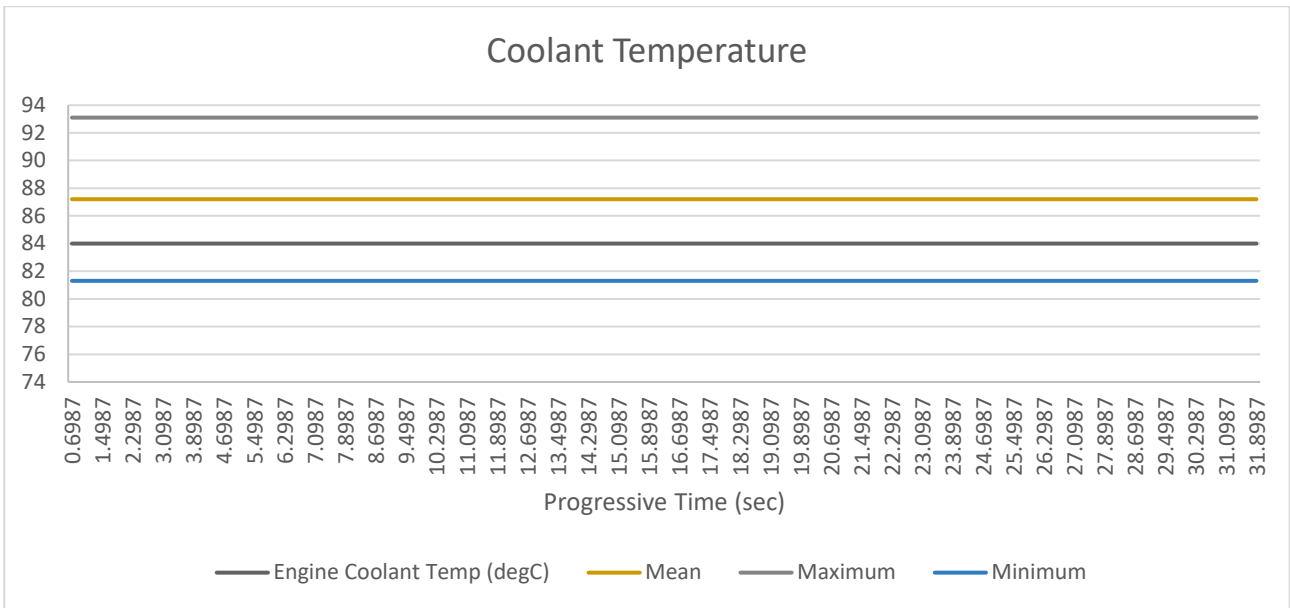


Appendix I – 3PL Deep Ripper – Bridging occurring across tines data

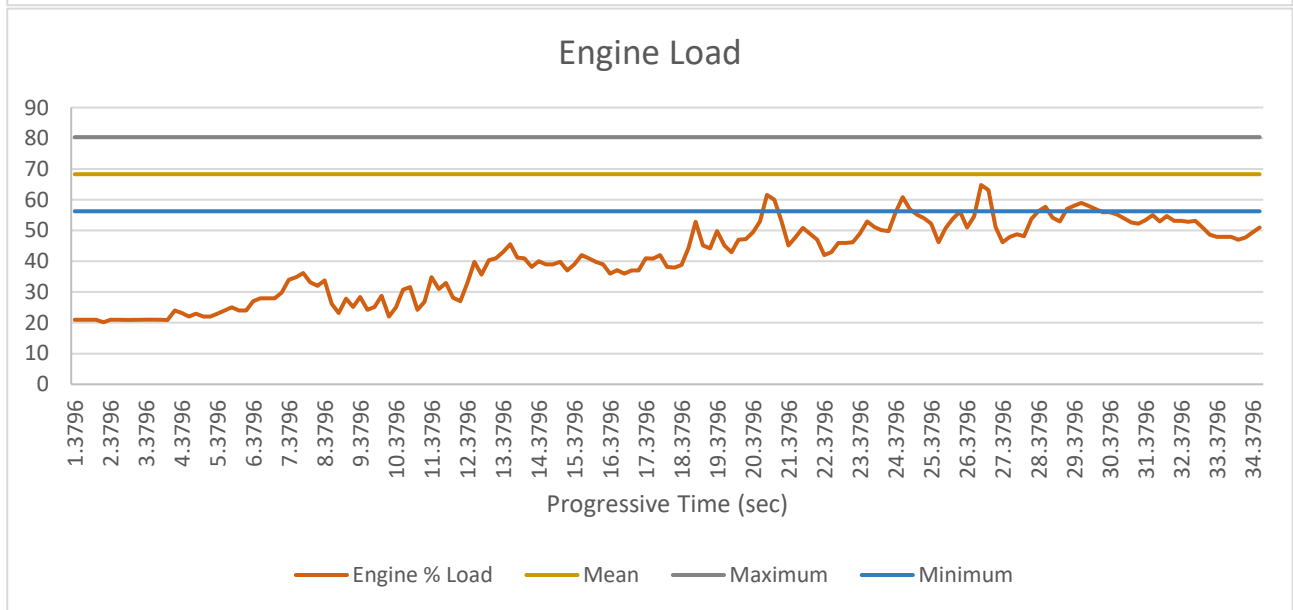
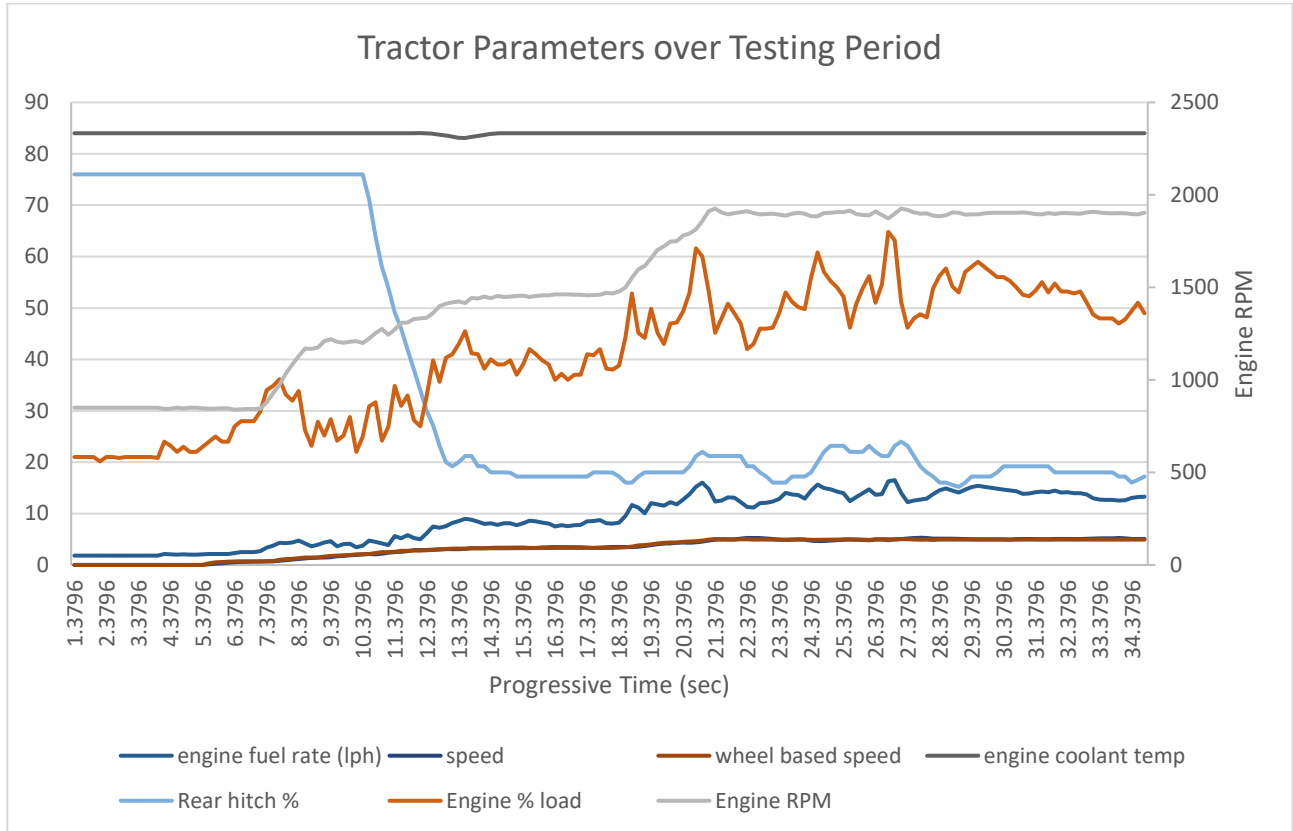
350mm – 3kph

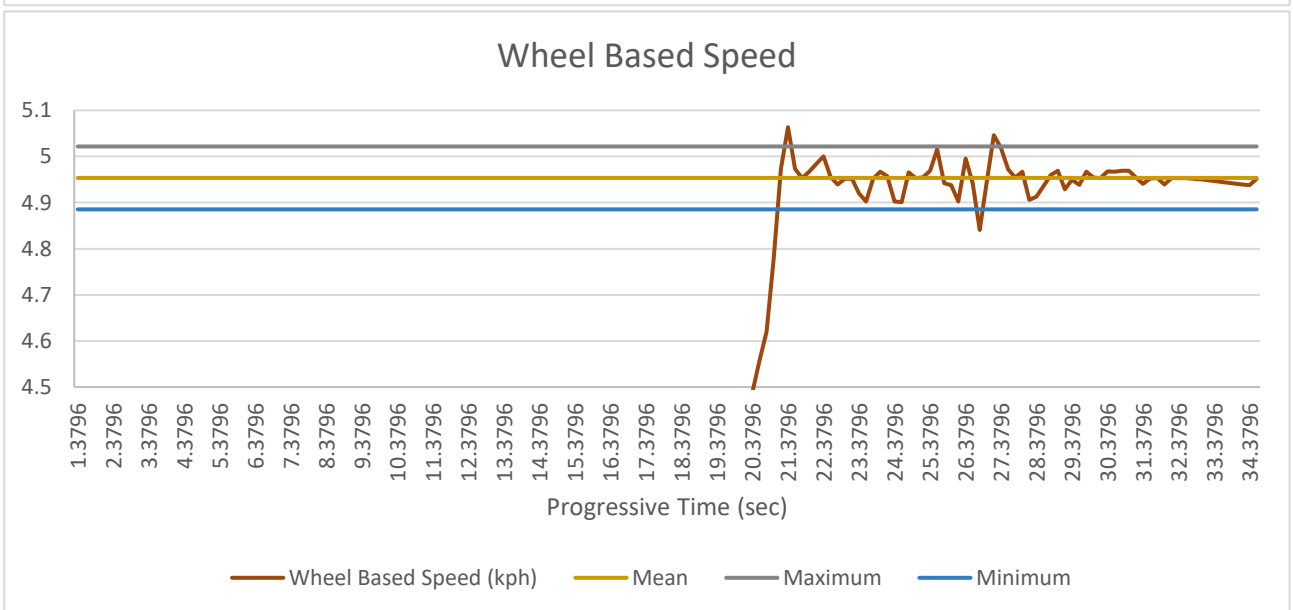
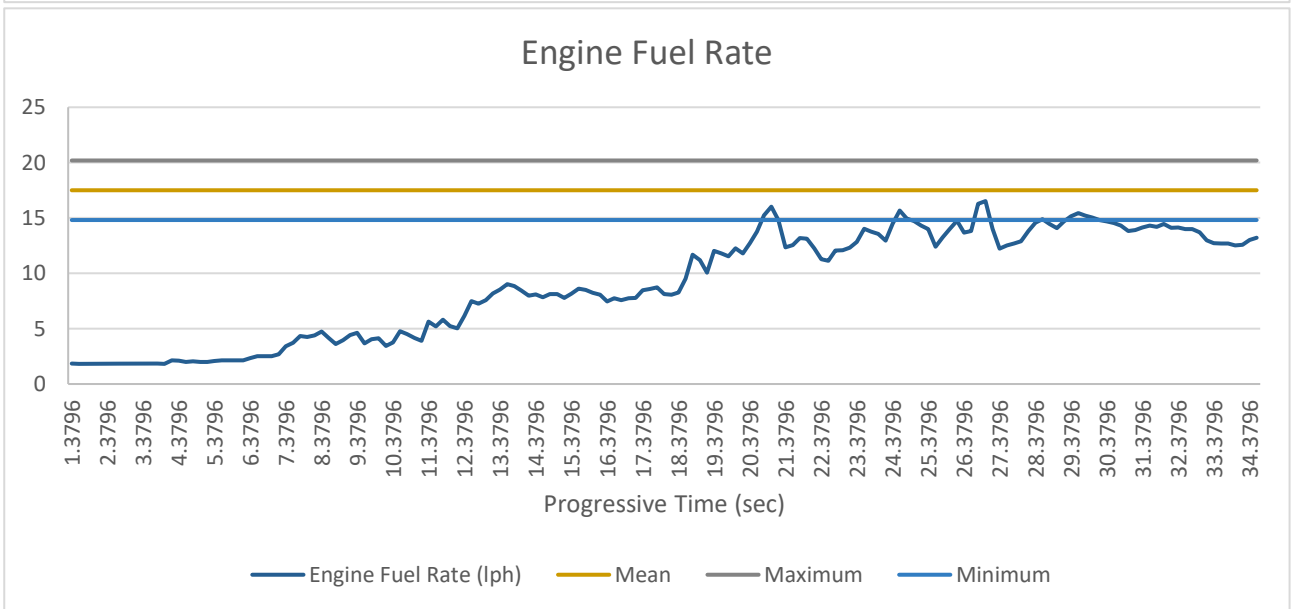
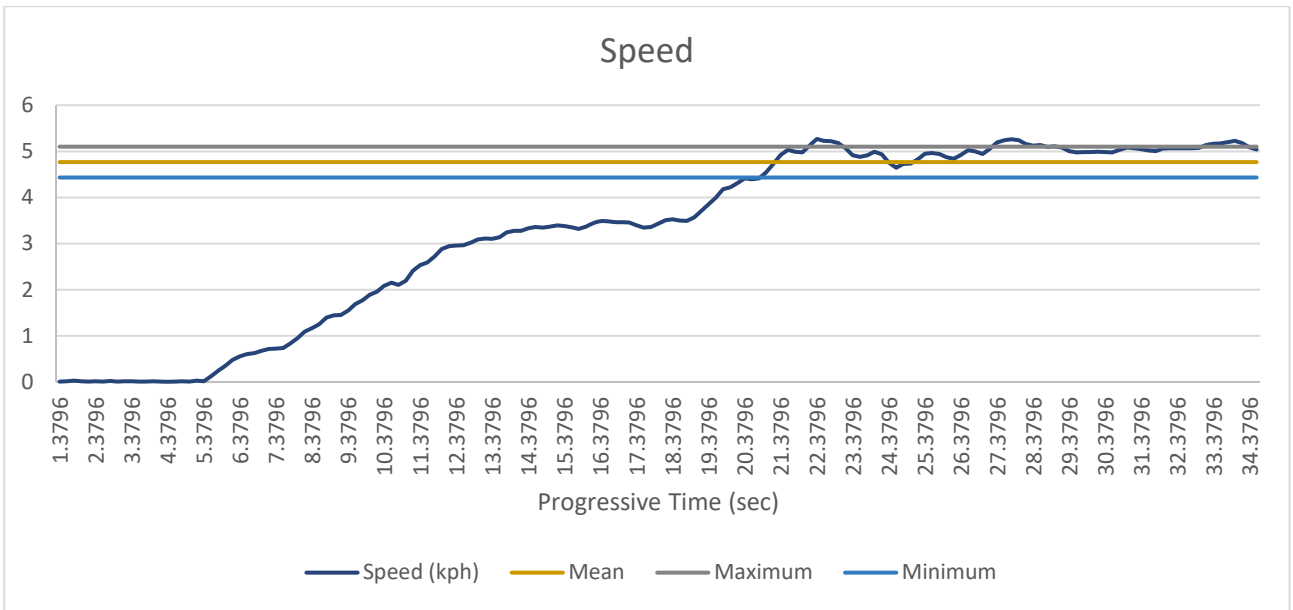


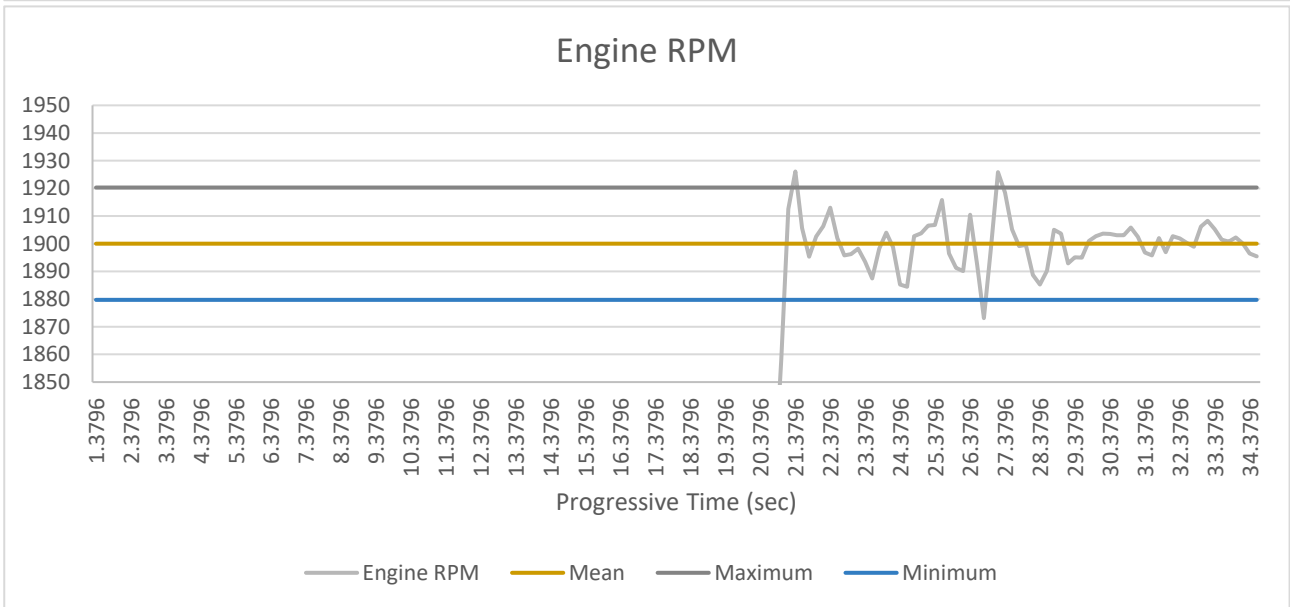
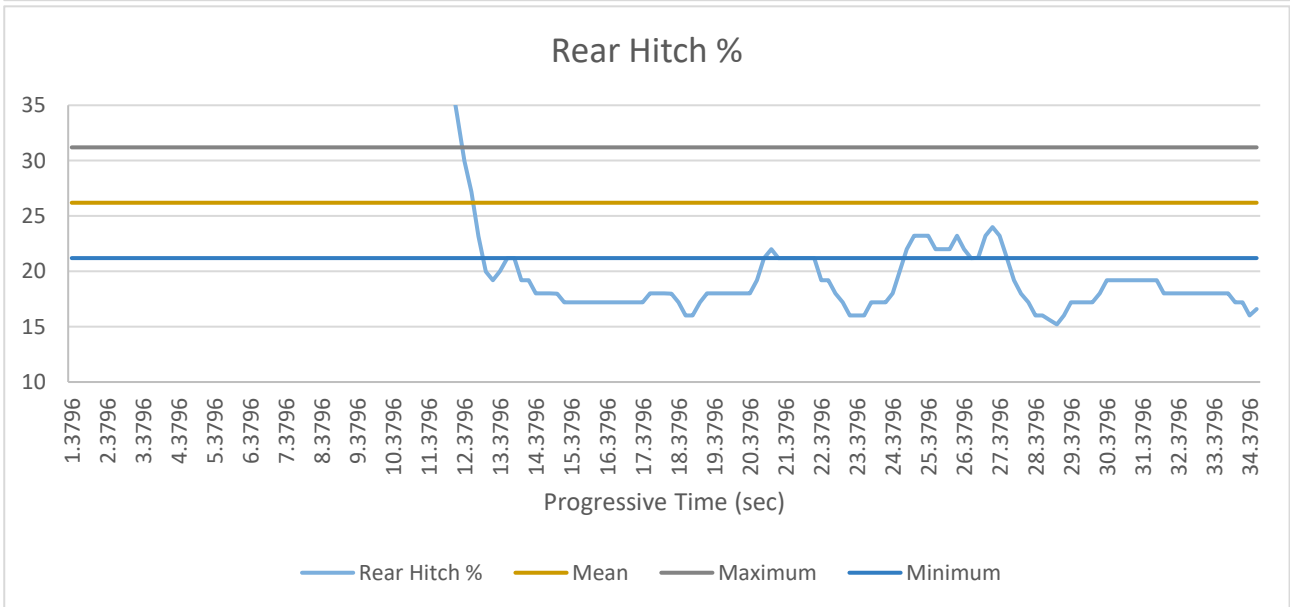
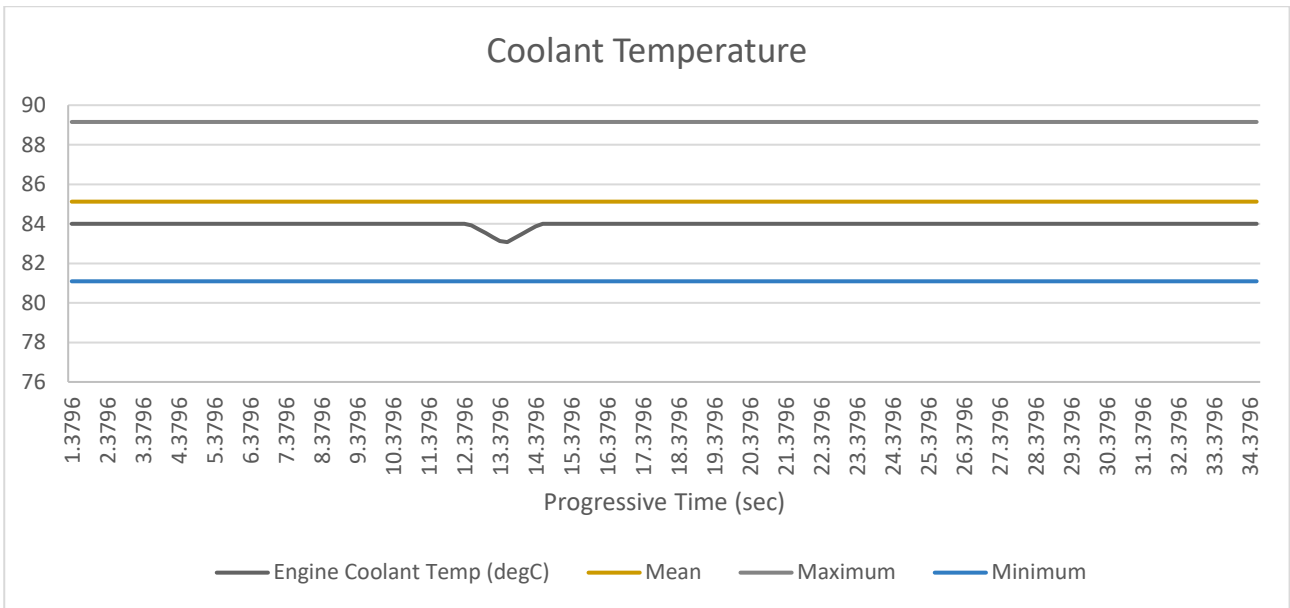




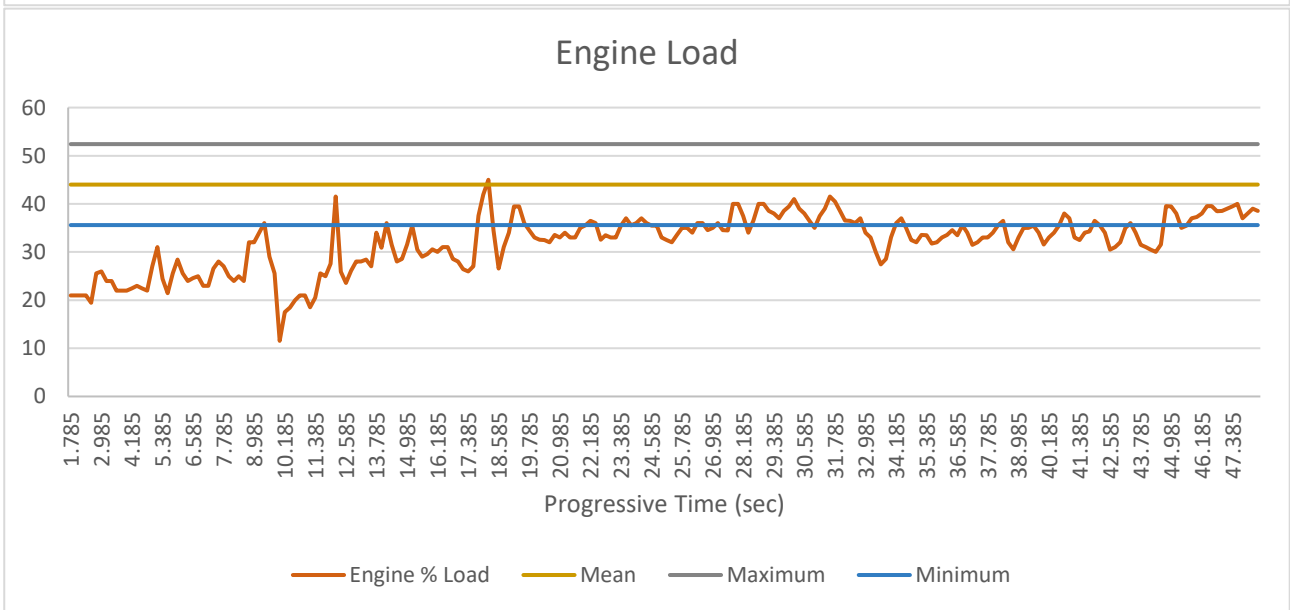
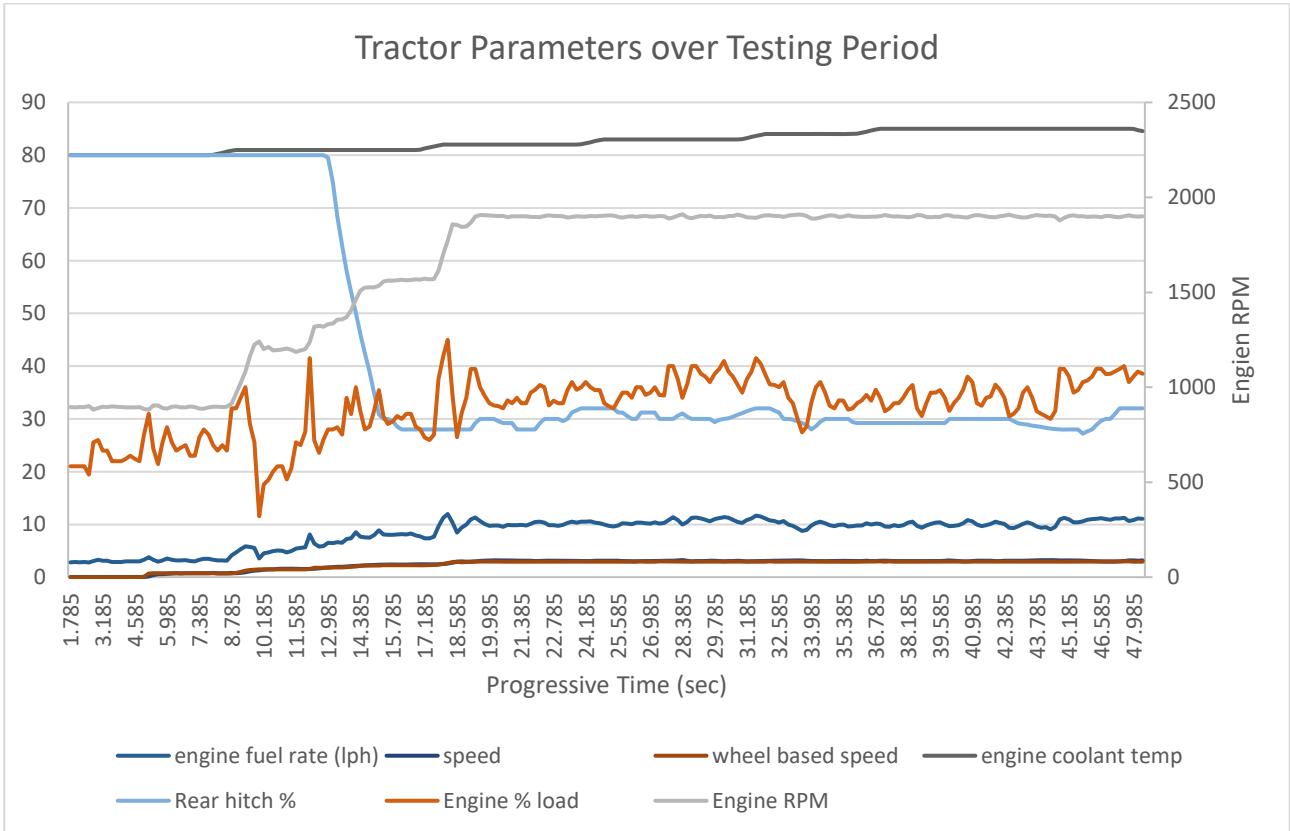
350mm – 5kph

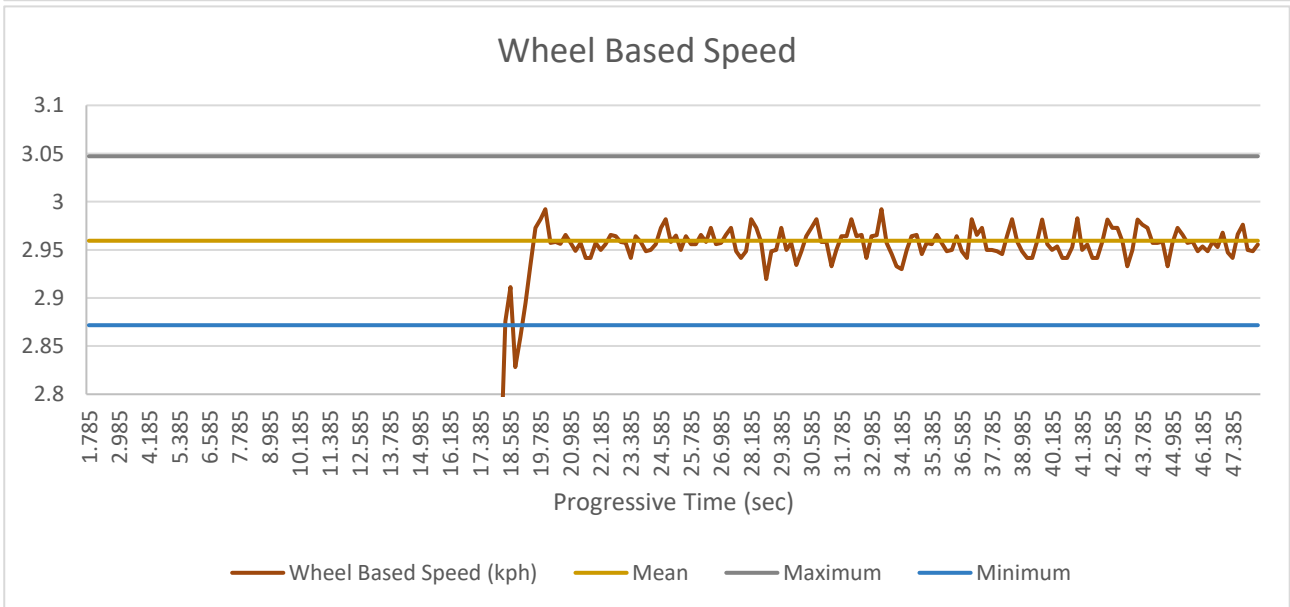
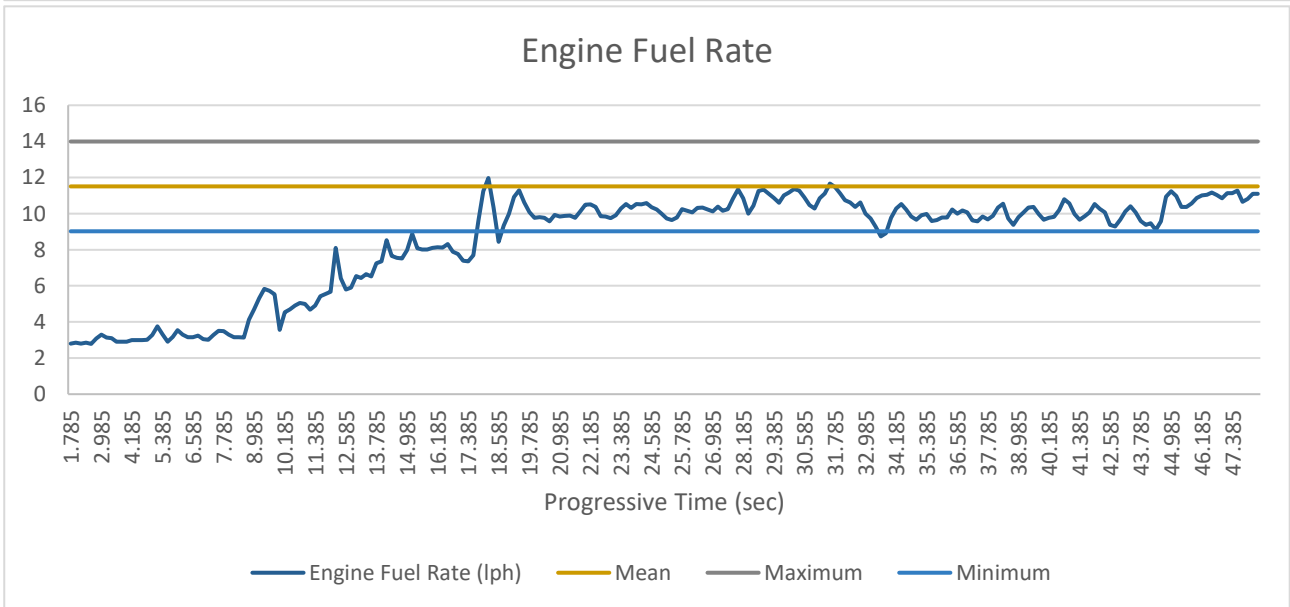
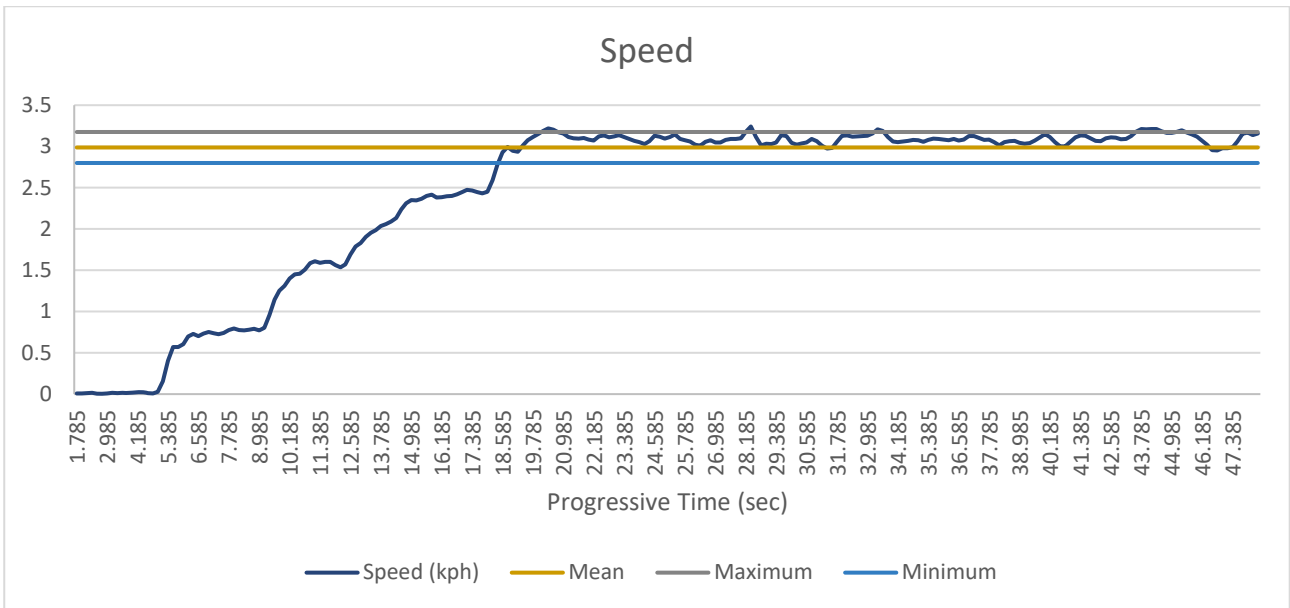


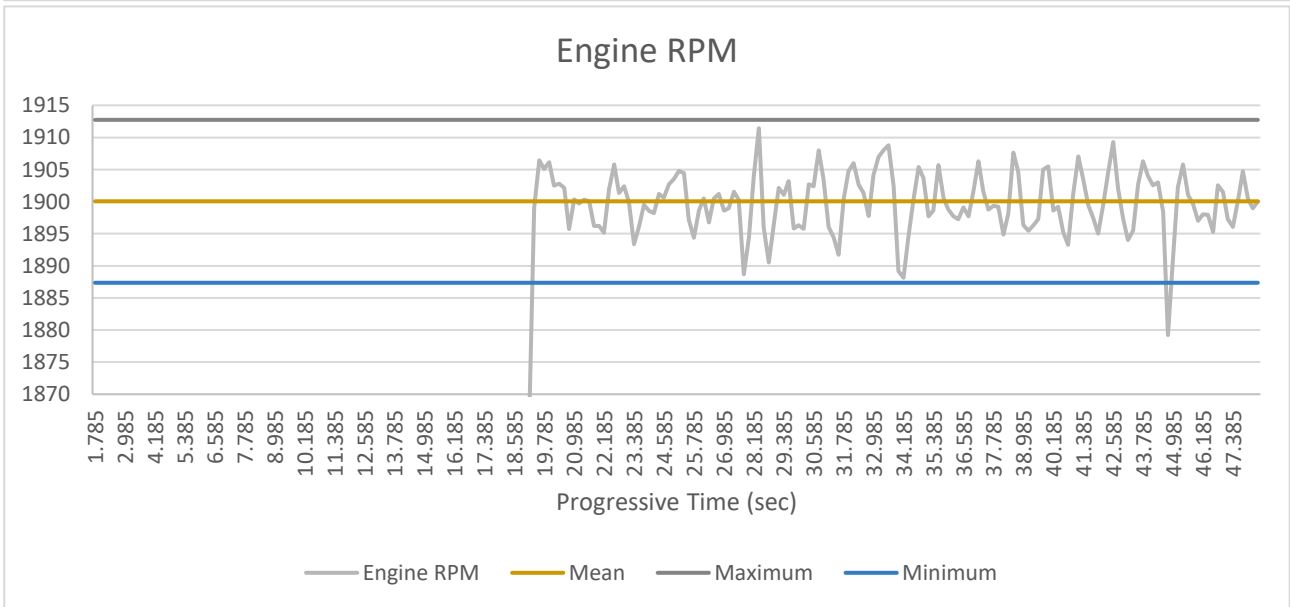
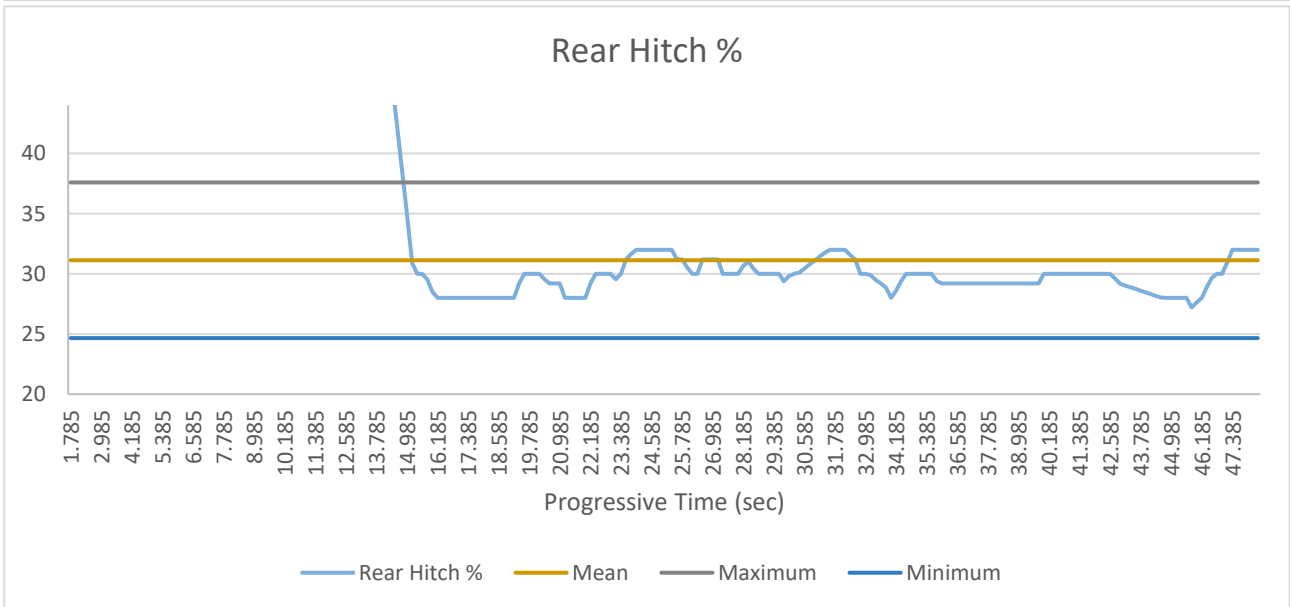
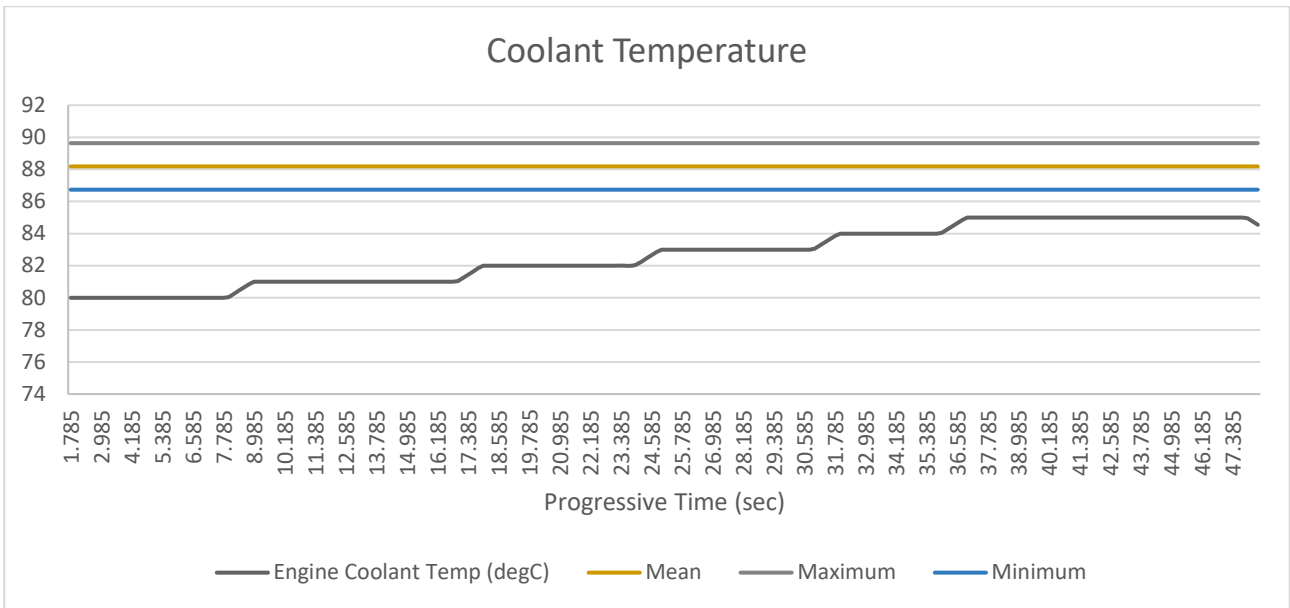




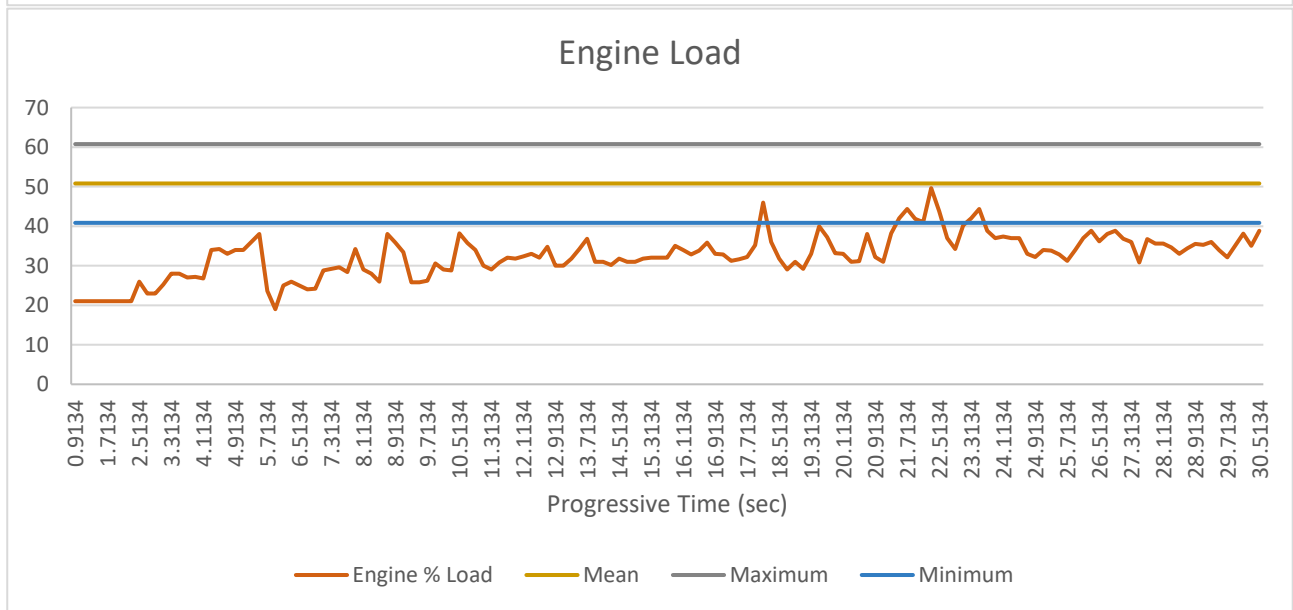
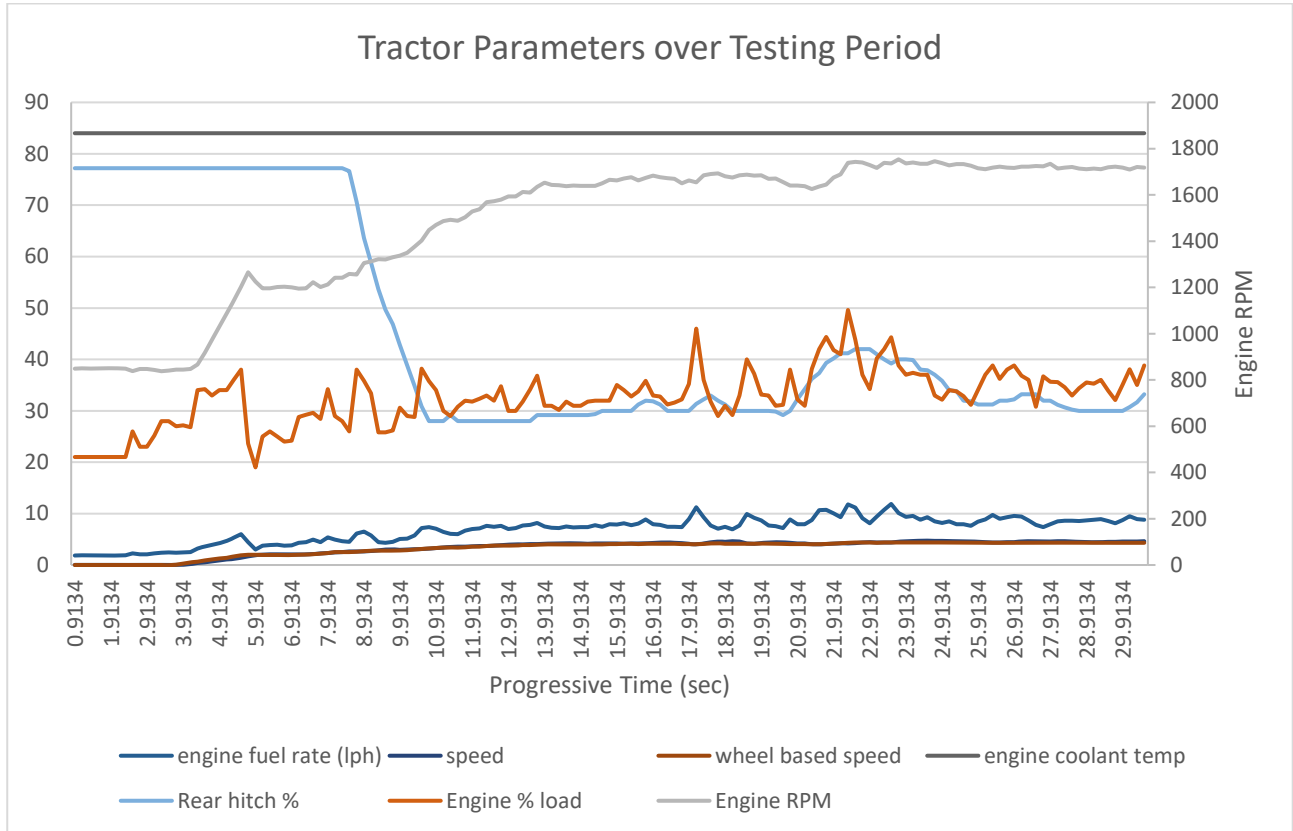
300mm – 3kph

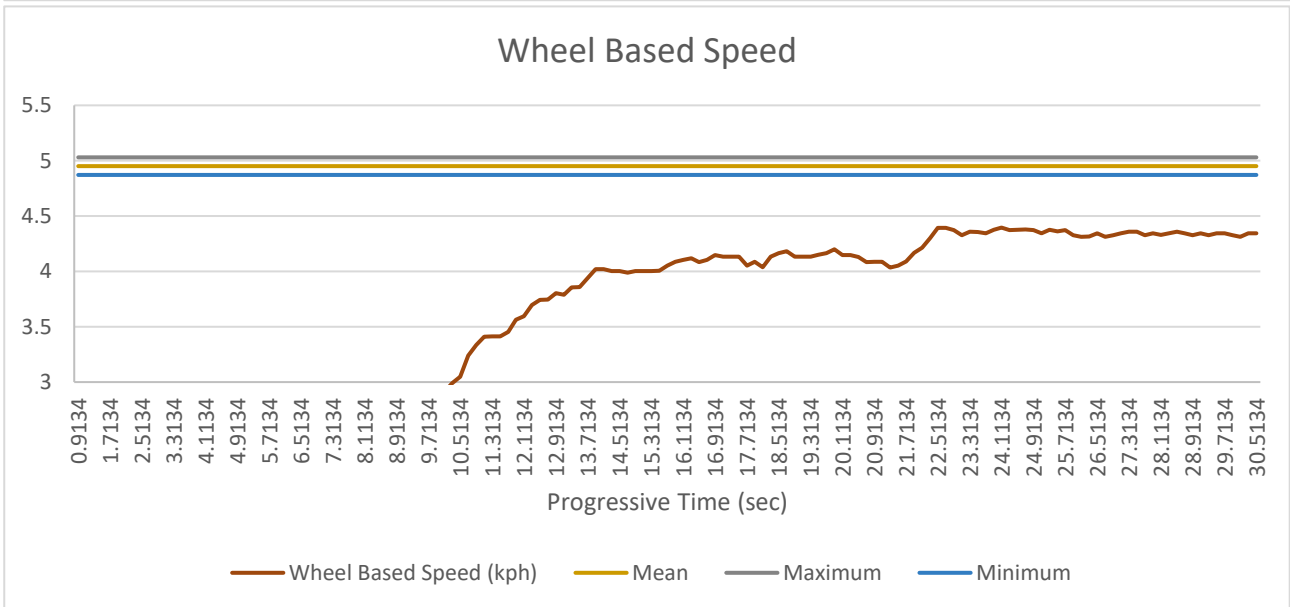
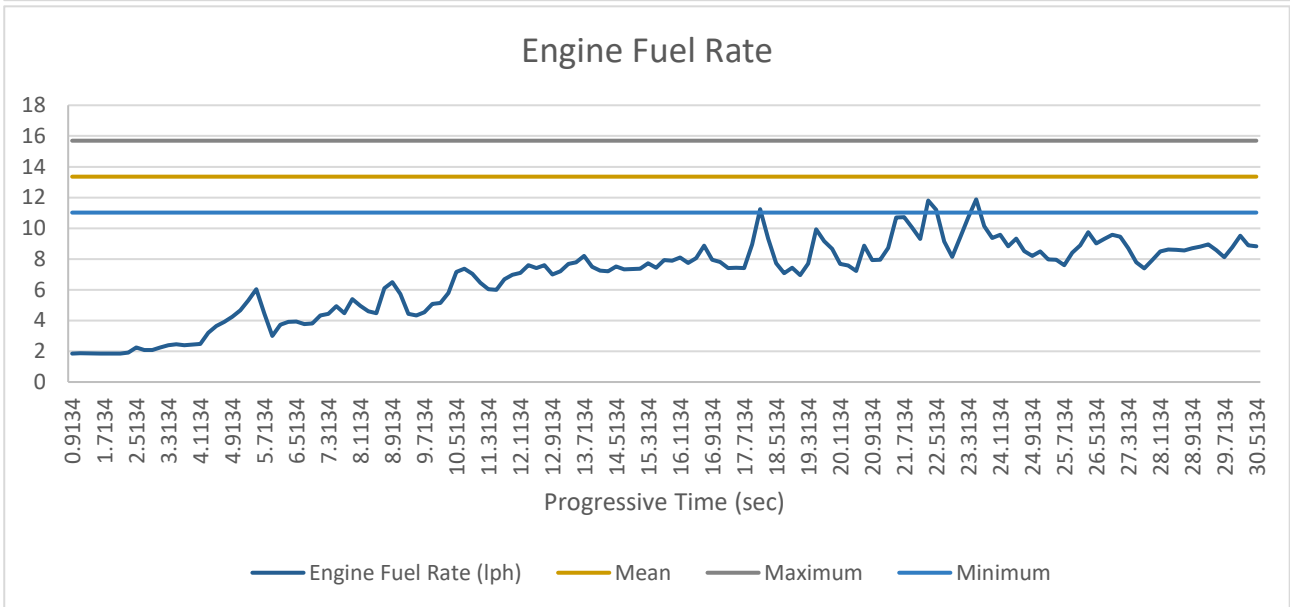
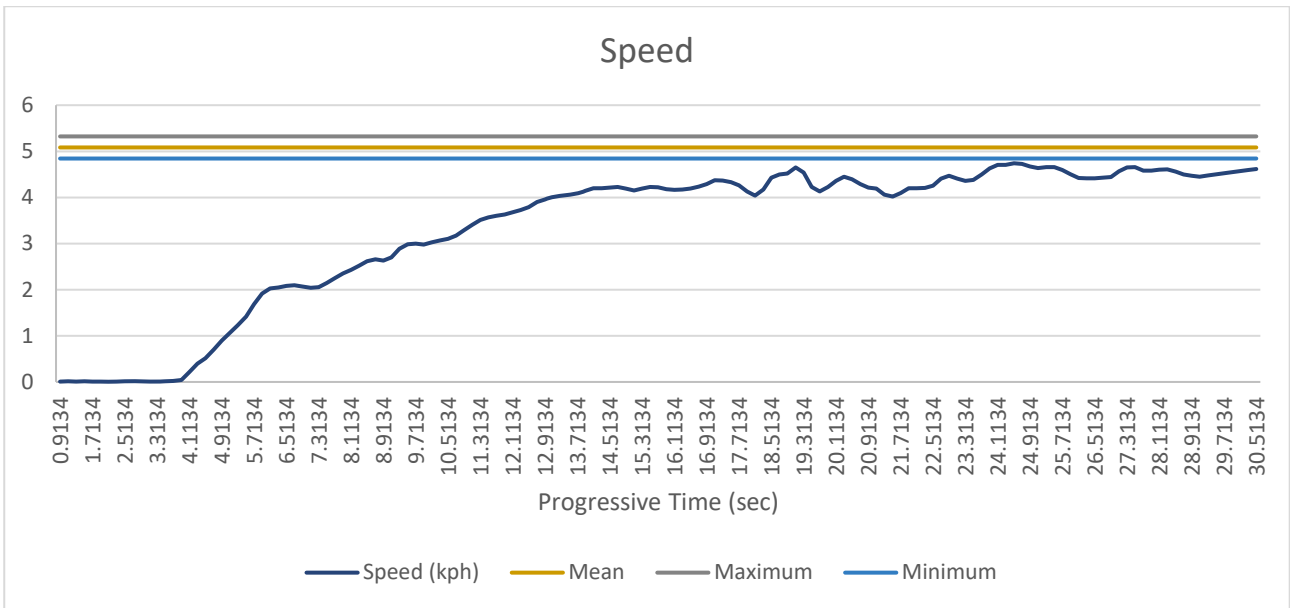


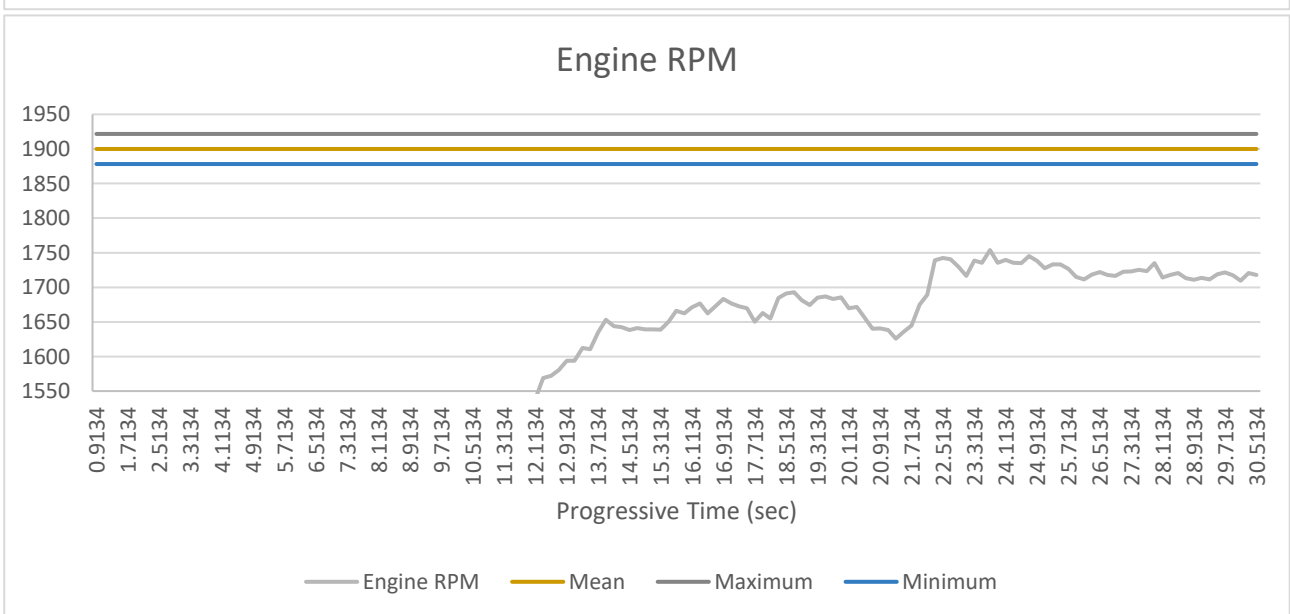
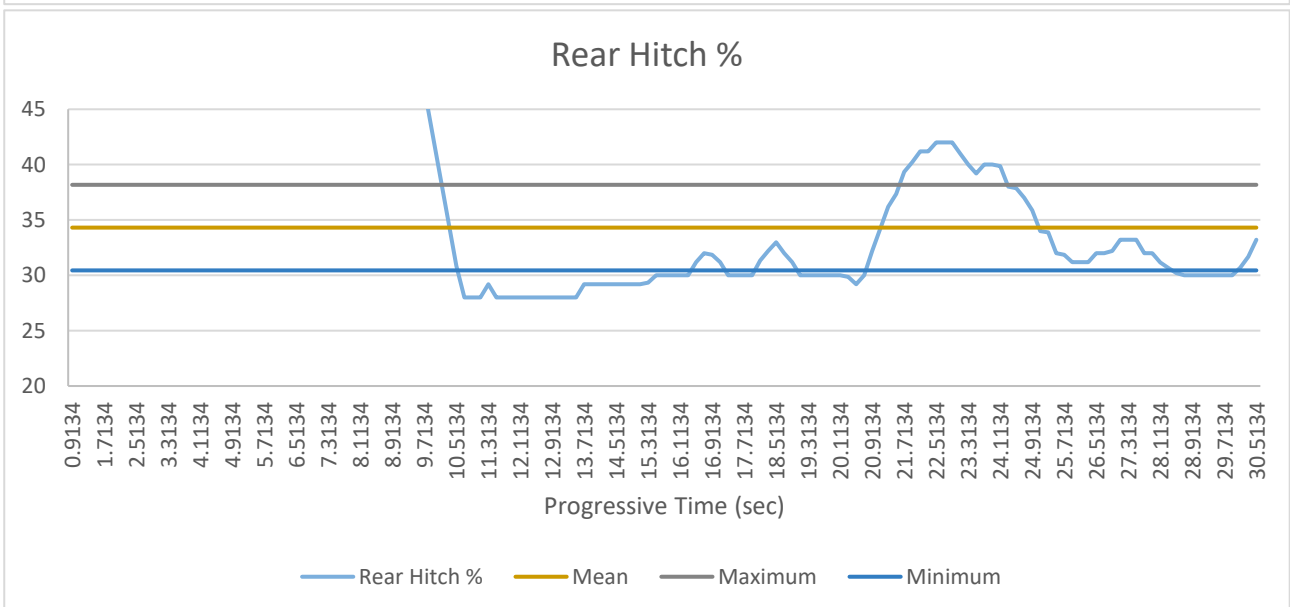
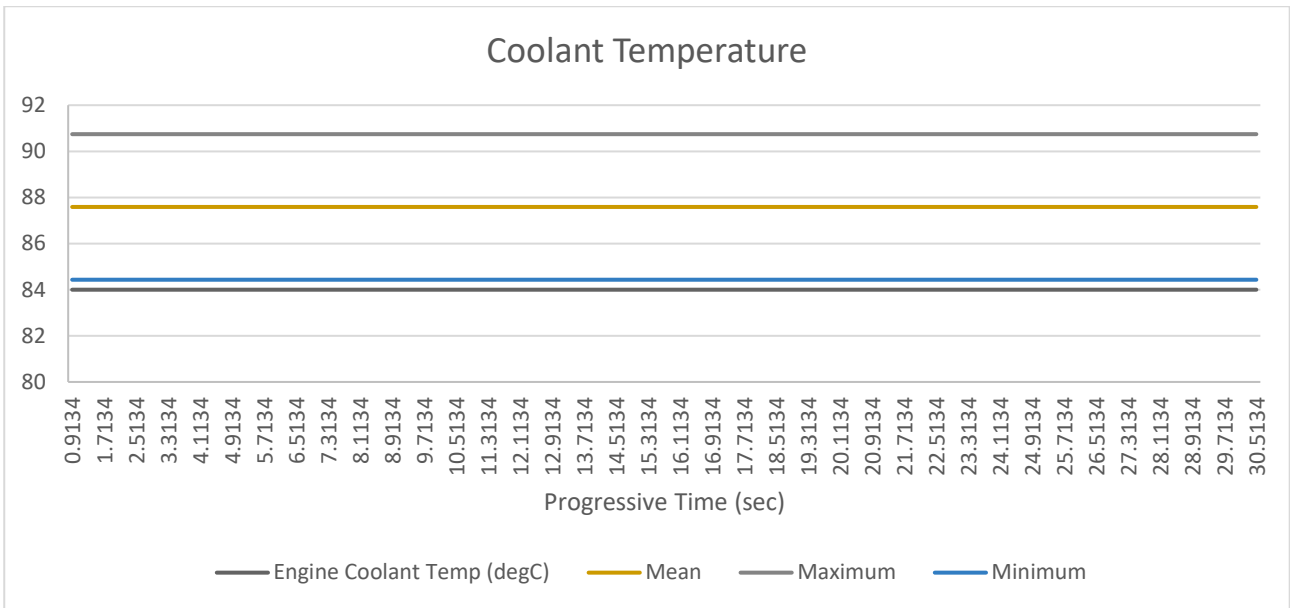




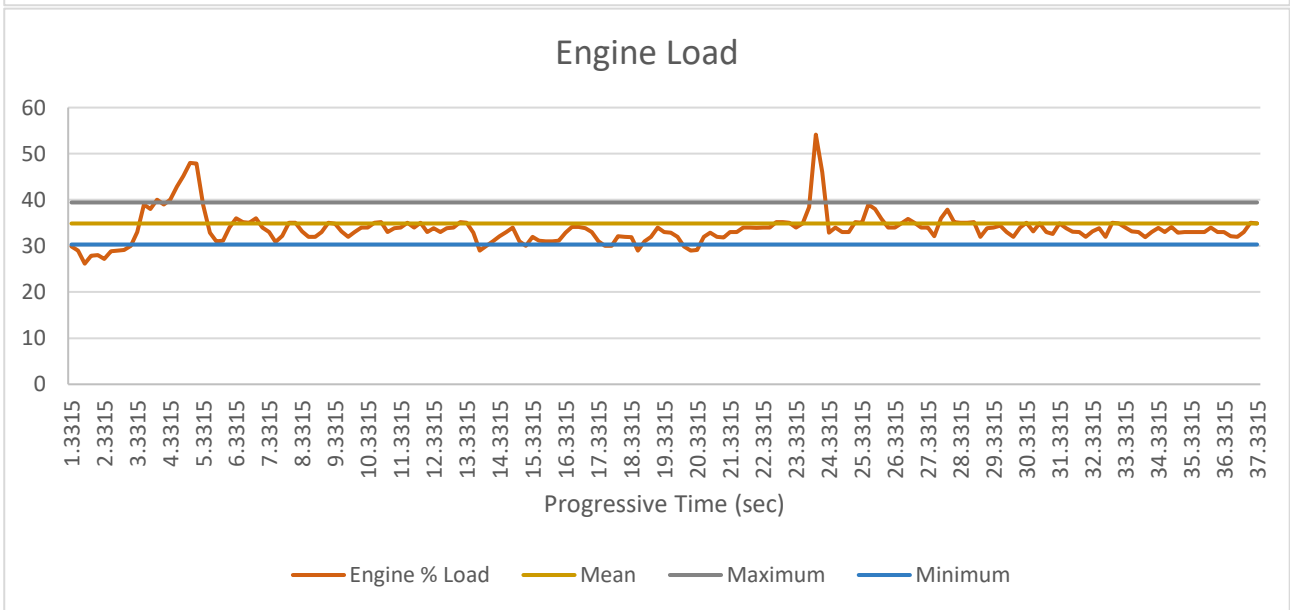
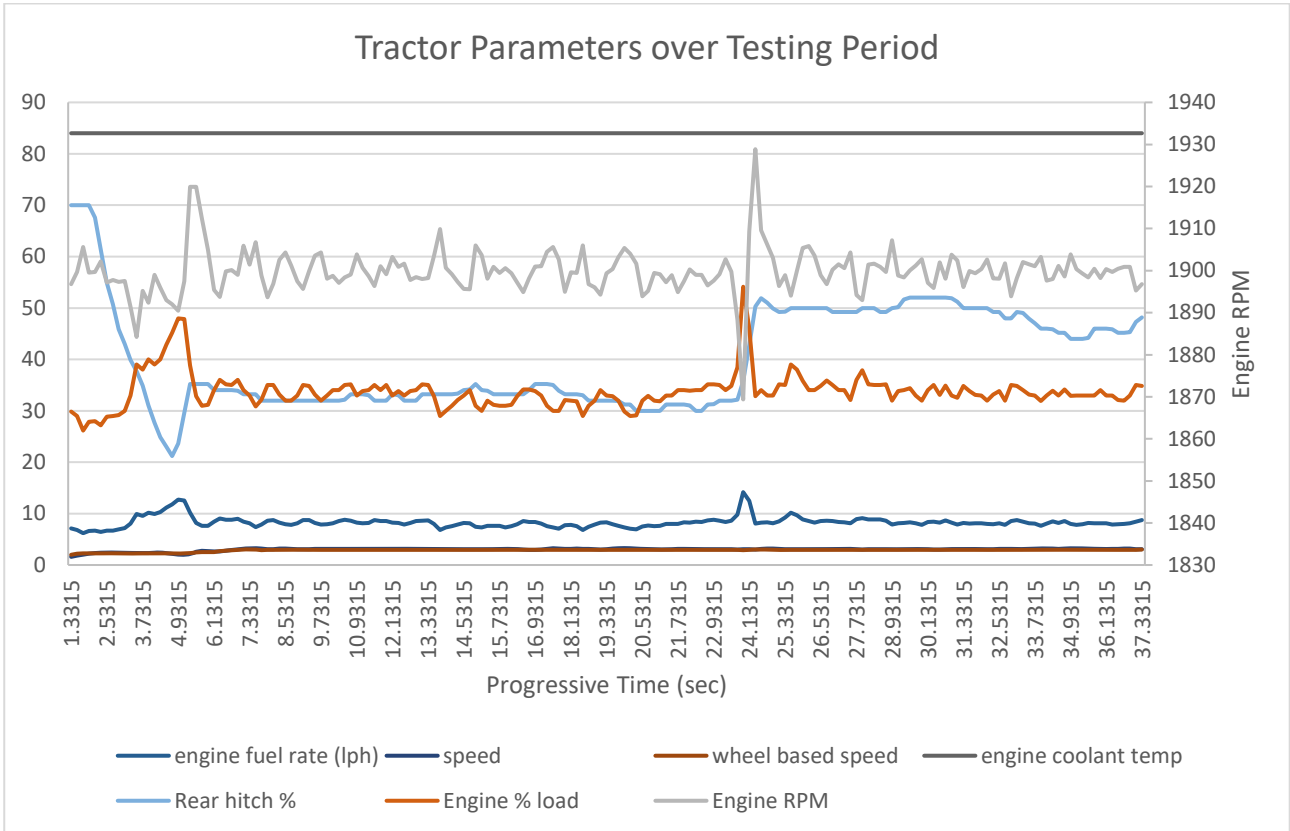
300mm – 5kph

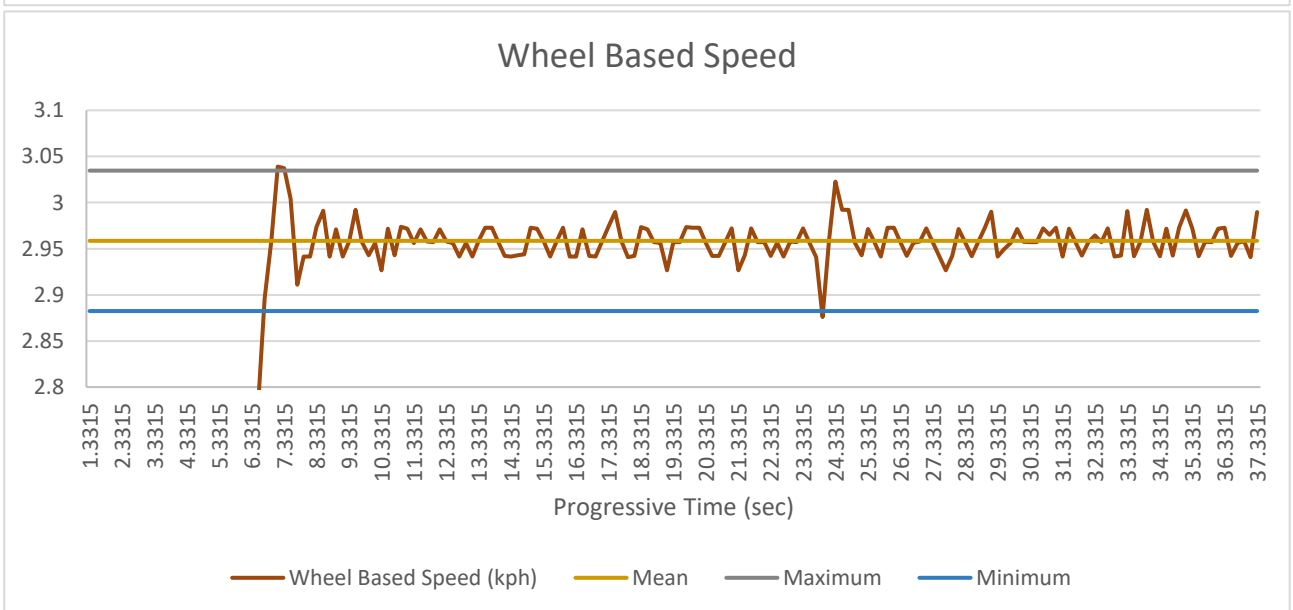
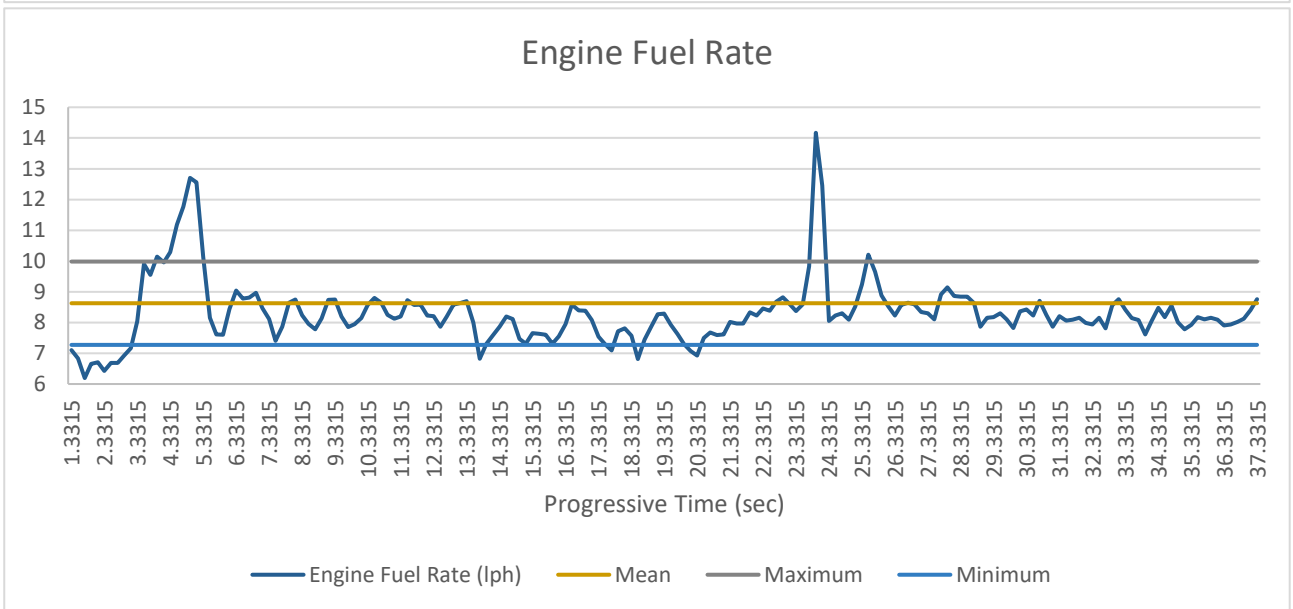
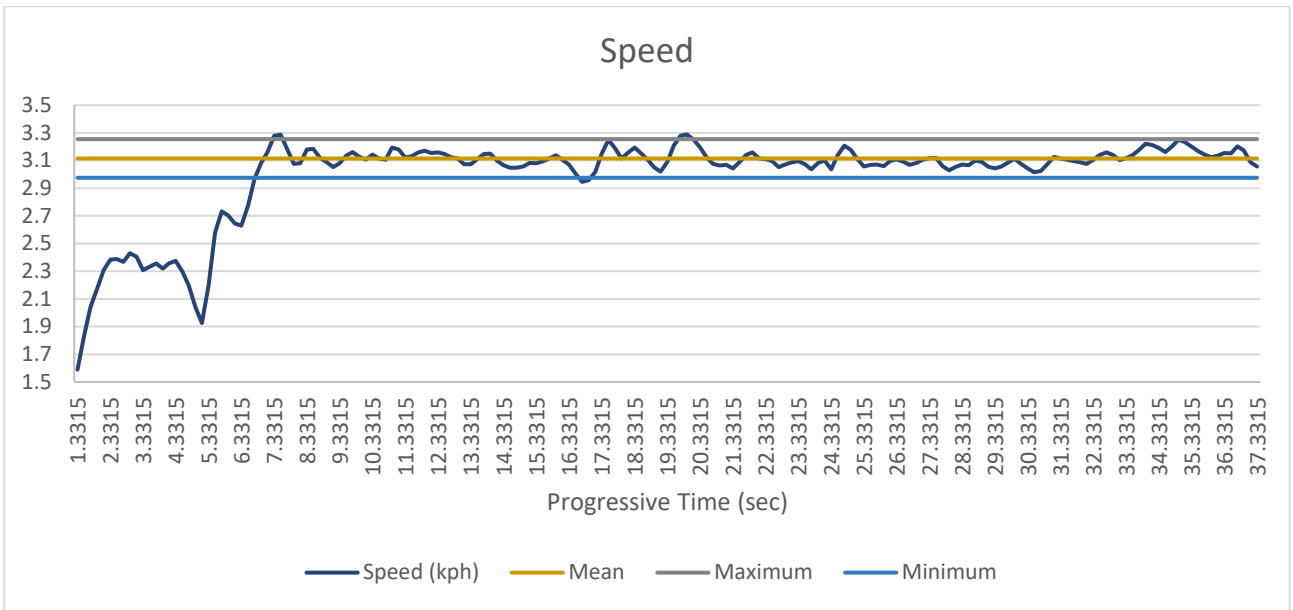


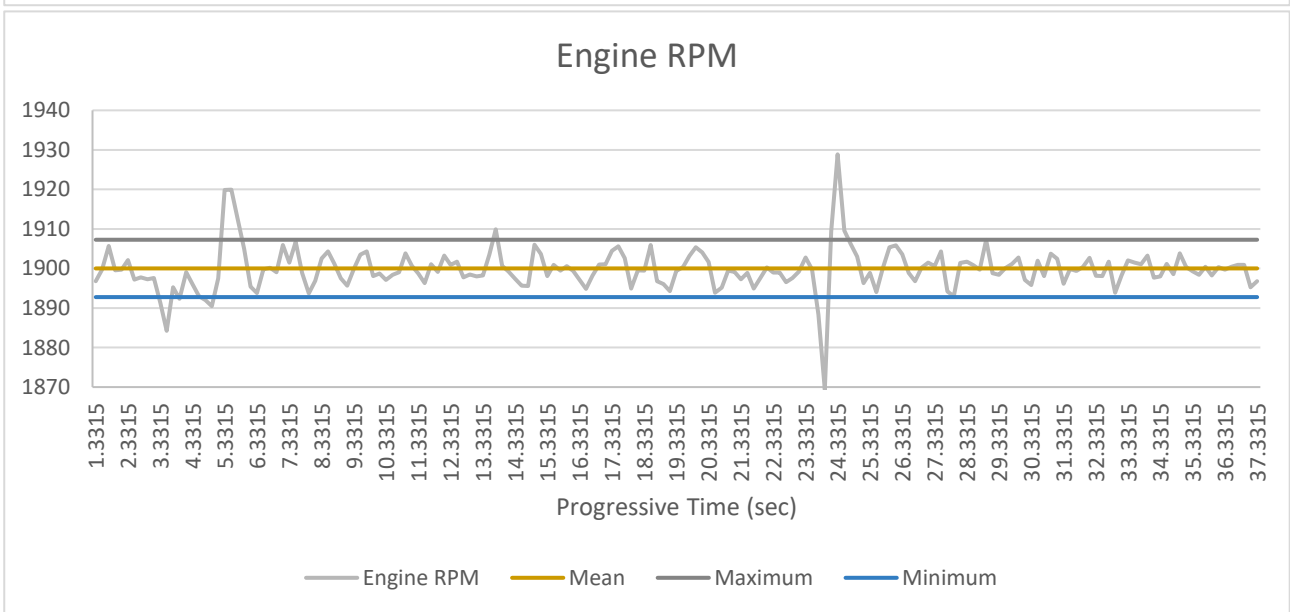
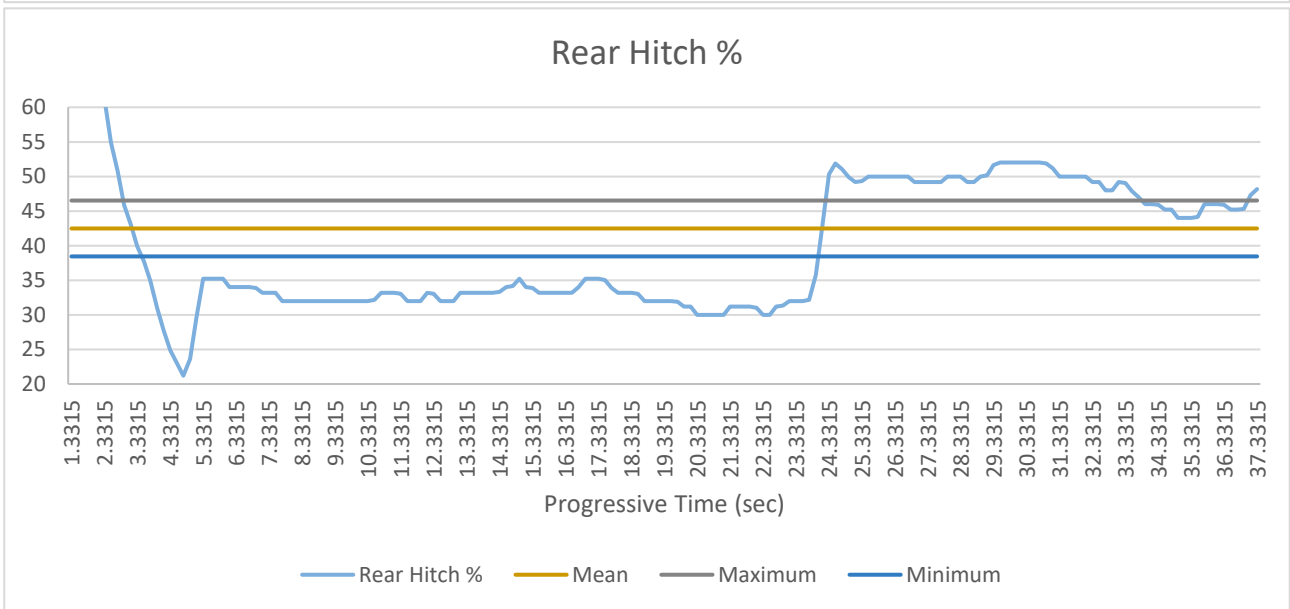
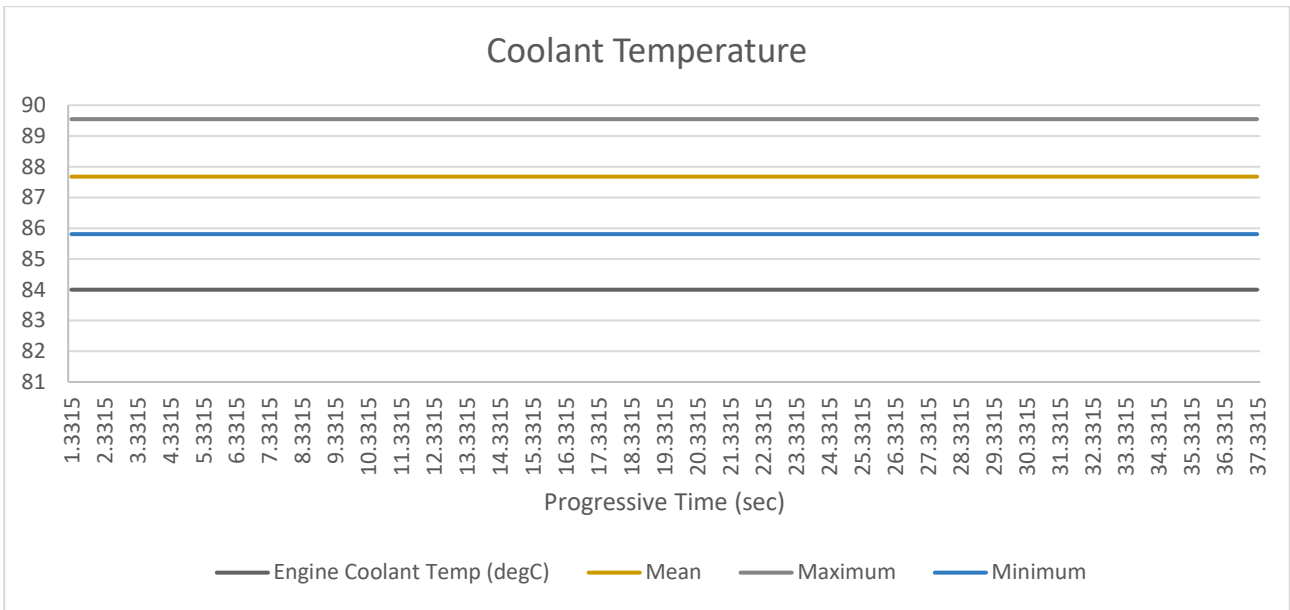




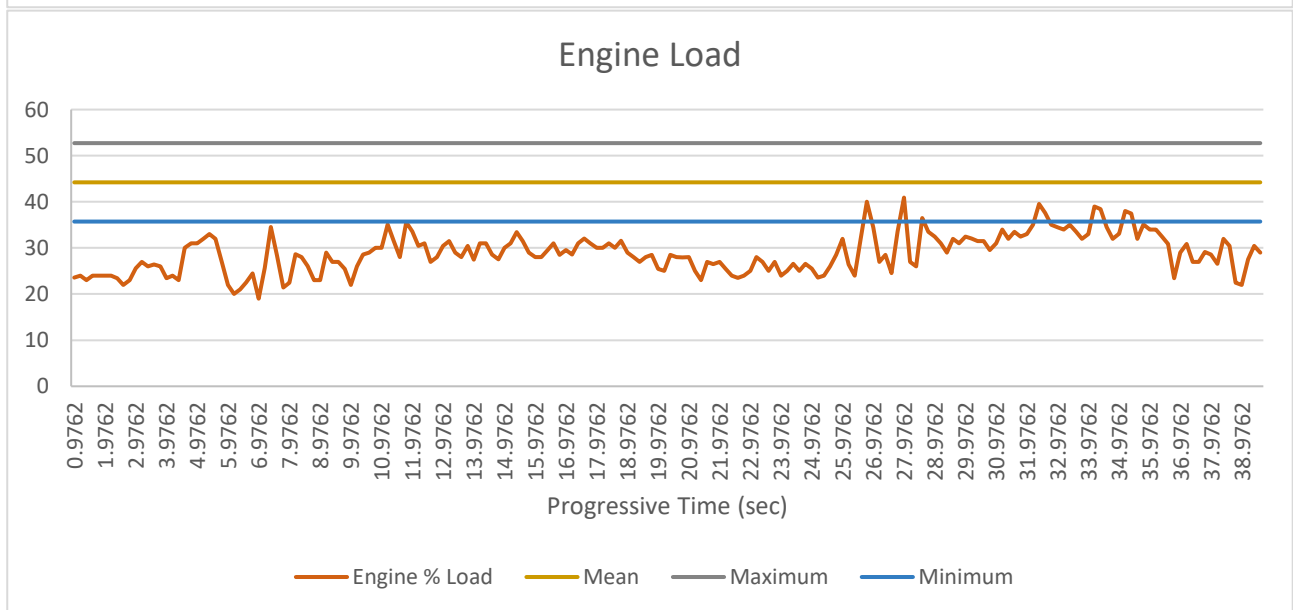
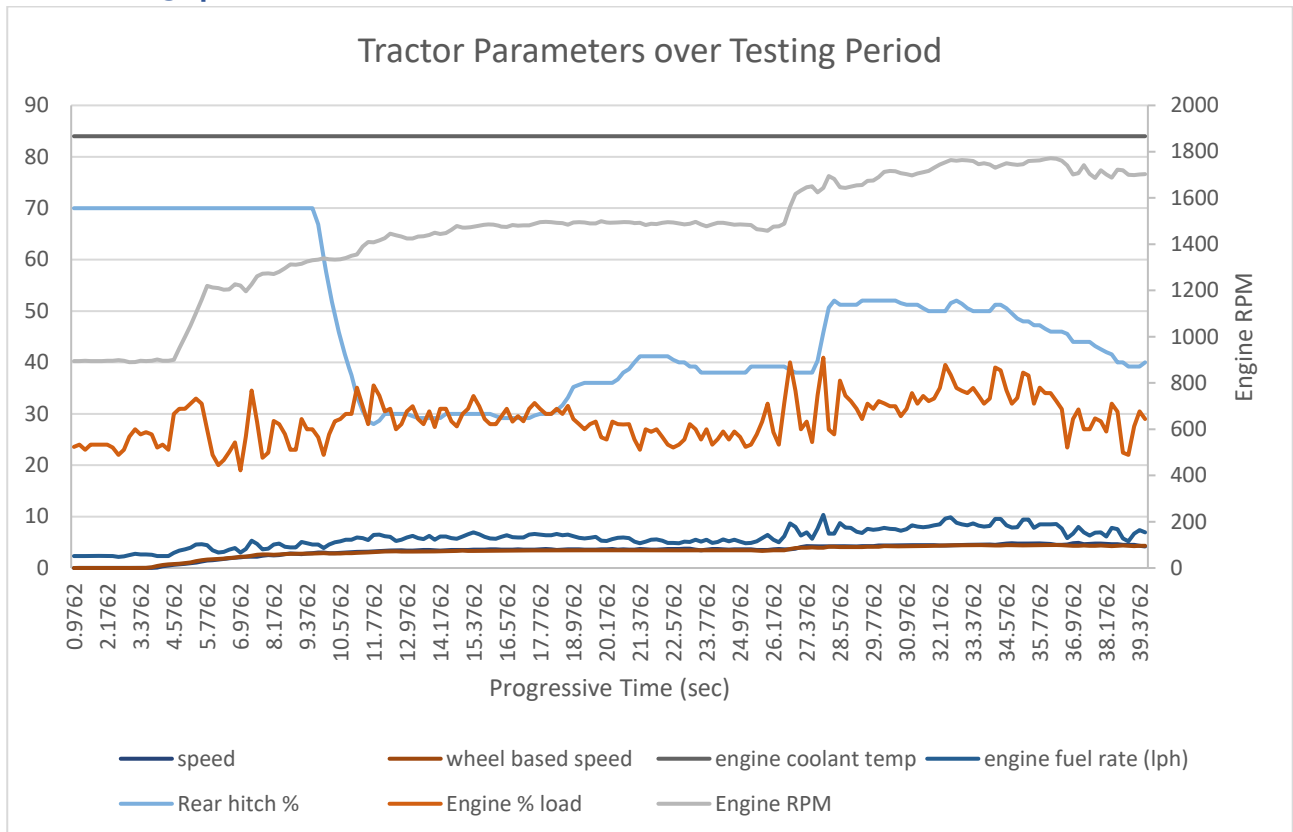
200mm – 3kph

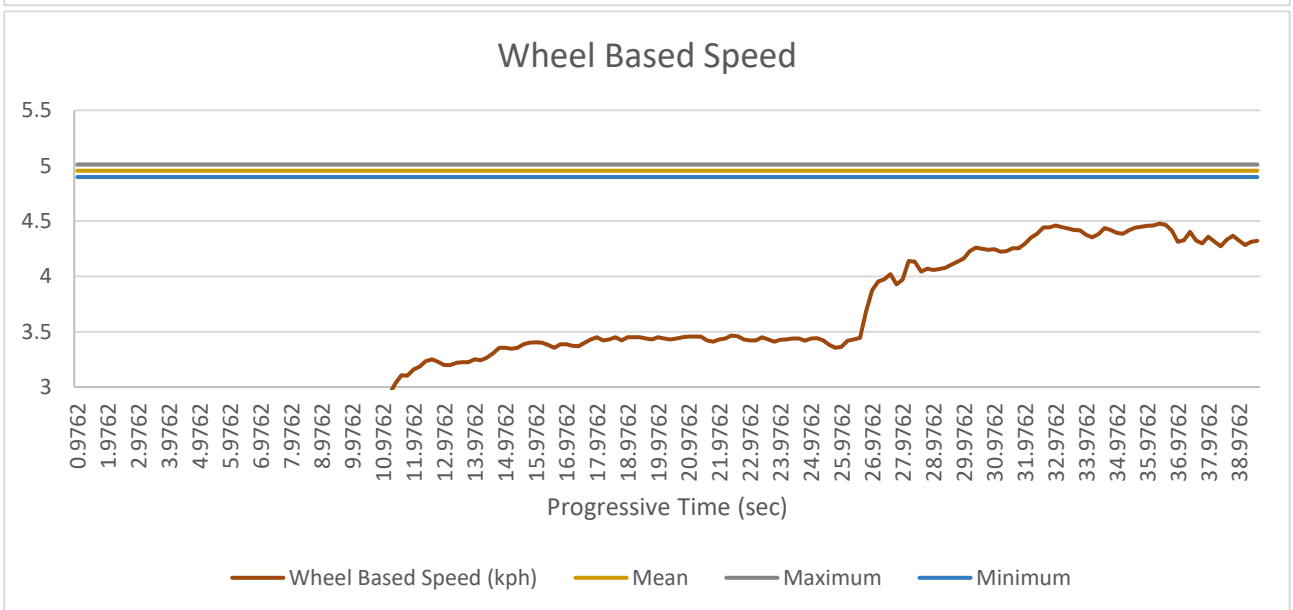
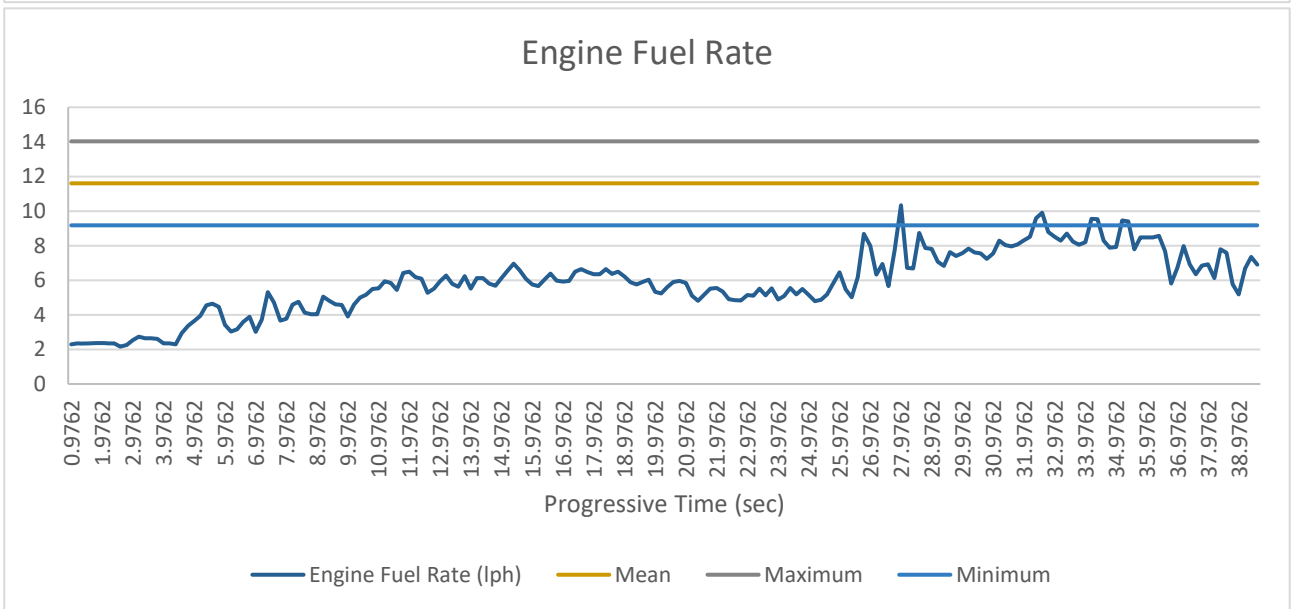
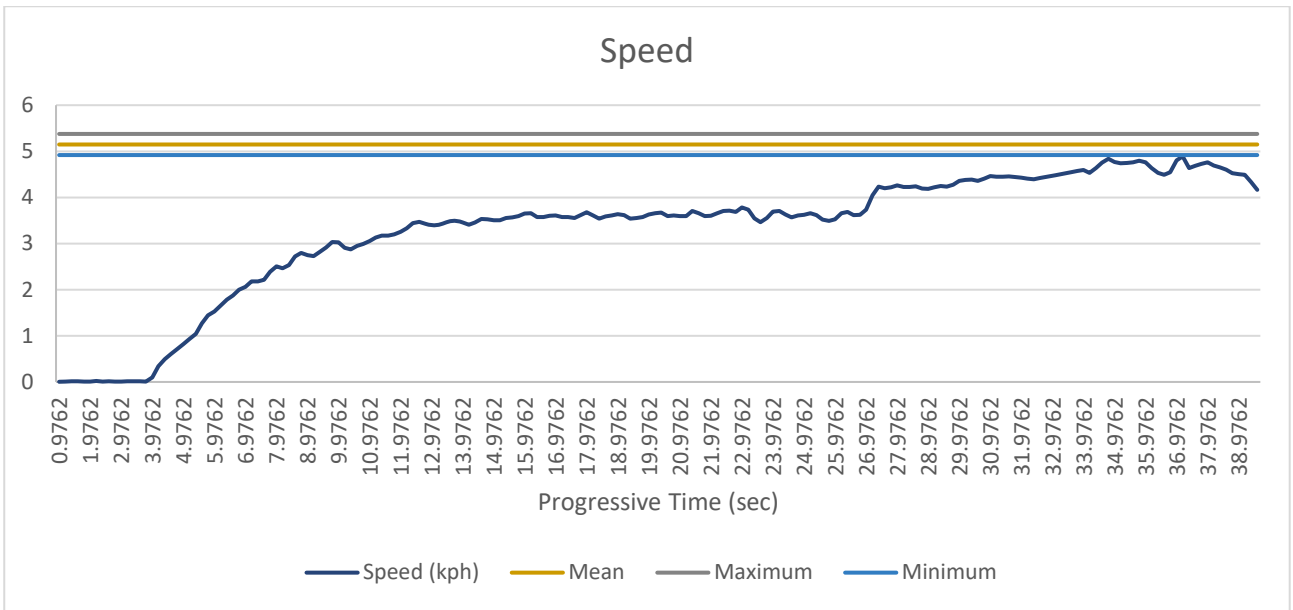


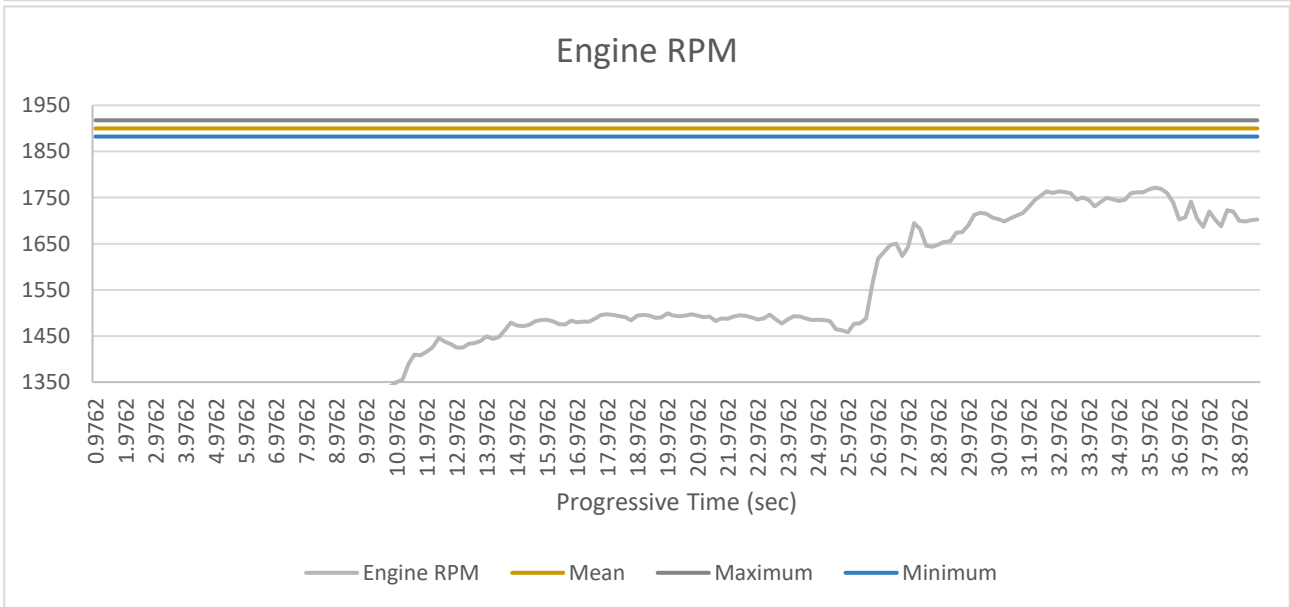
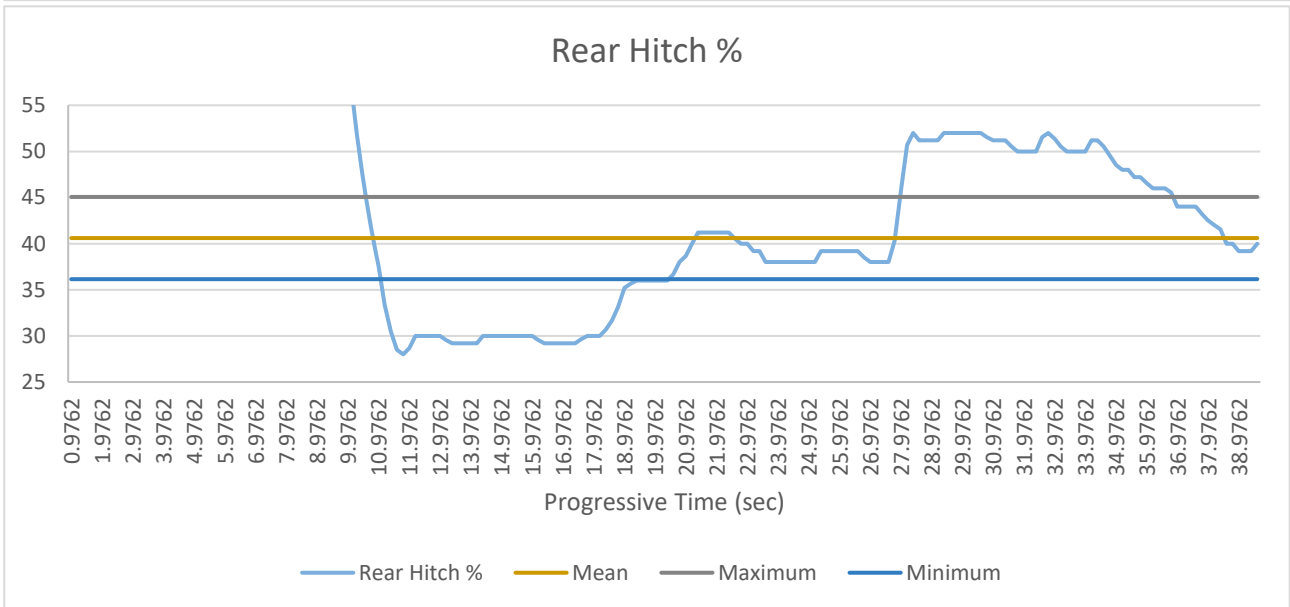
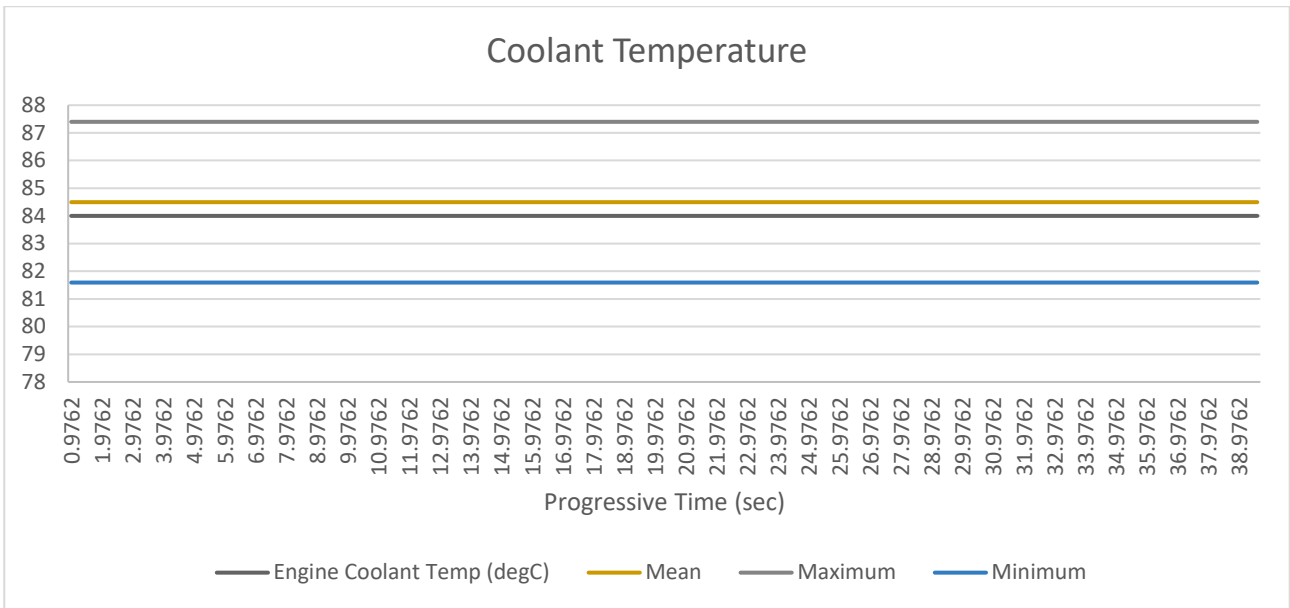




200mm – 5kph

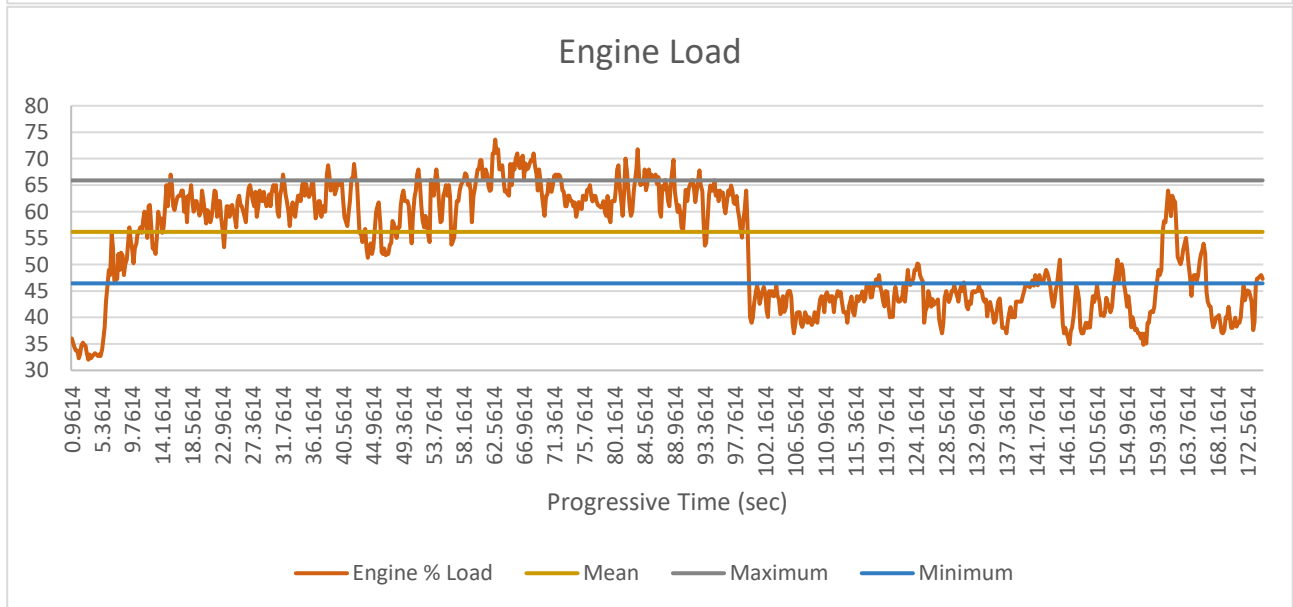
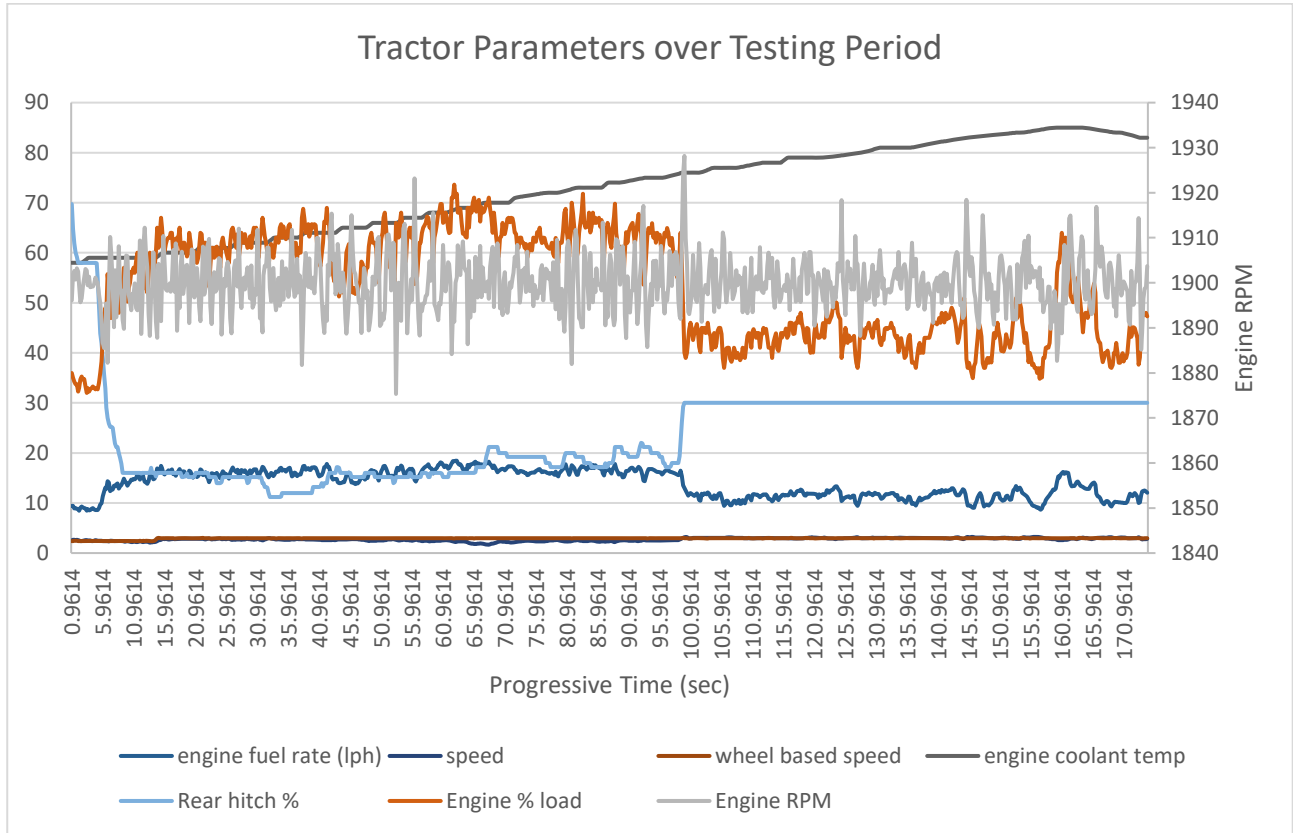


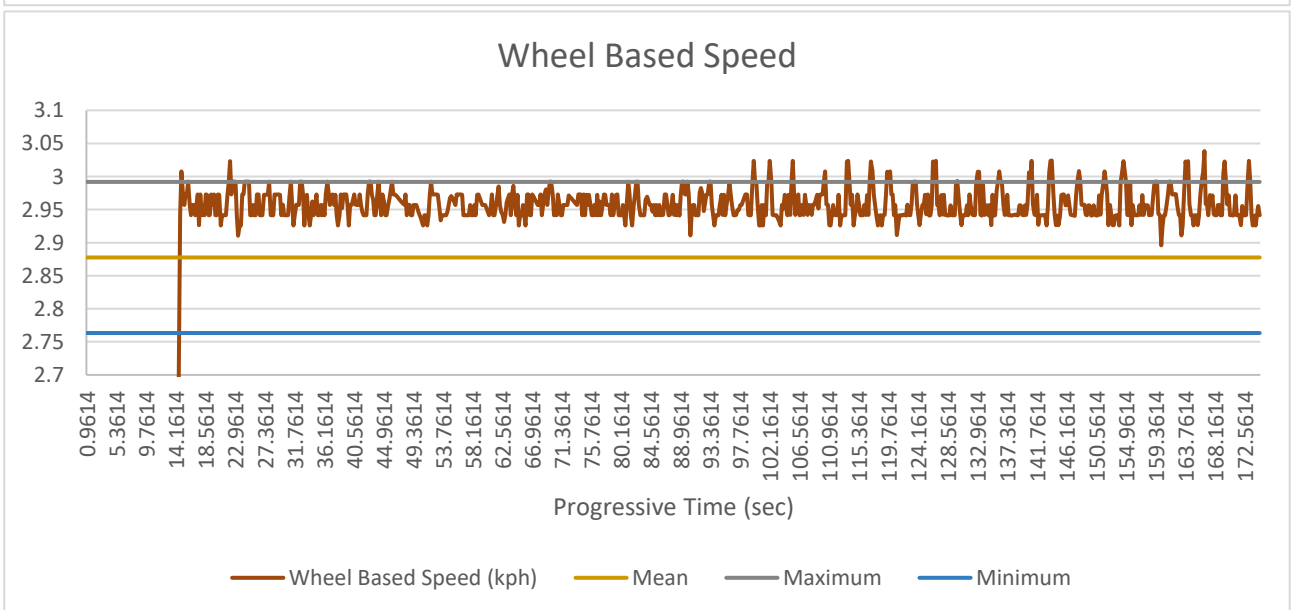
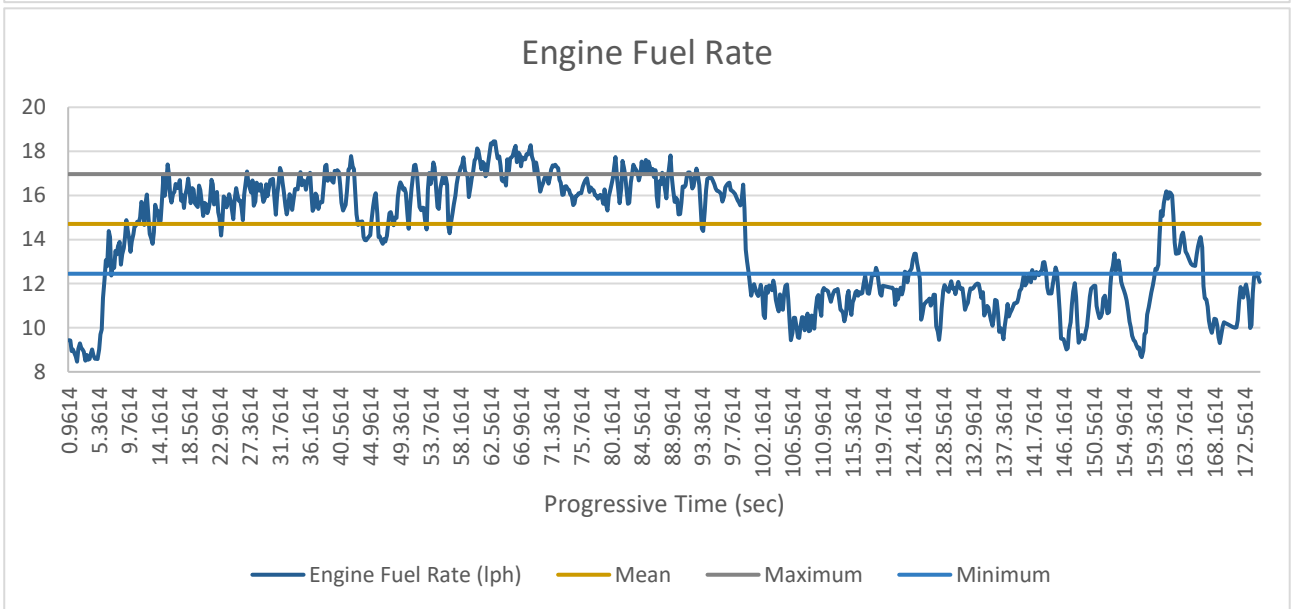
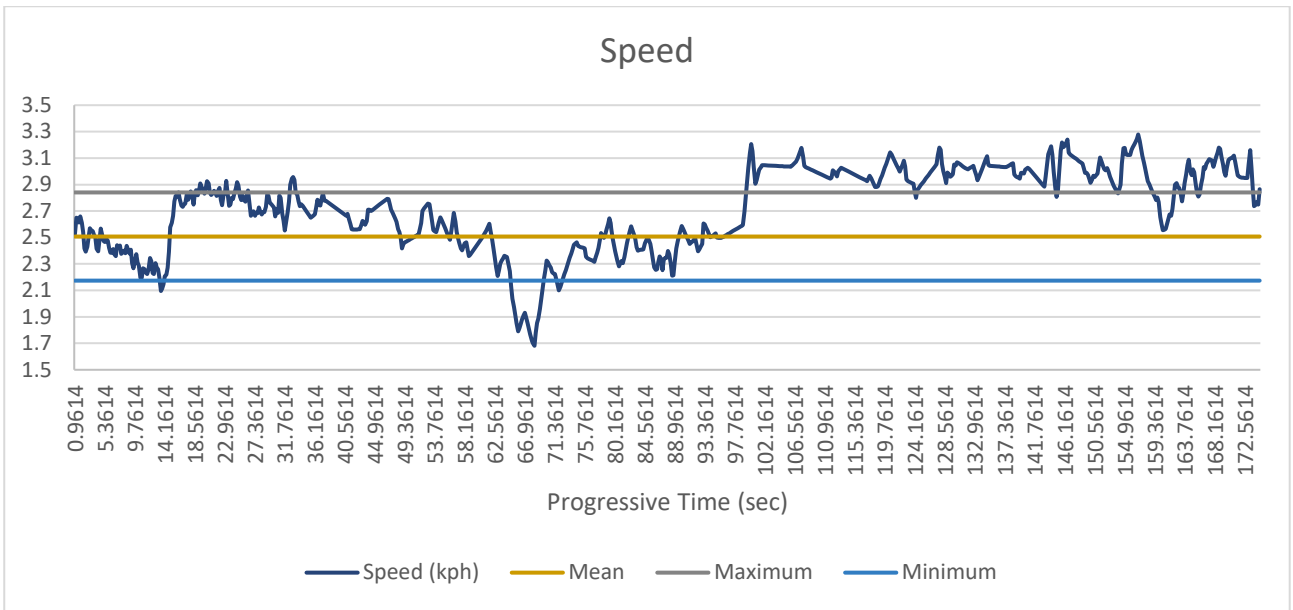


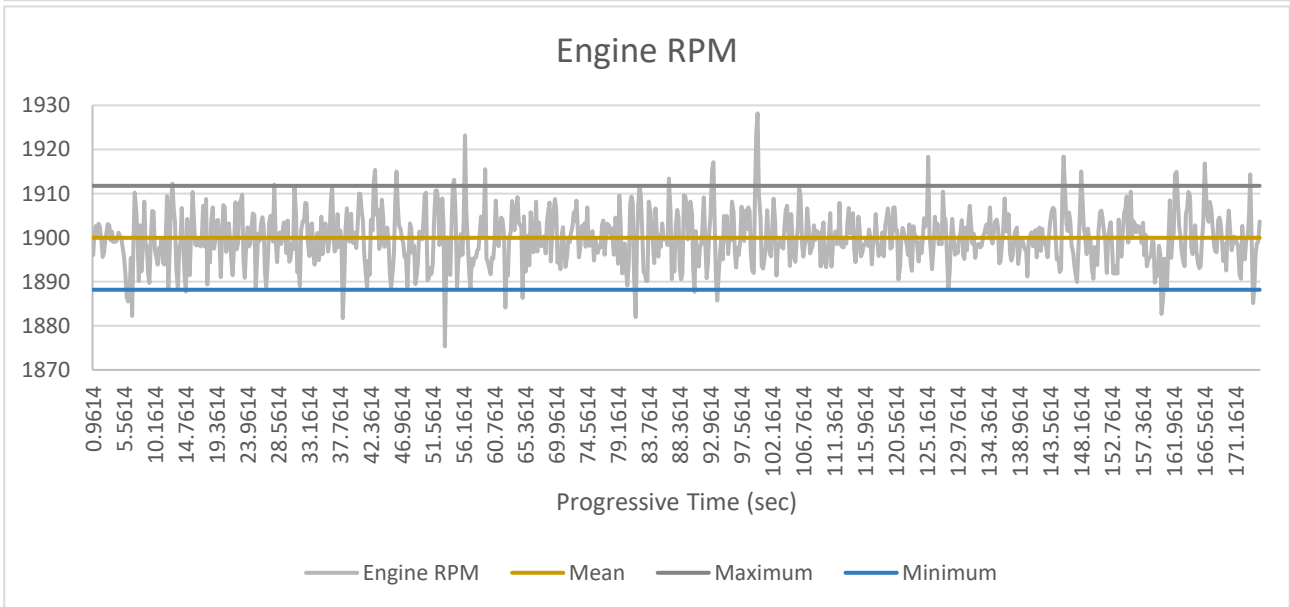
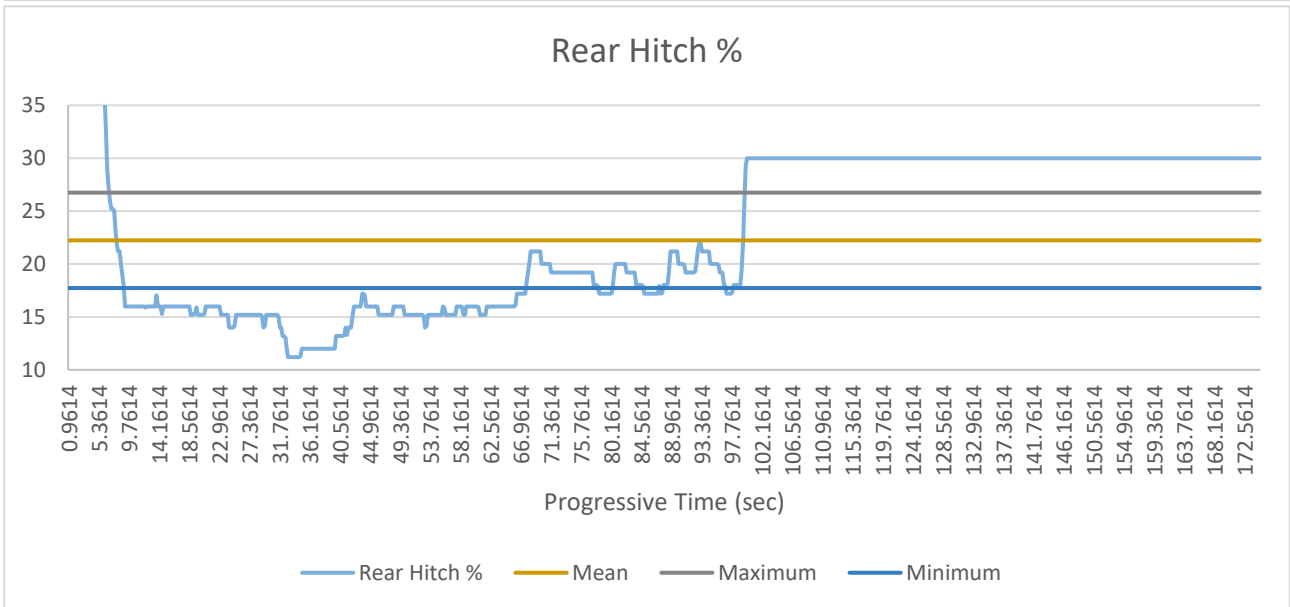
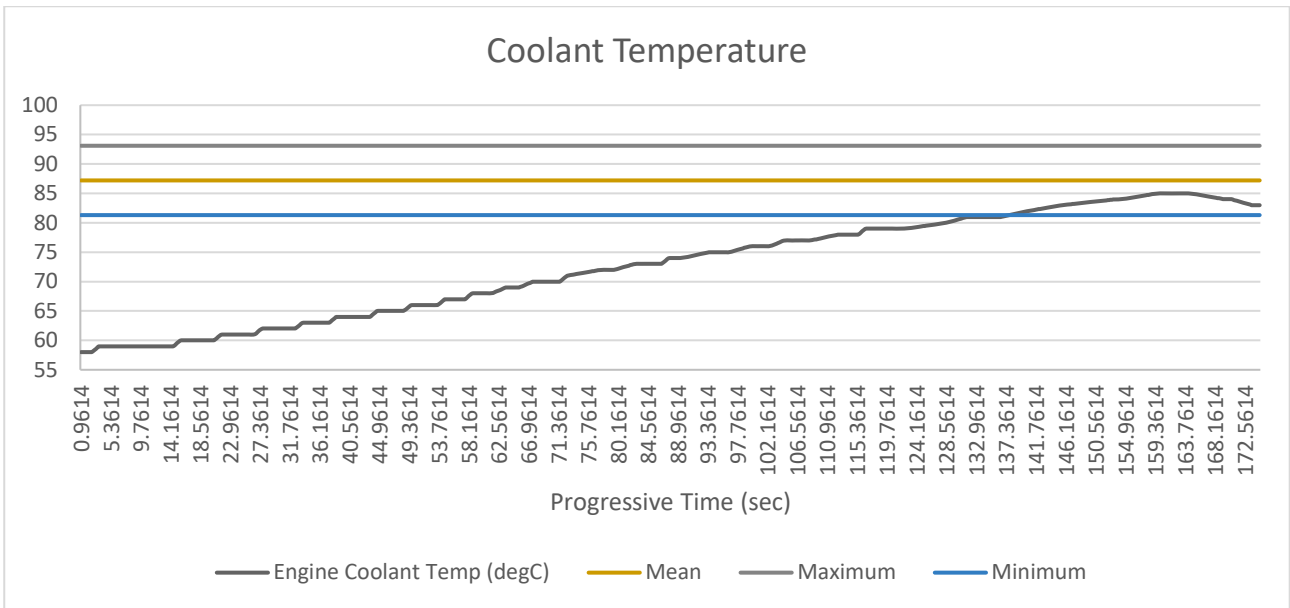


Appendix J – 3PL Deep Ripper – Ripper not digging in far enough data

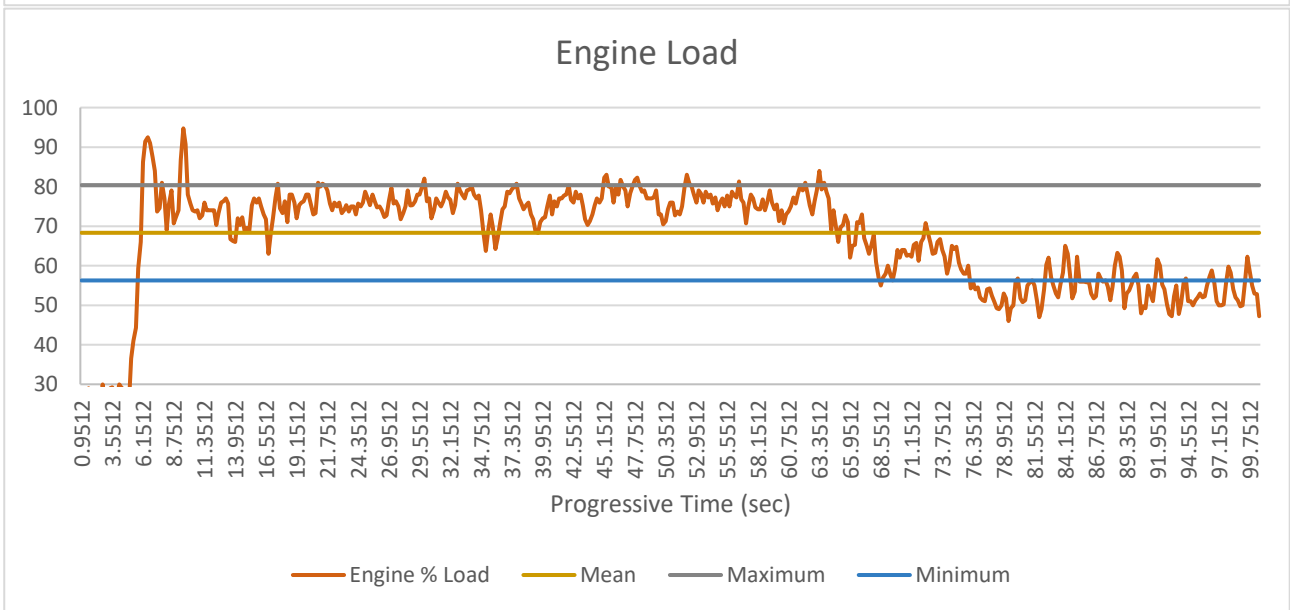
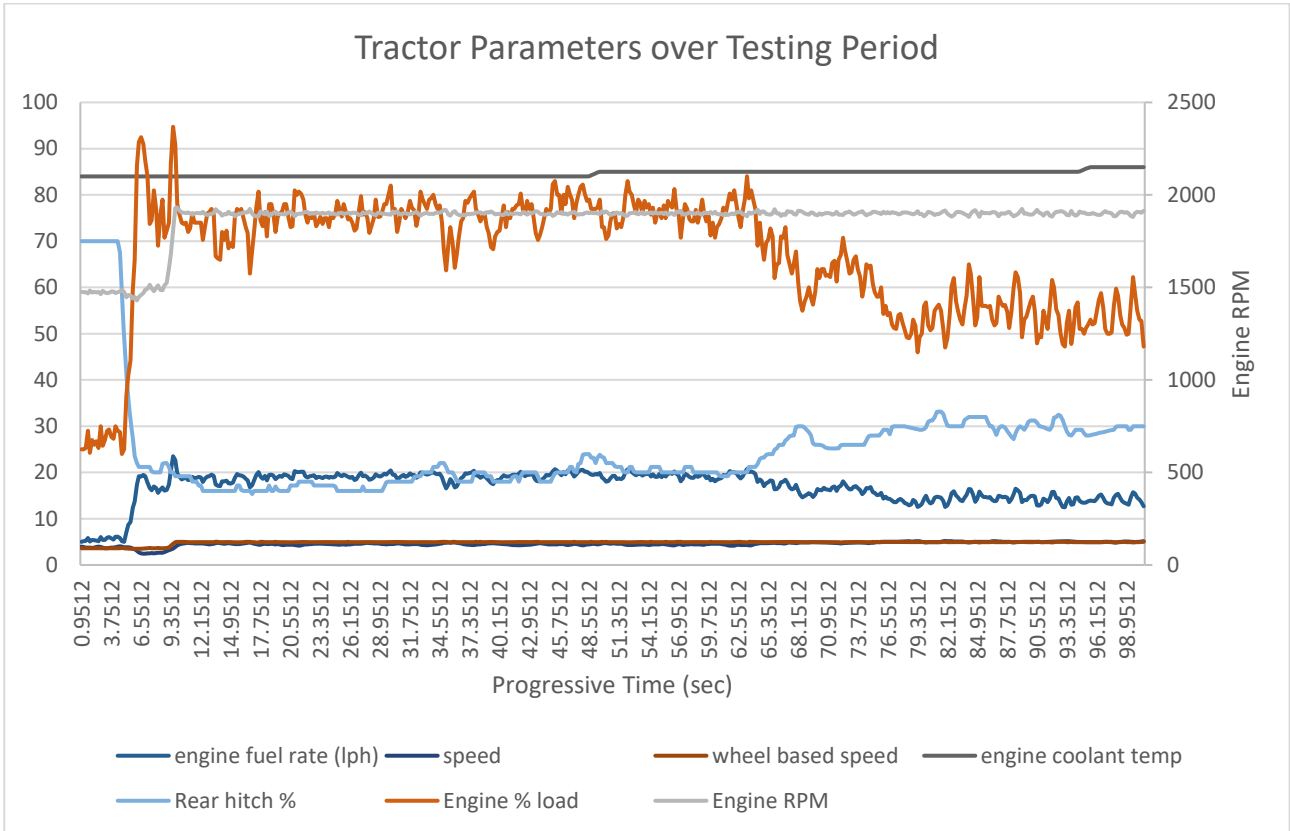
350mm – 3kph

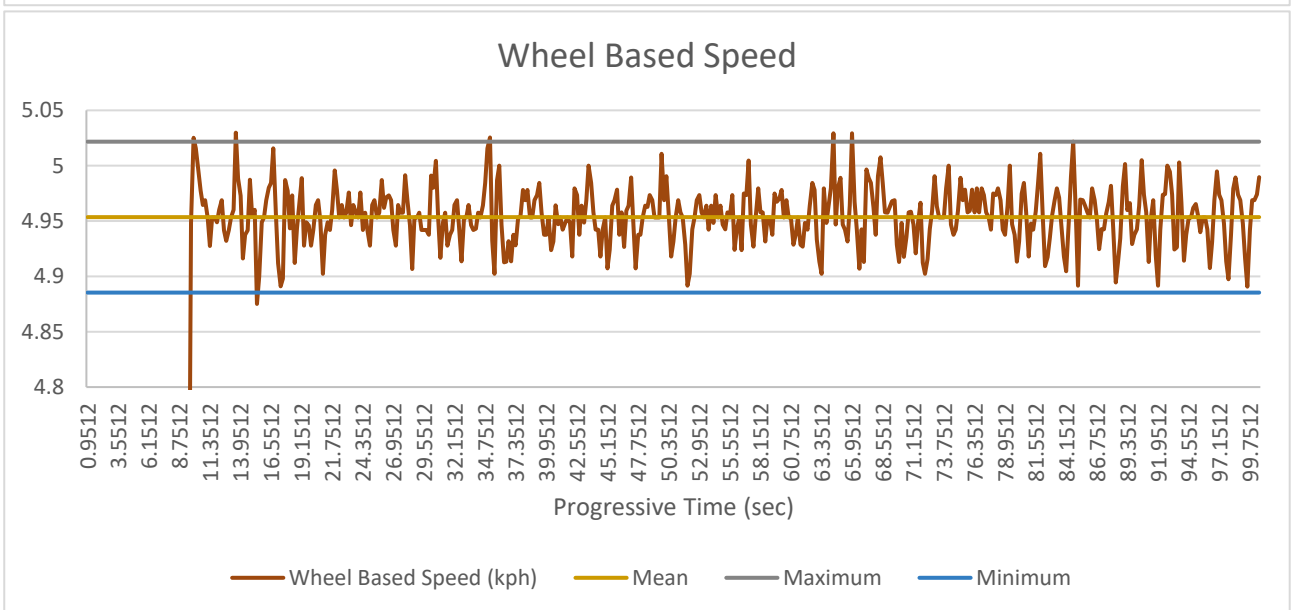
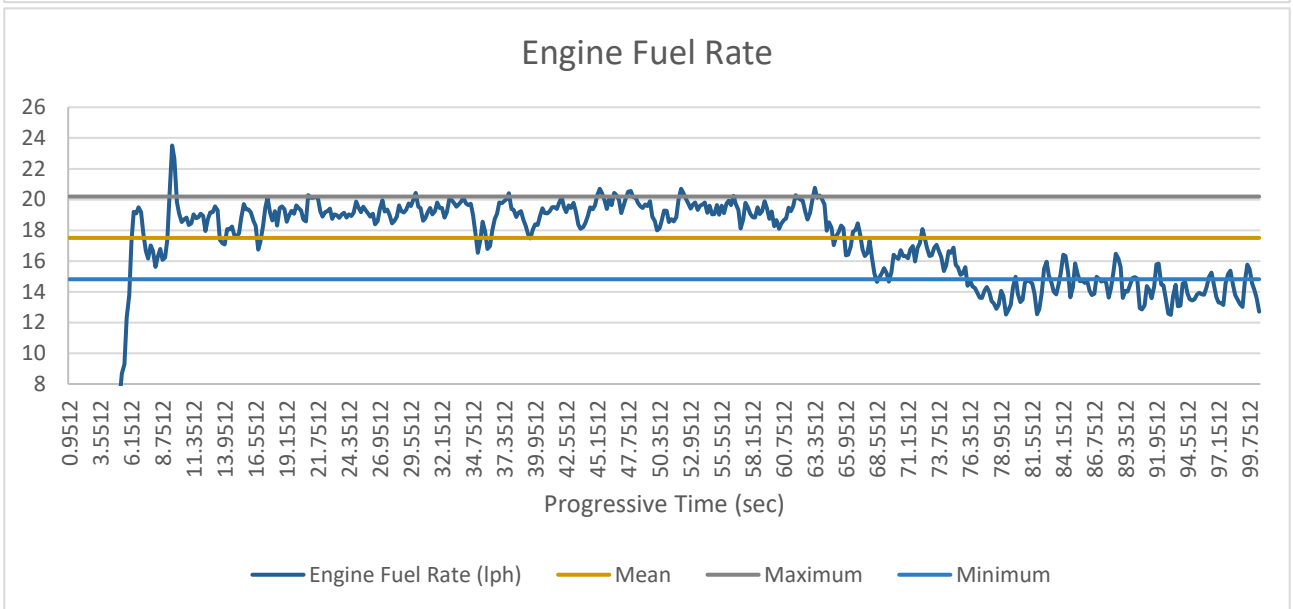
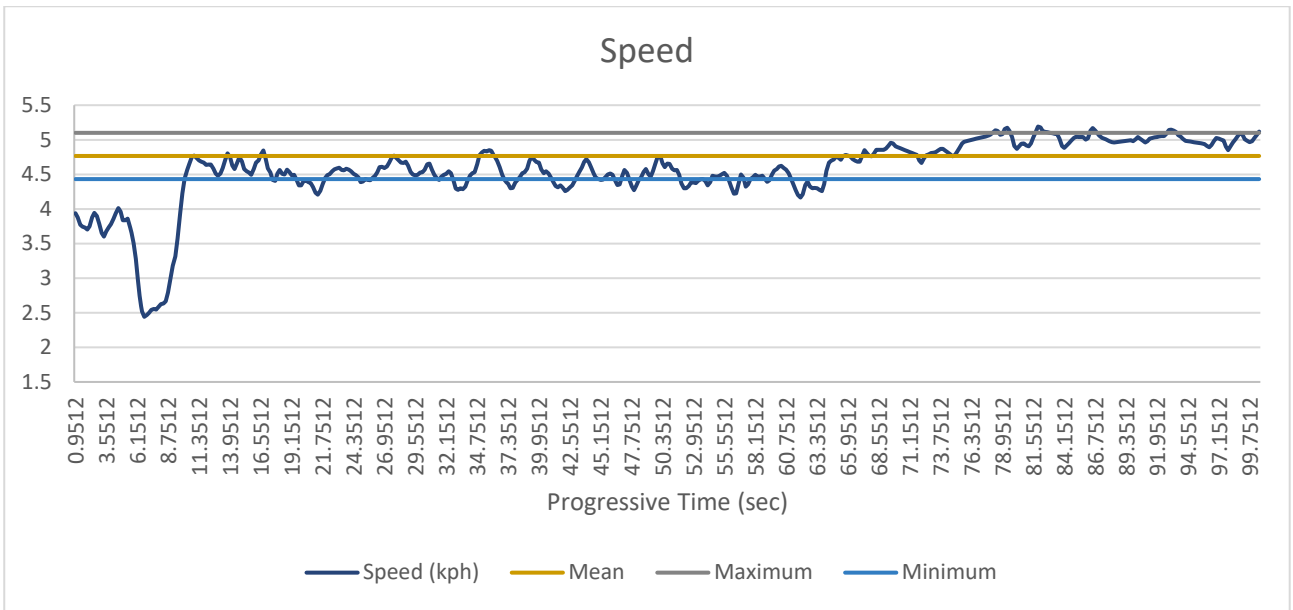




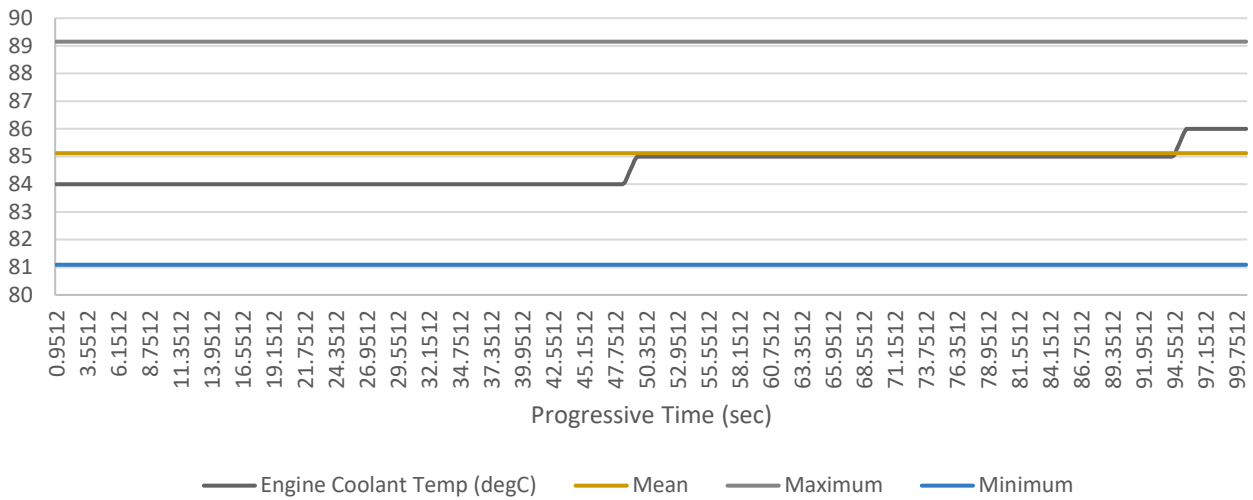


350mm – 5kph

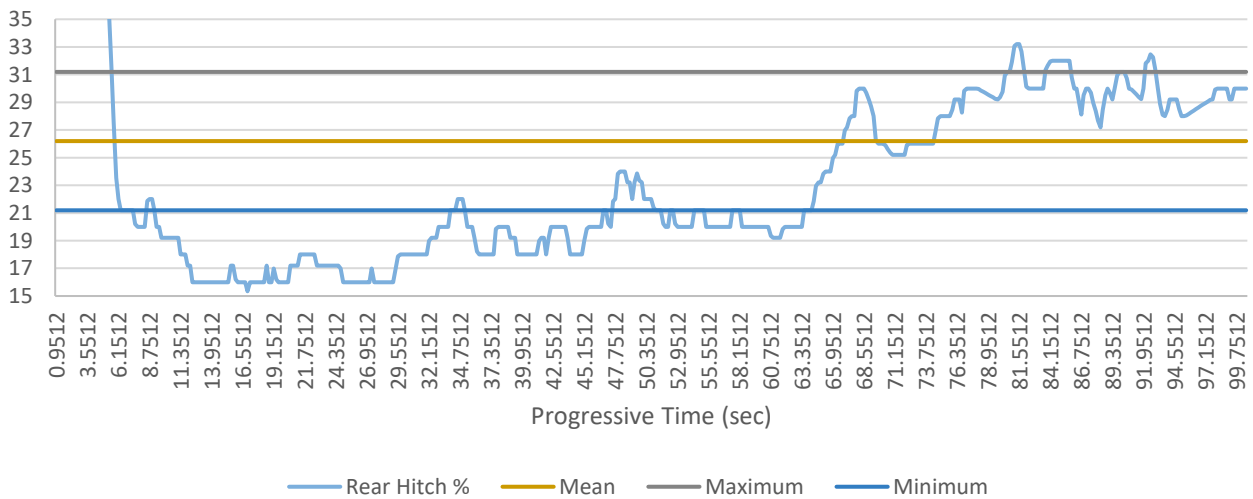




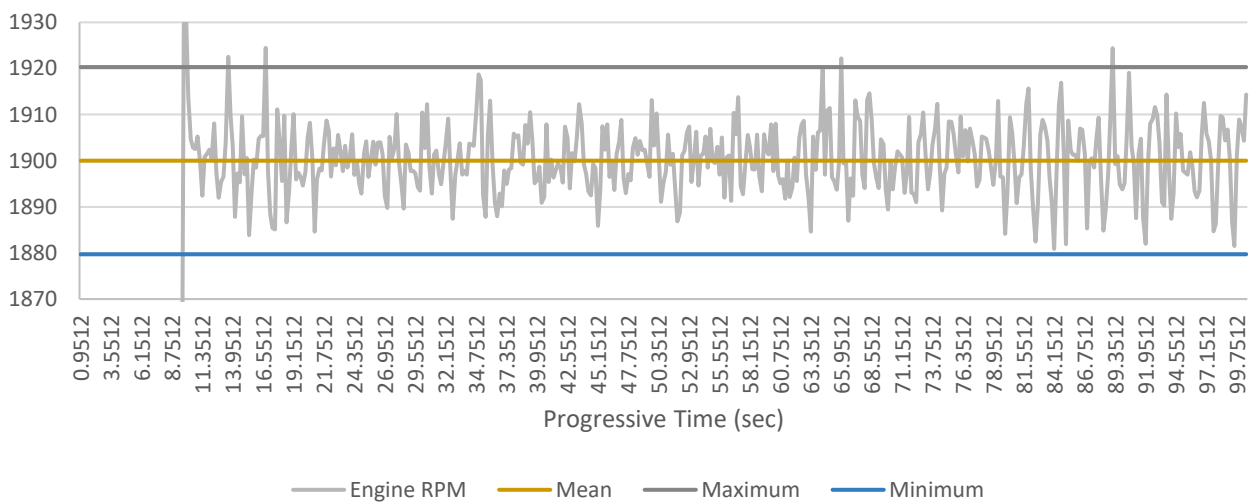
Coolant Temperature



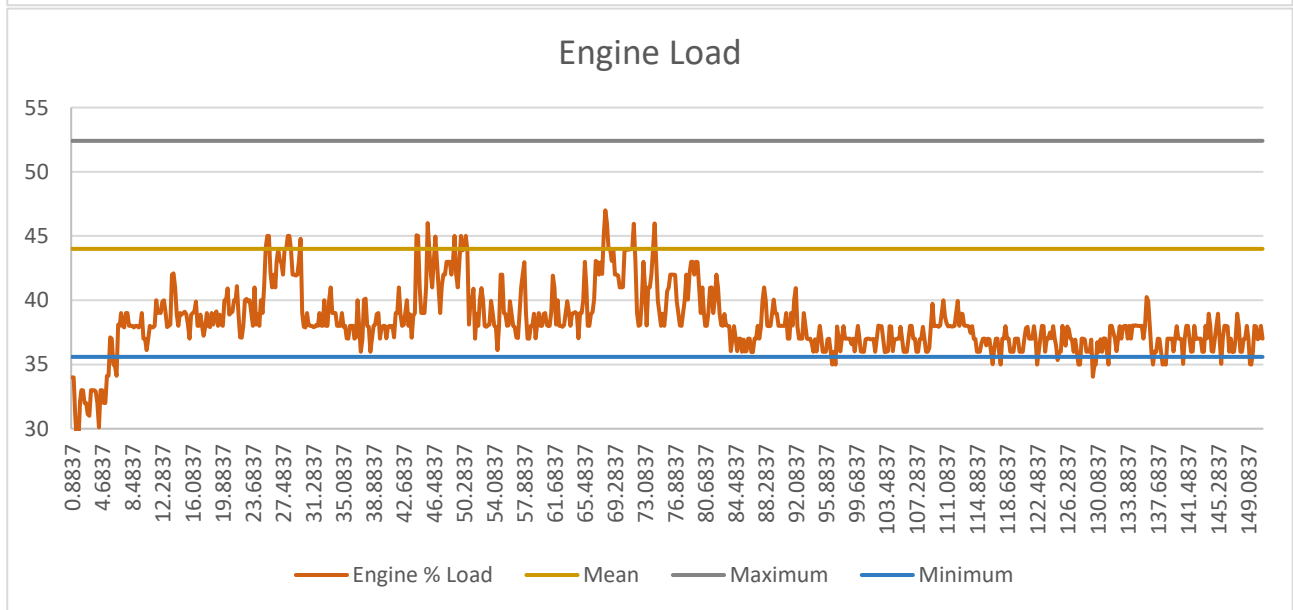
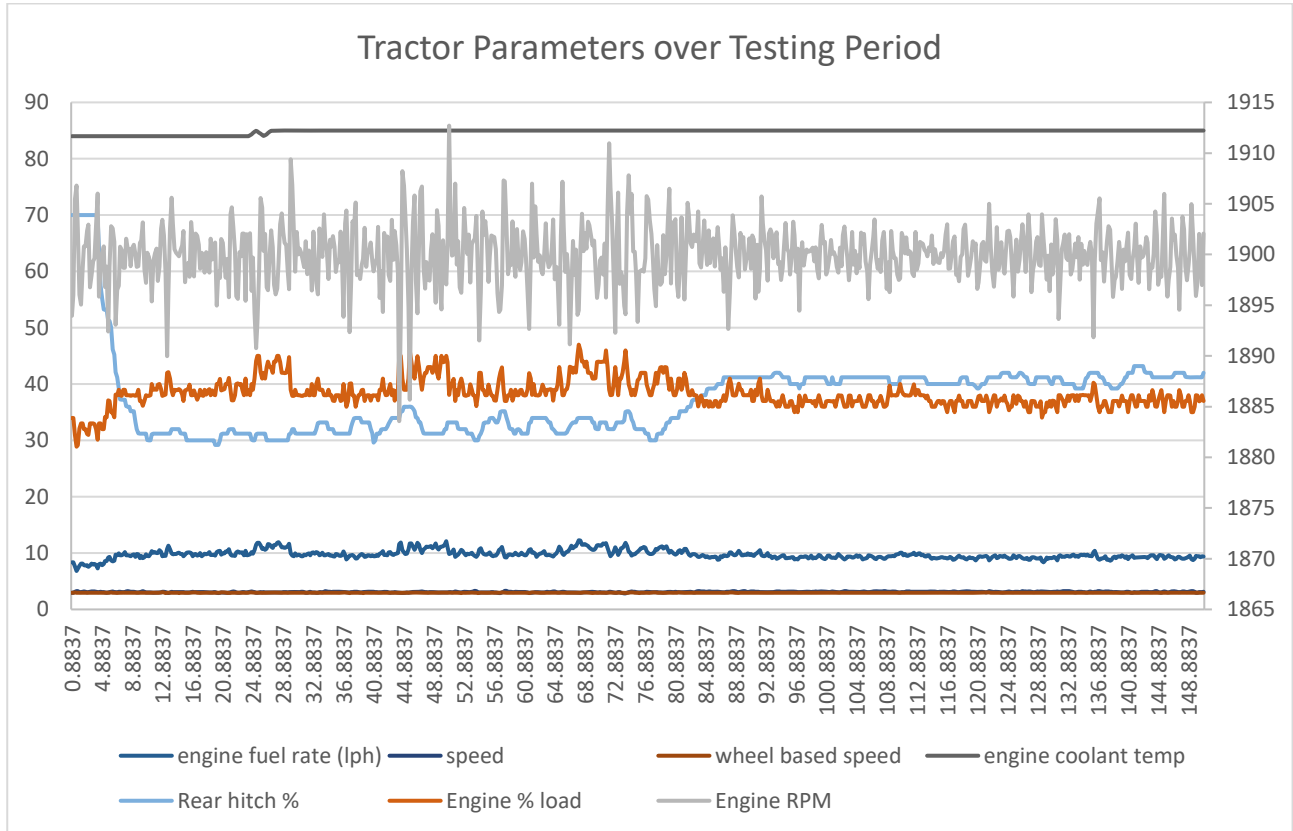
Rear Hitch %

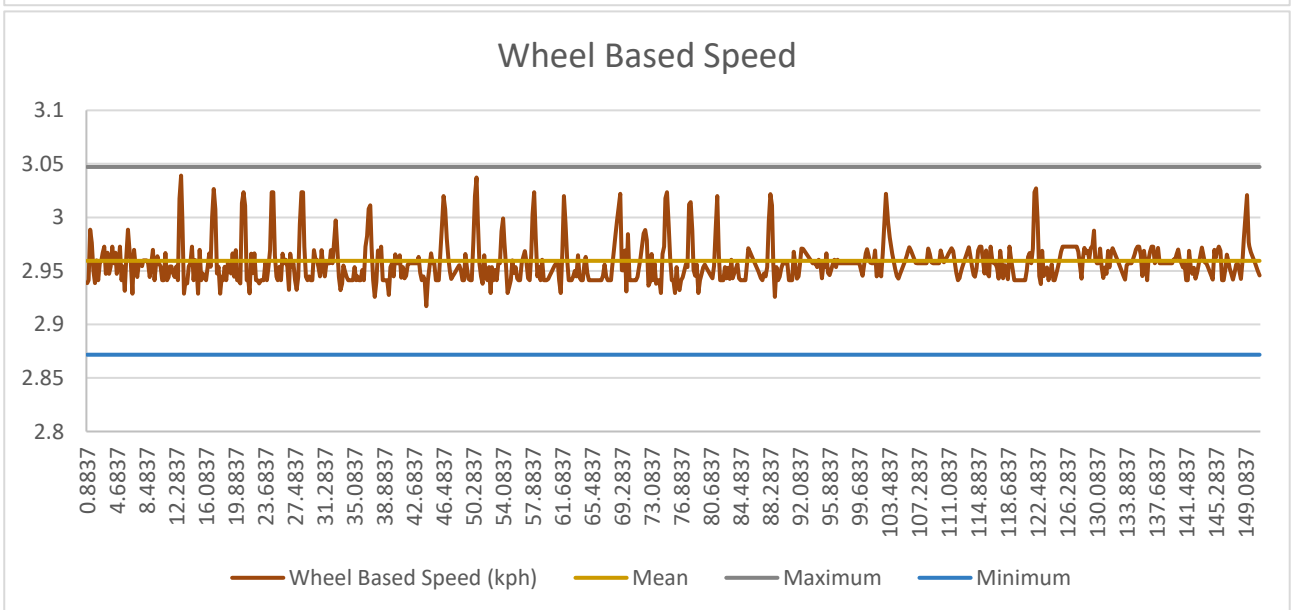
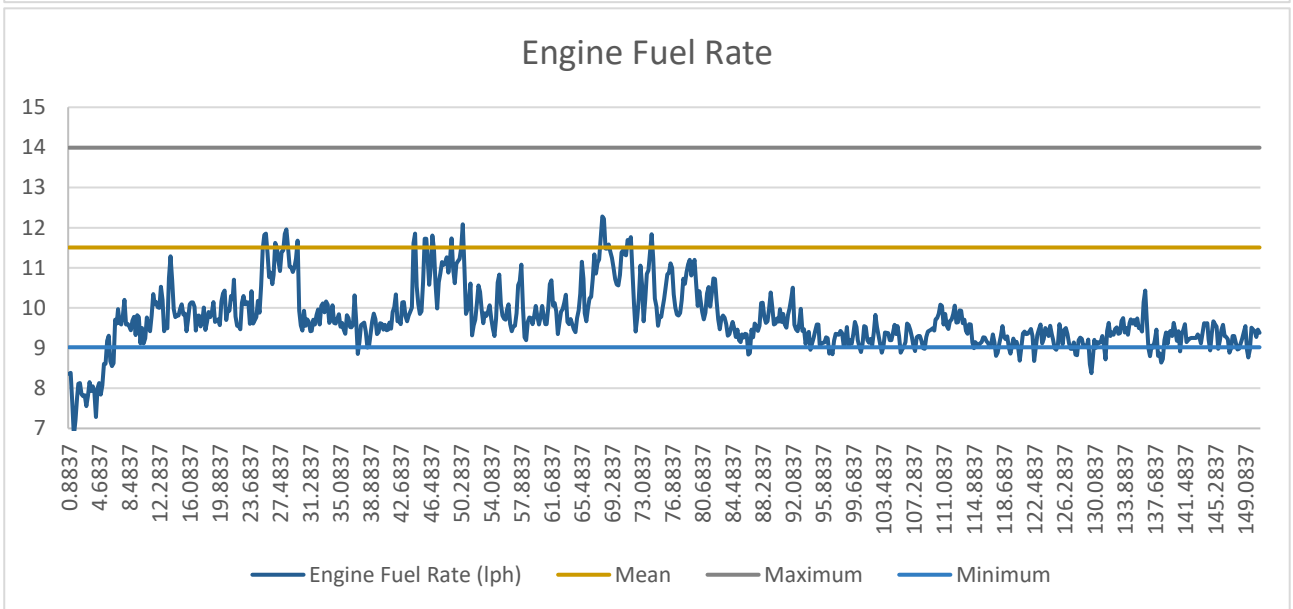
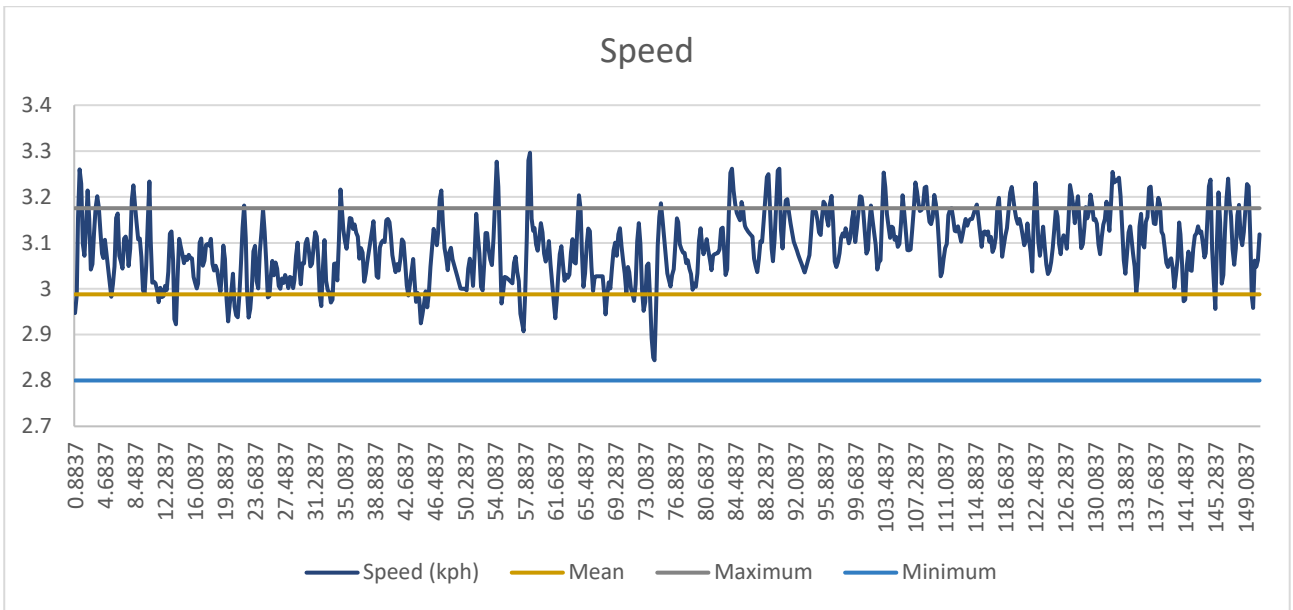


Engine RPM

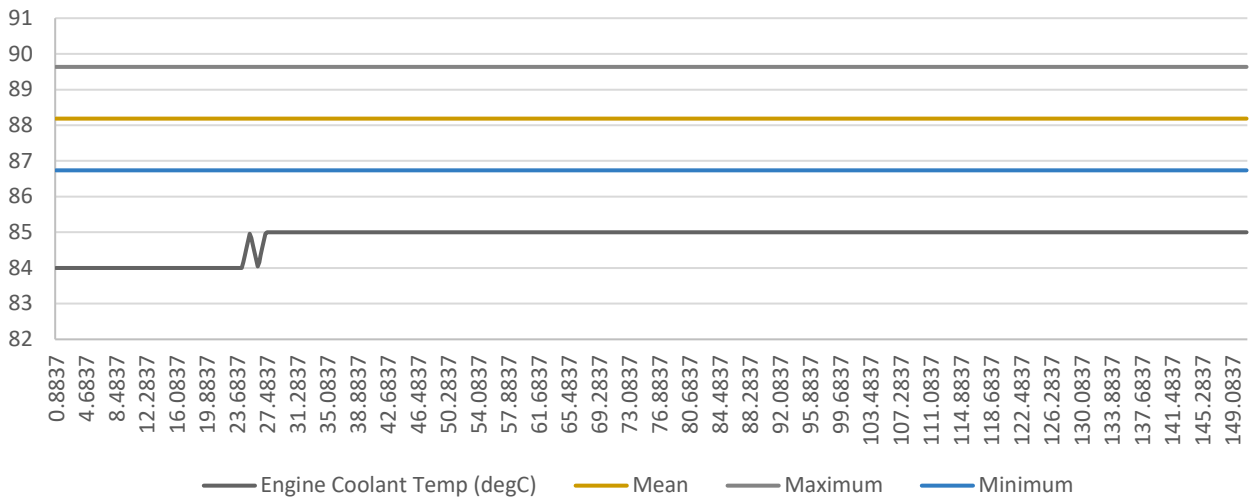


300mm – 3kph

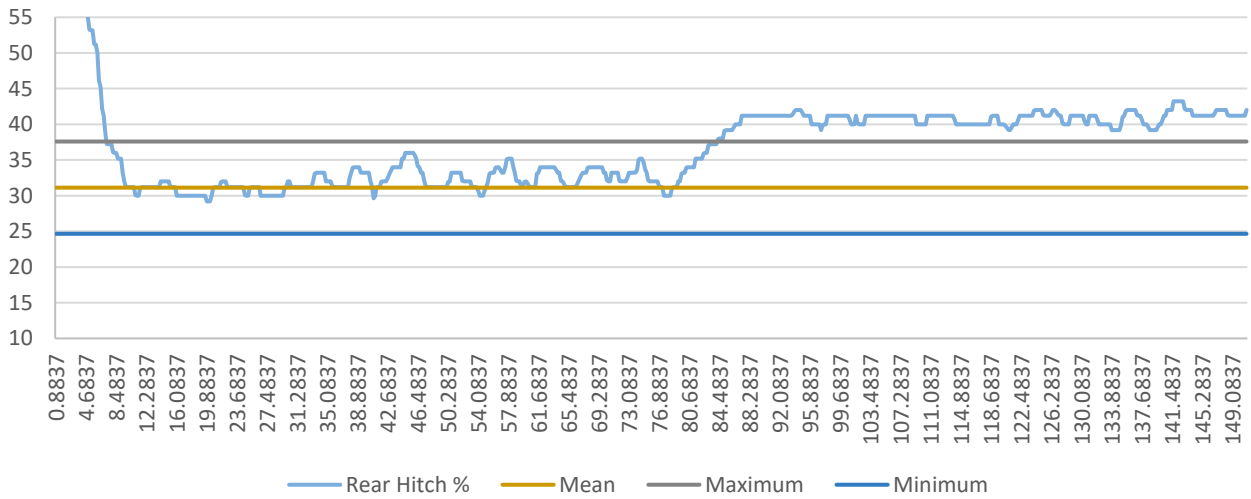




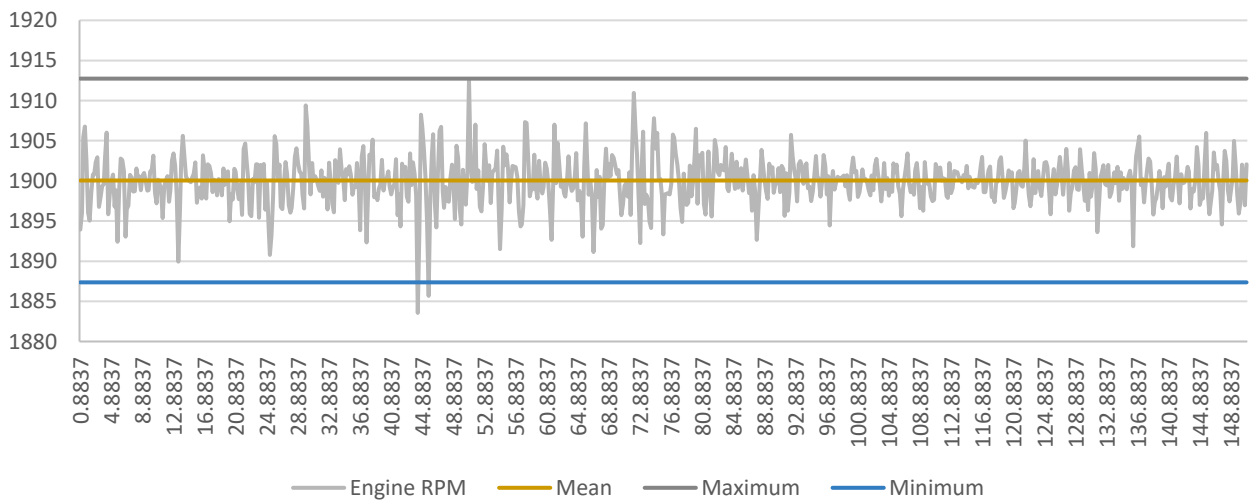
Coolant Temperature



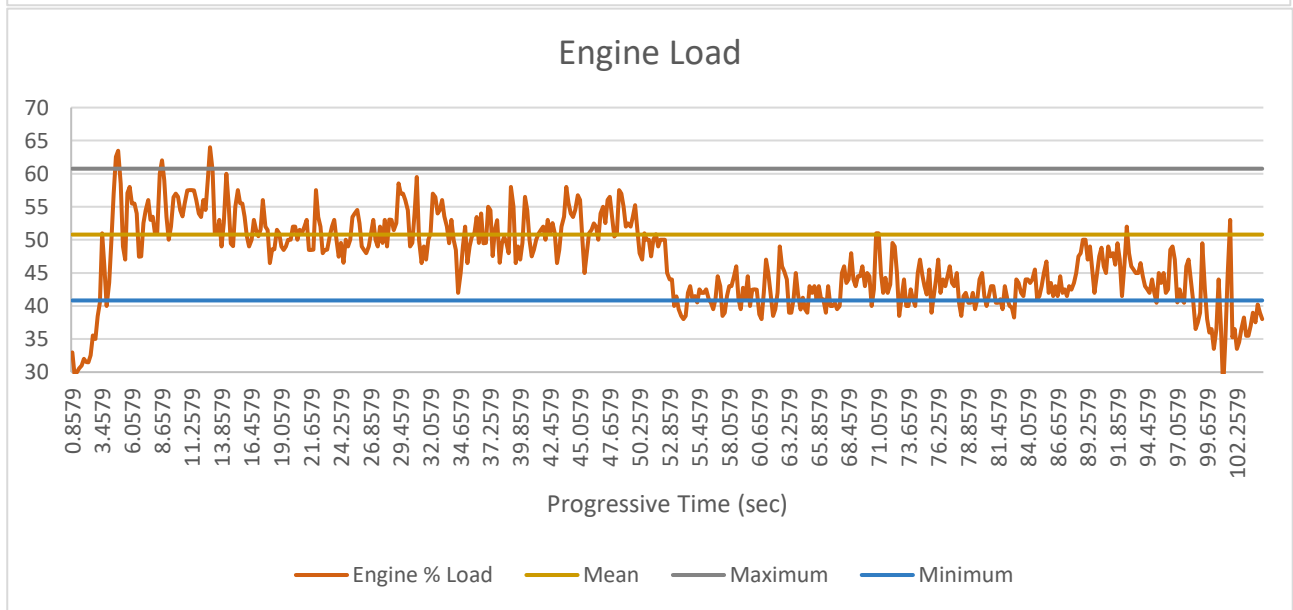
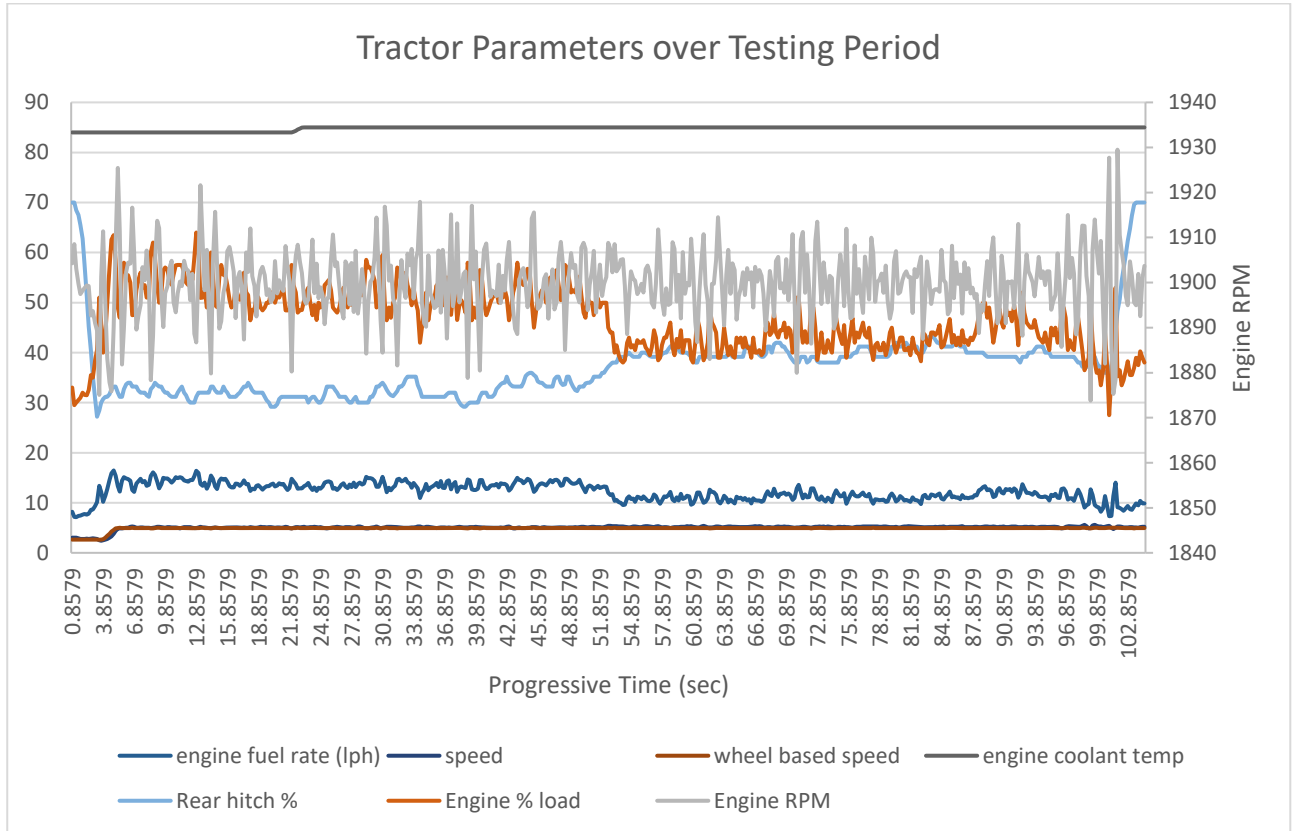
Rear Hitch %

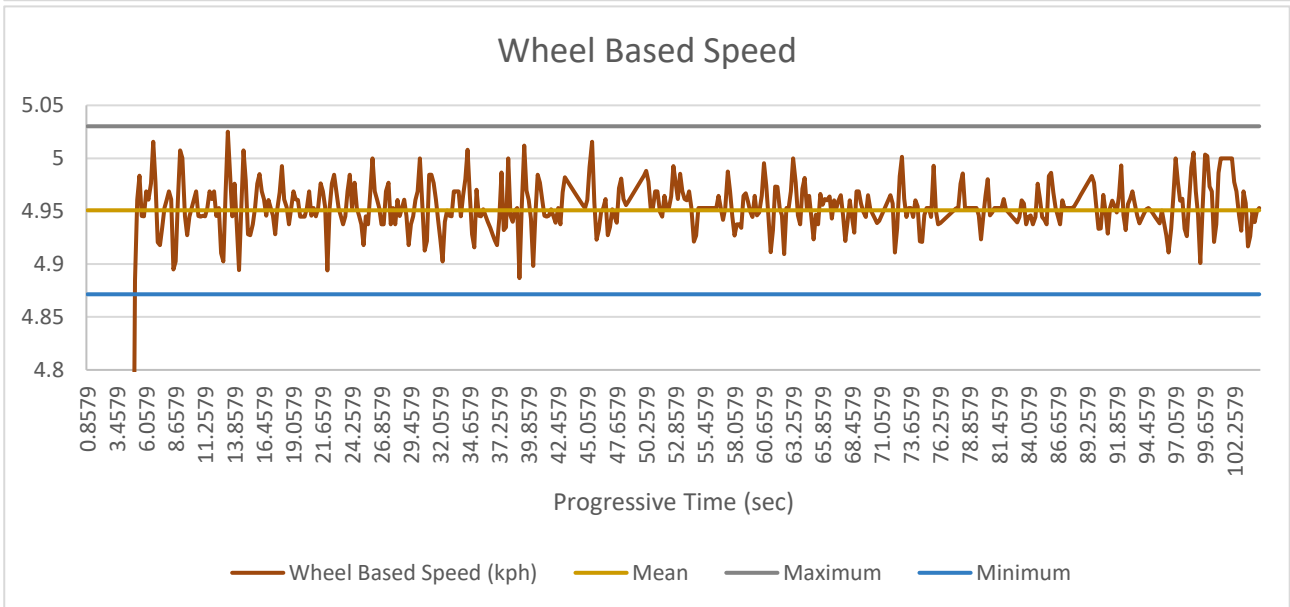
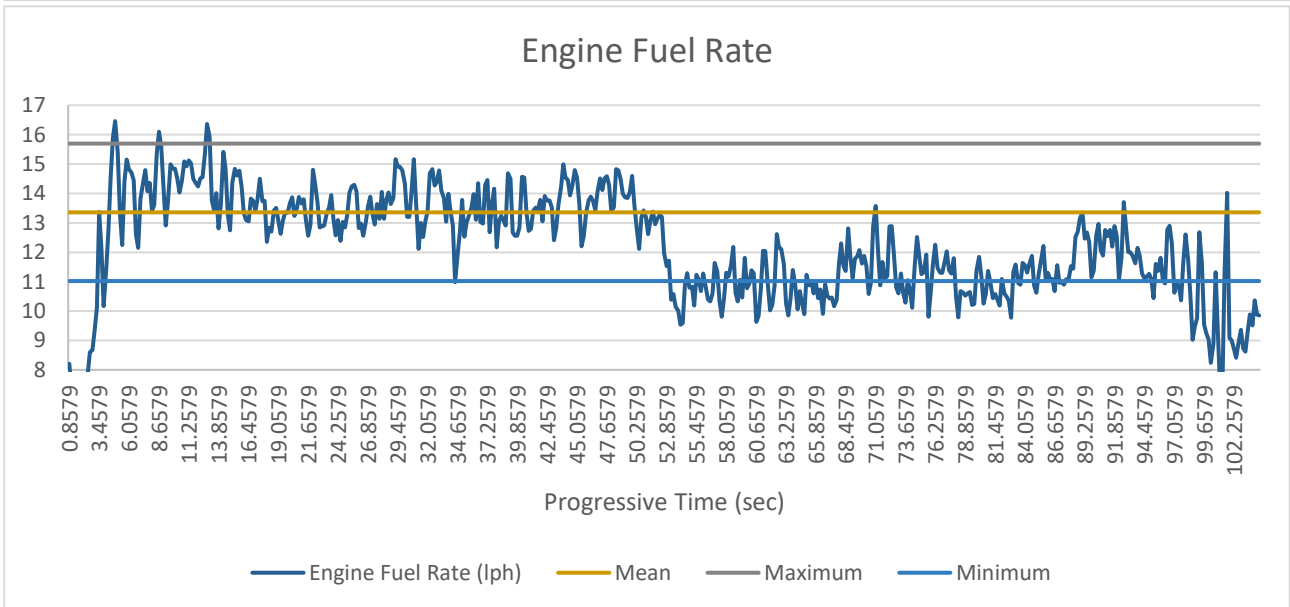
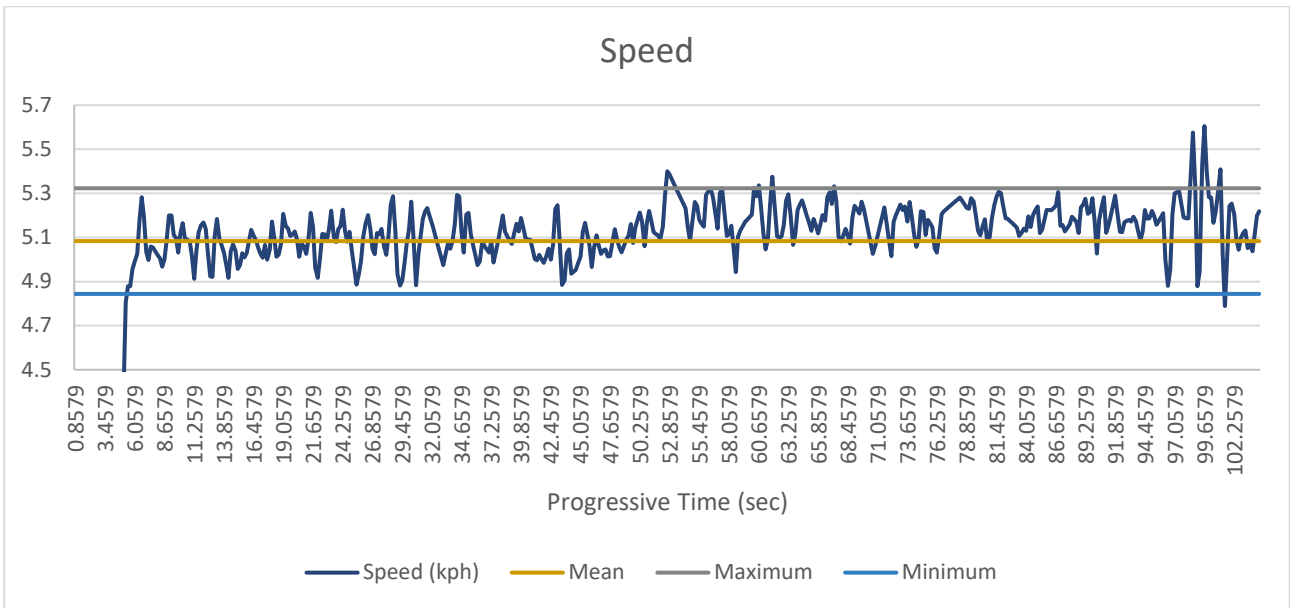


Engine RPM

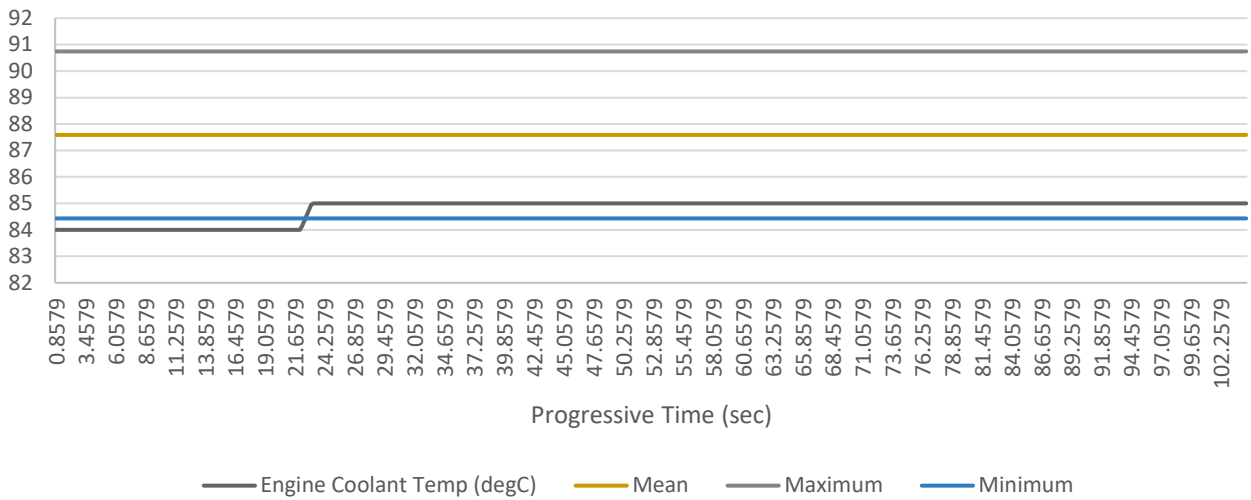


300mm – 5kph

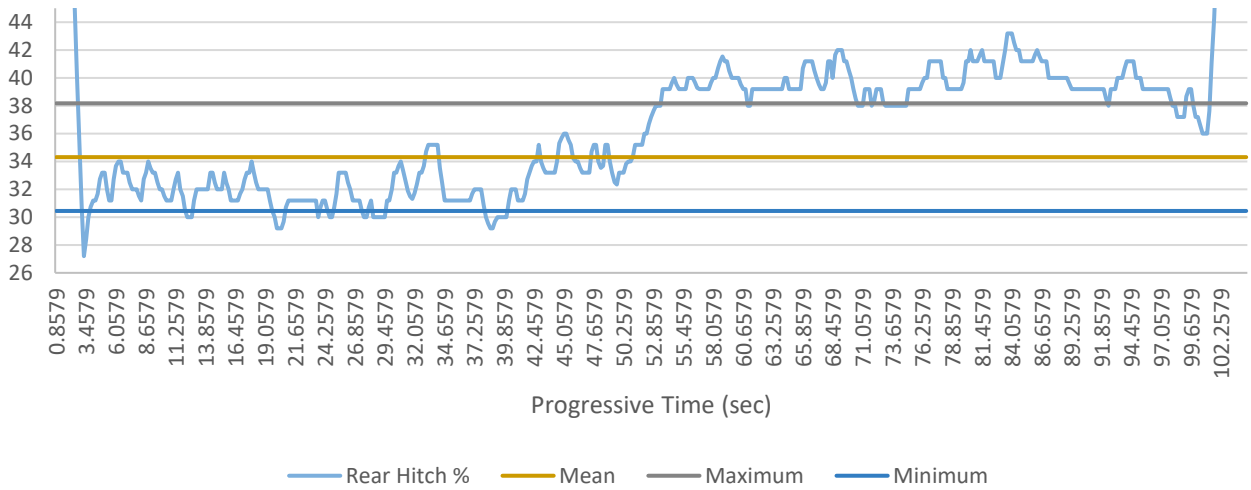




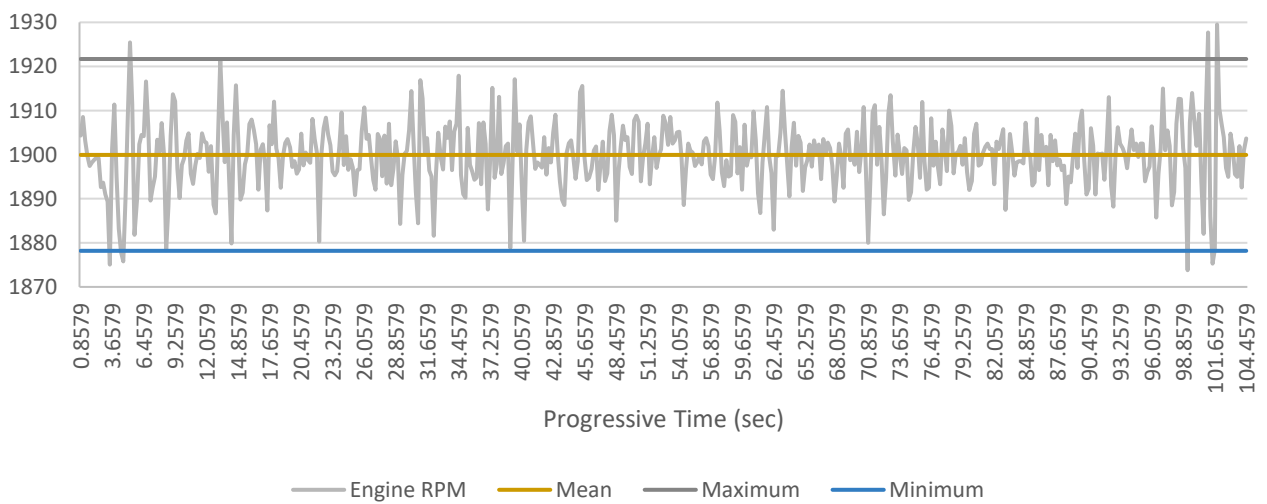
Coolant Temperature



Rear Hitch %

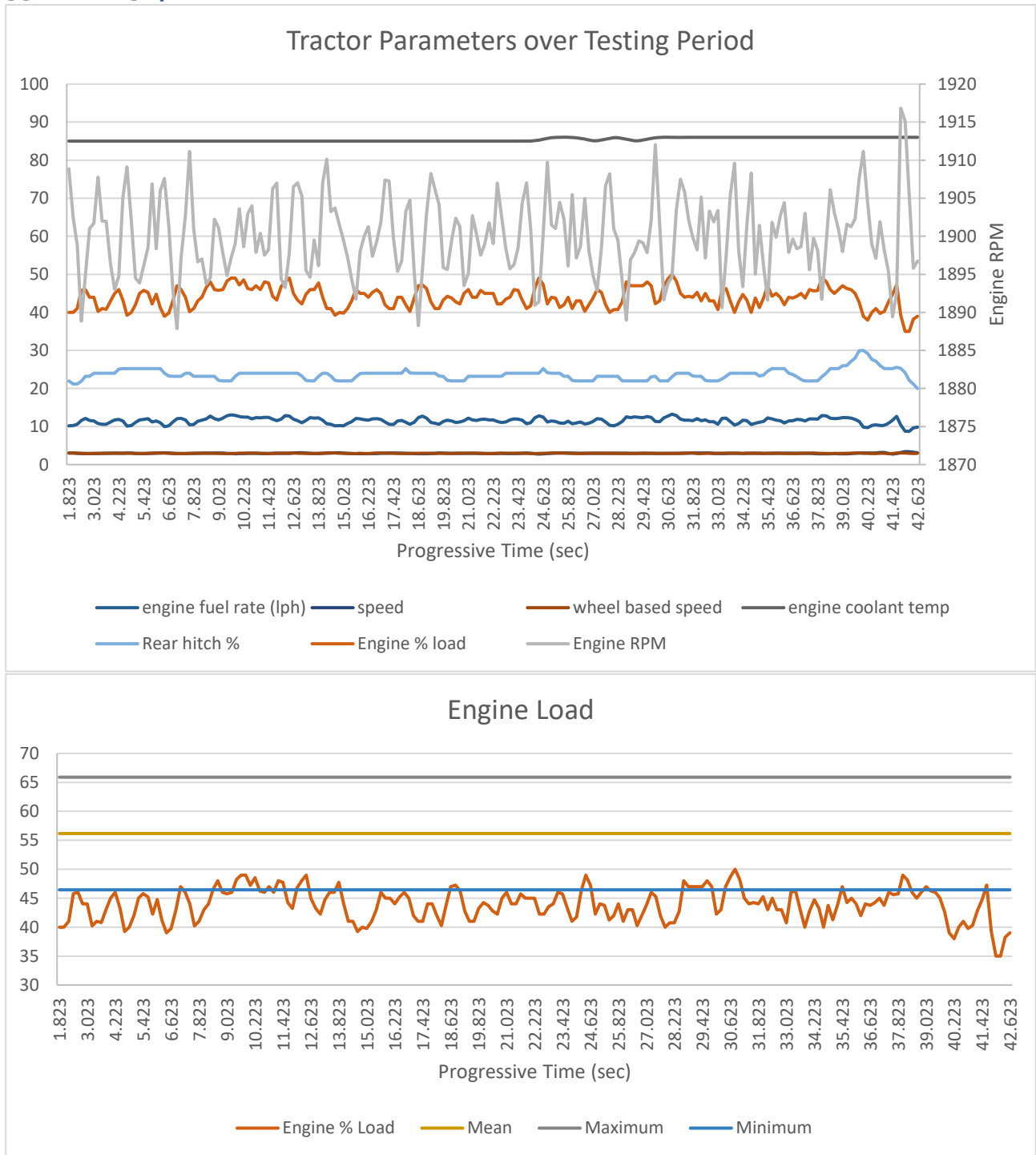


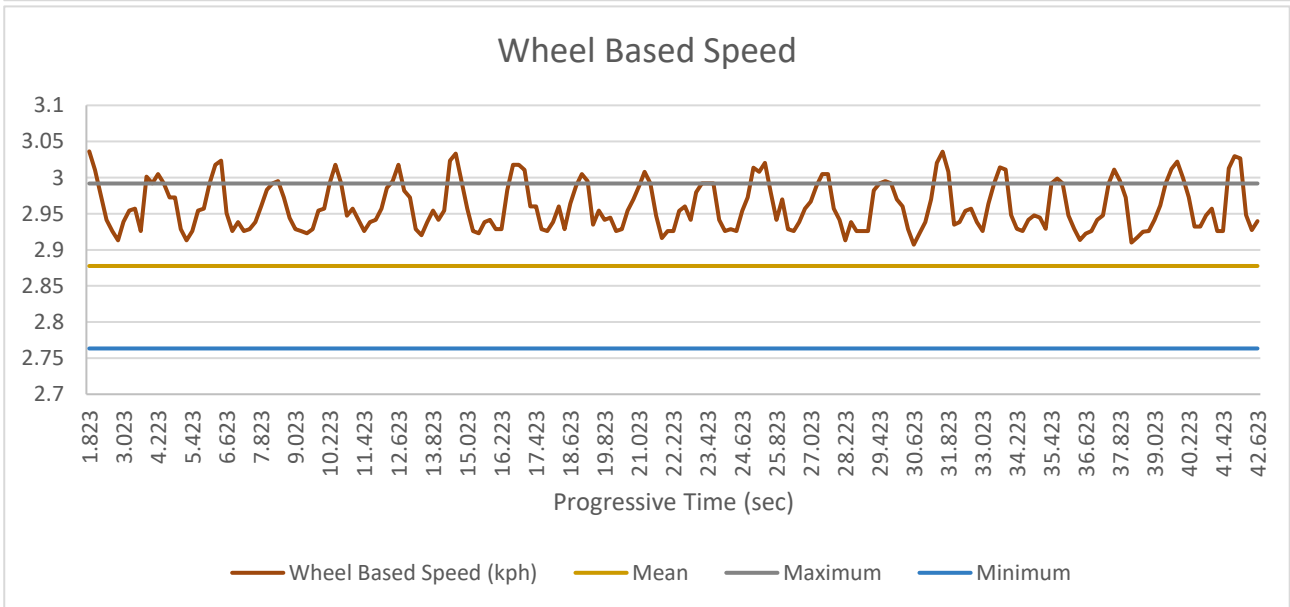
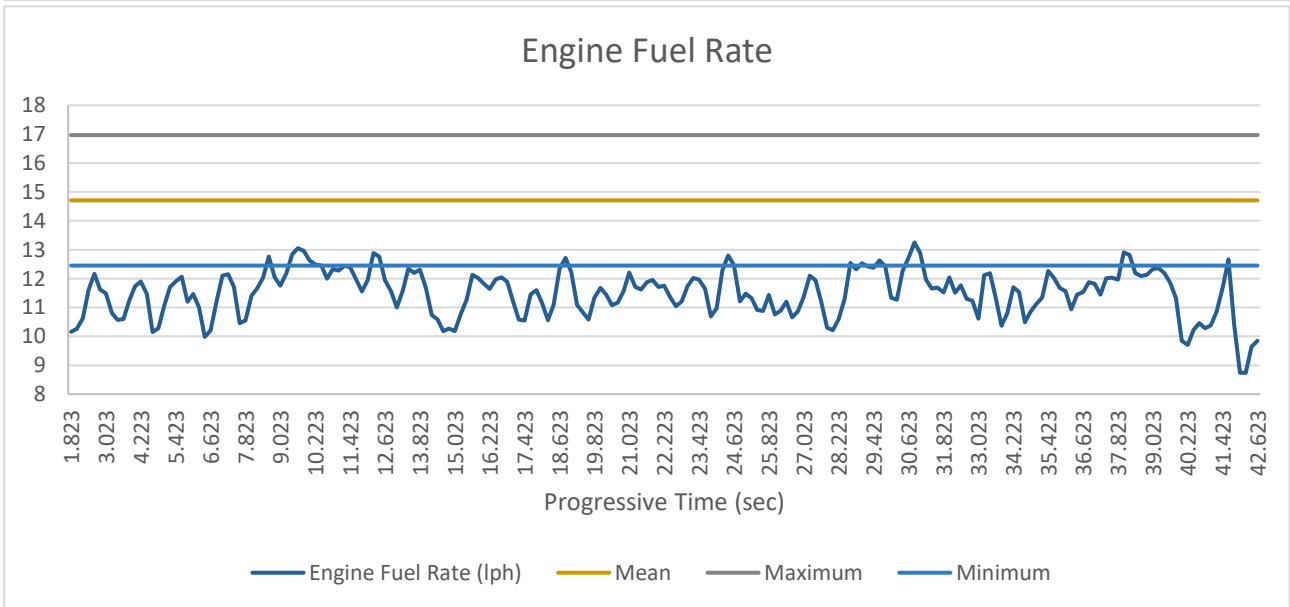
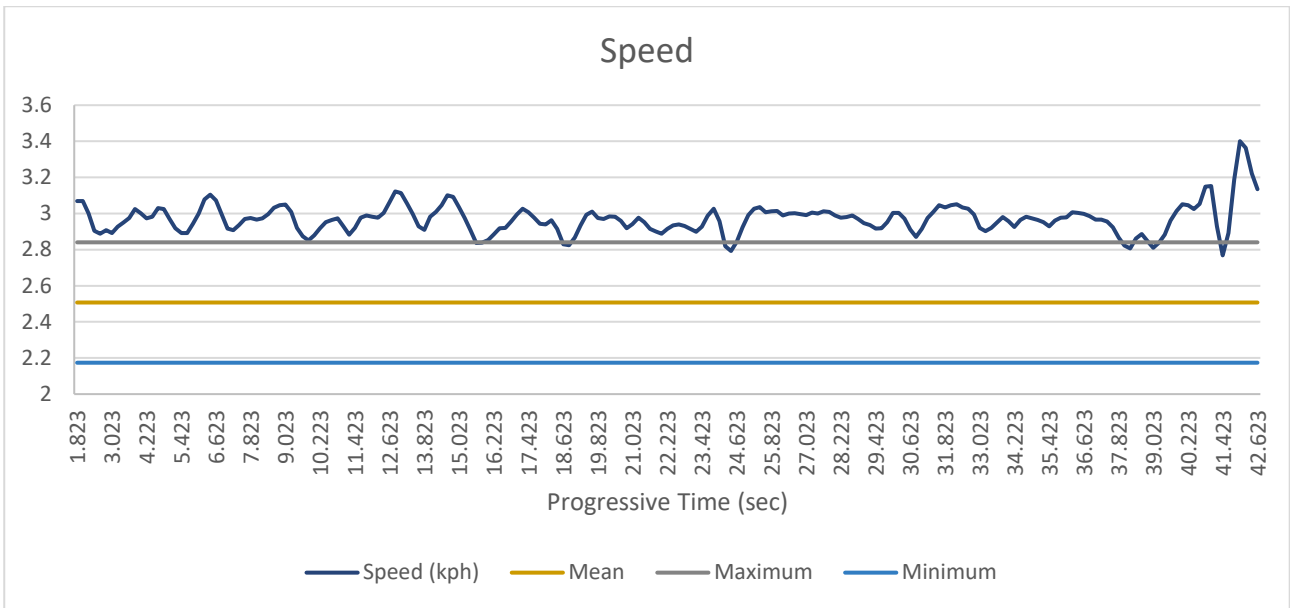
Engine RPM

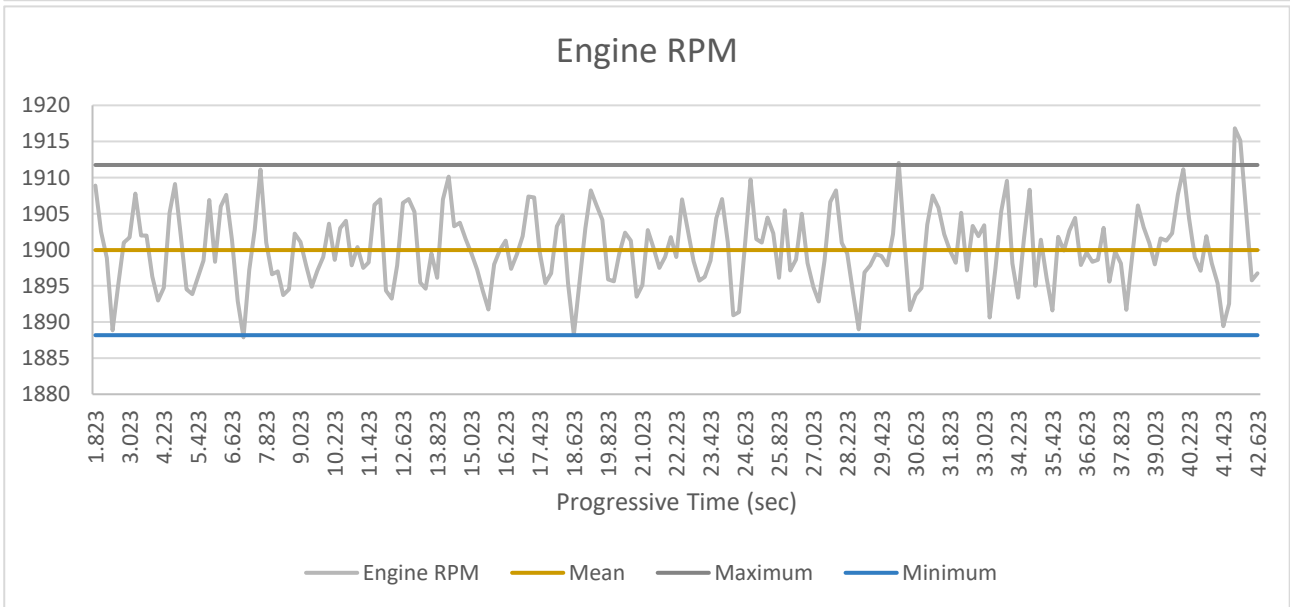
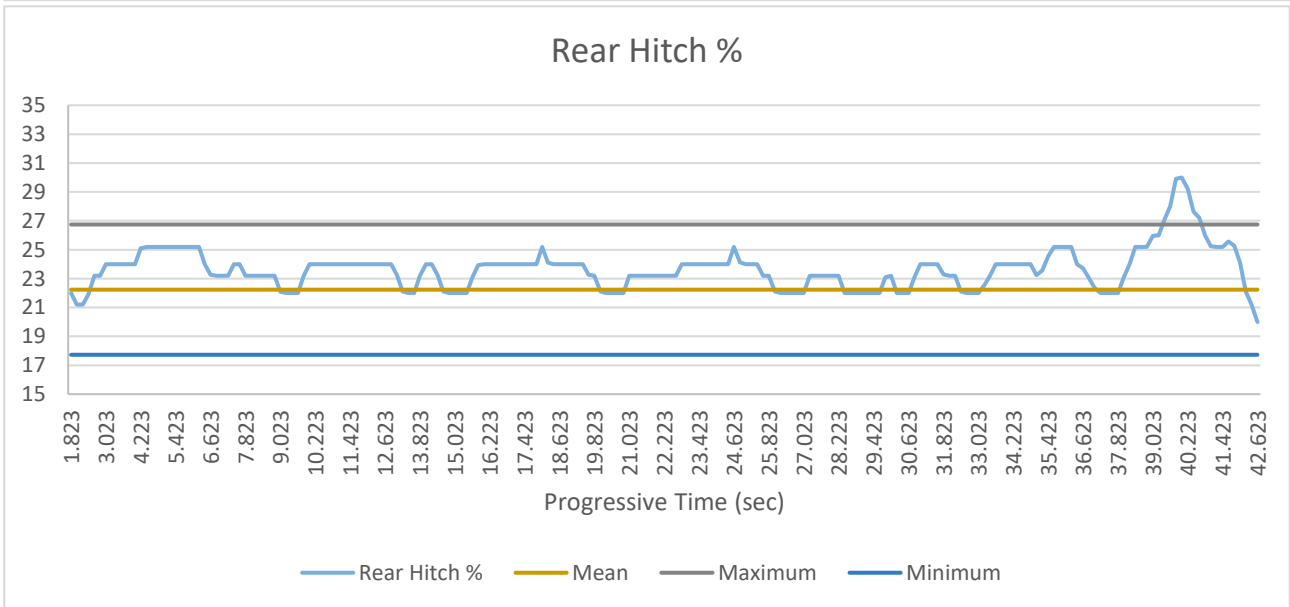
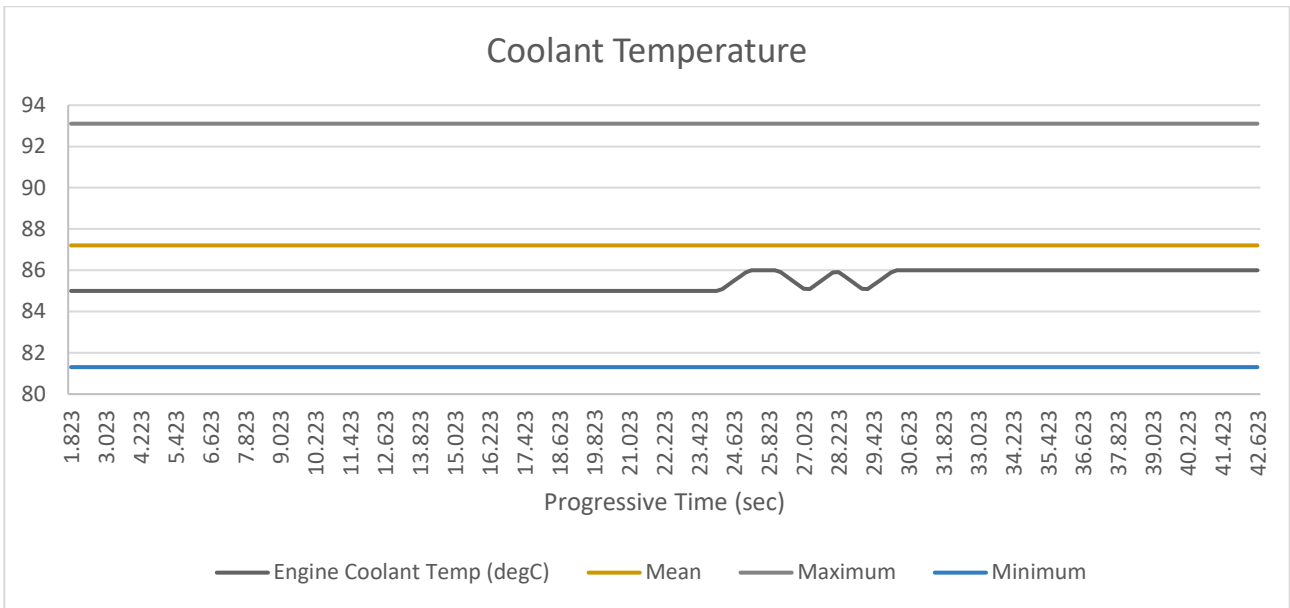


Appendix K – 3PL Deep Ripper – Failing to lift 3PL prior to headland execution data

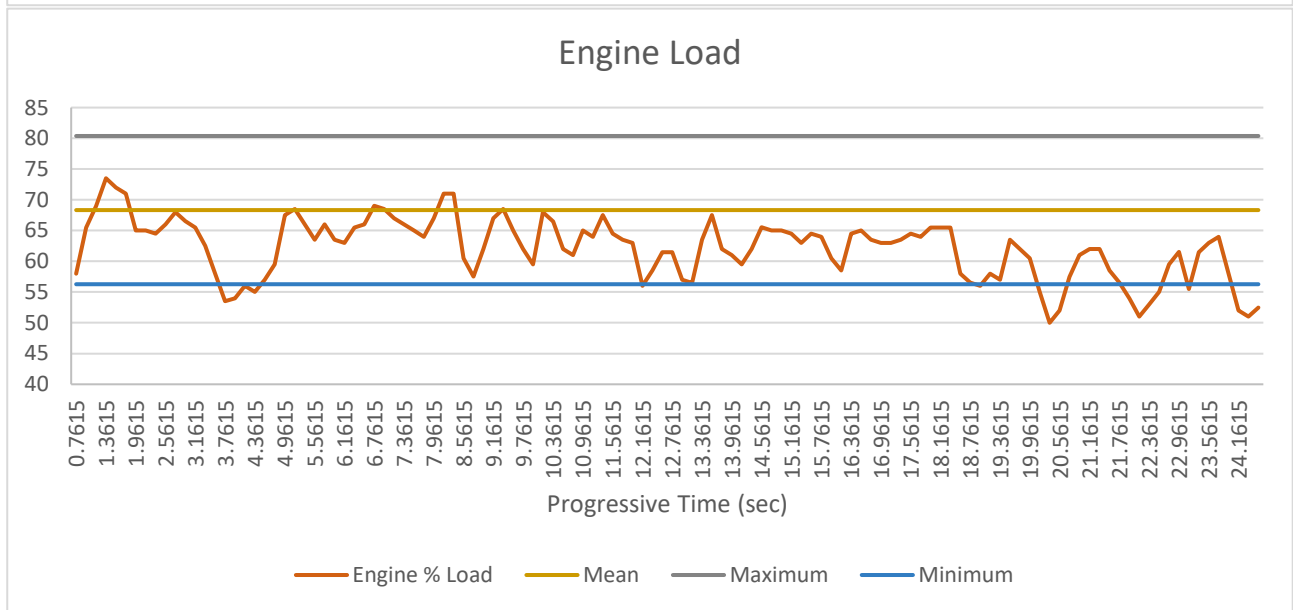
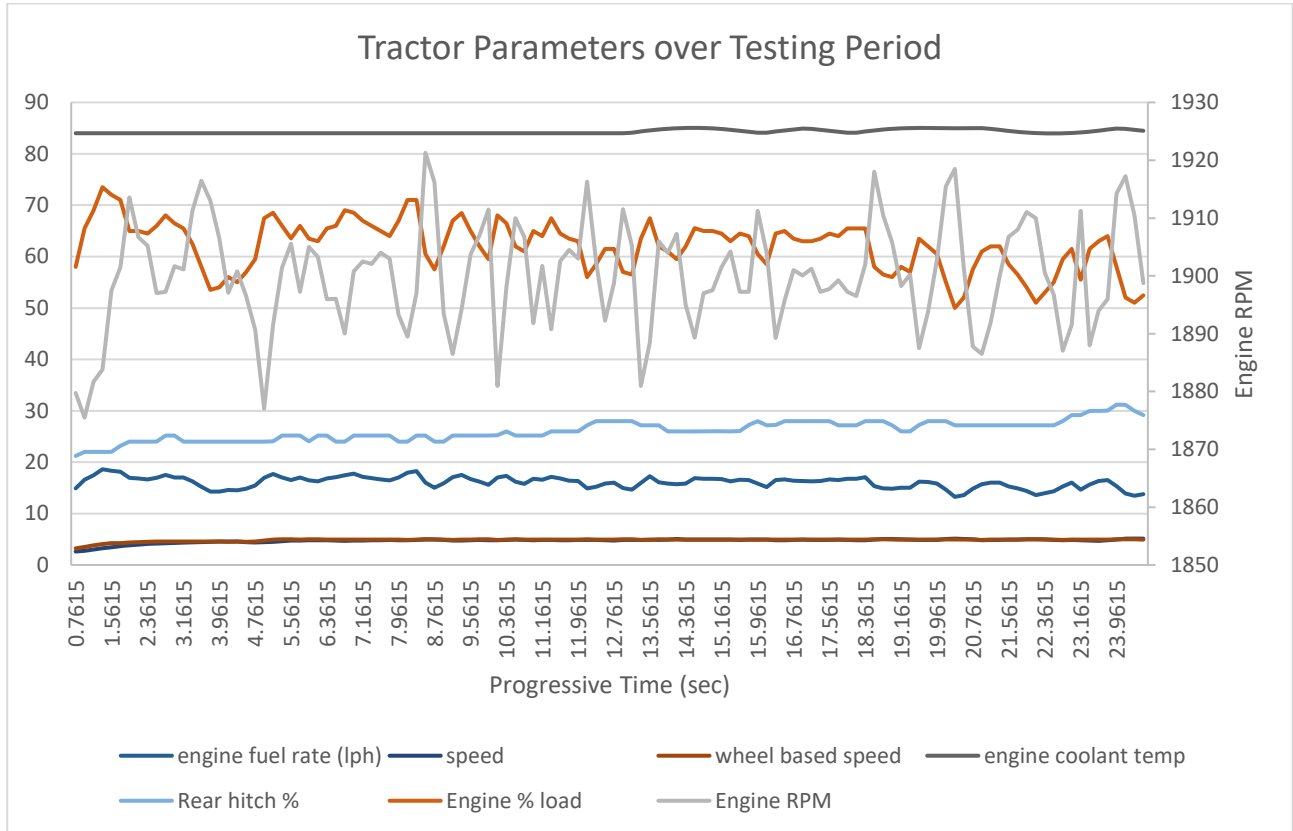
350mm – 3kph

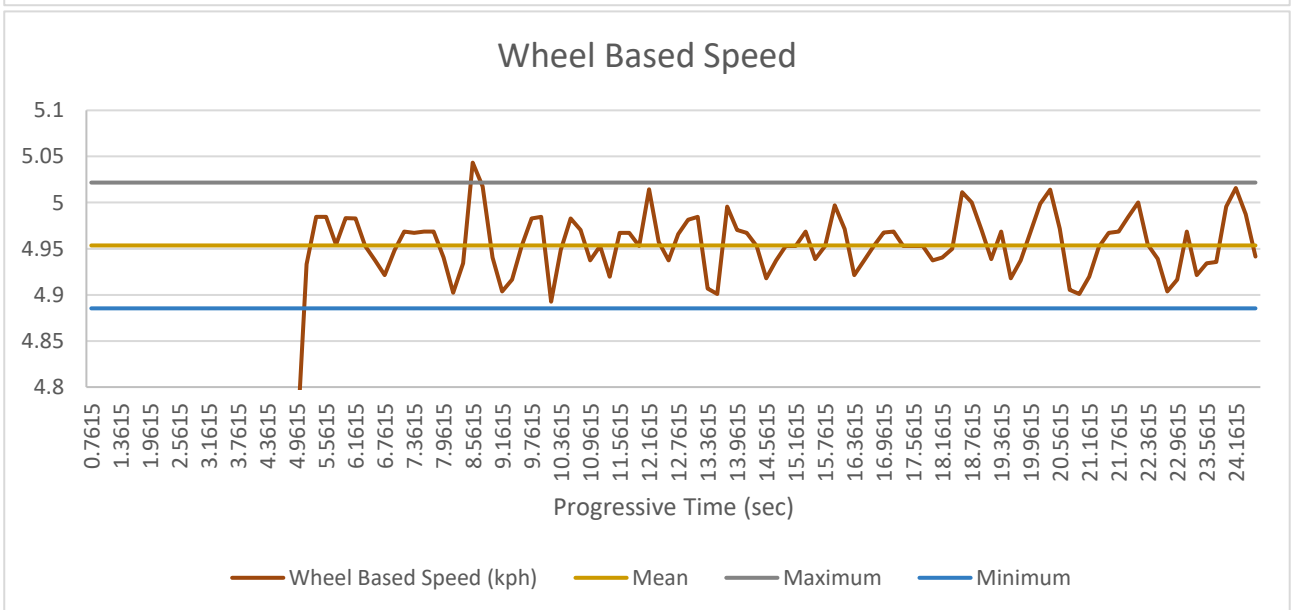
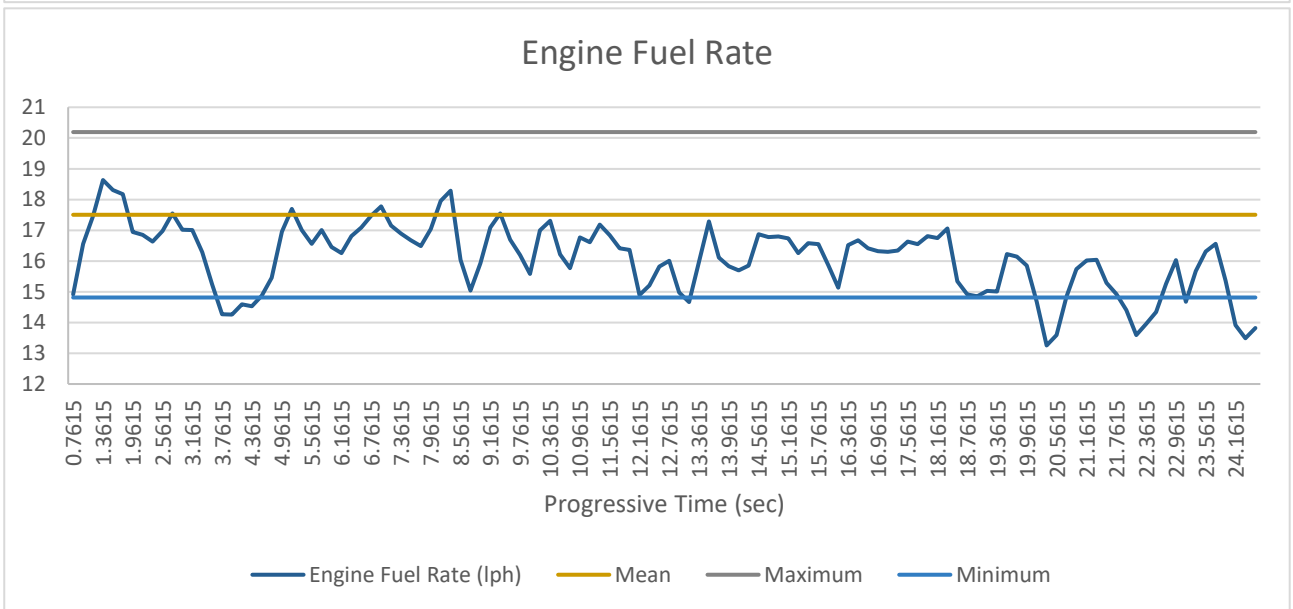
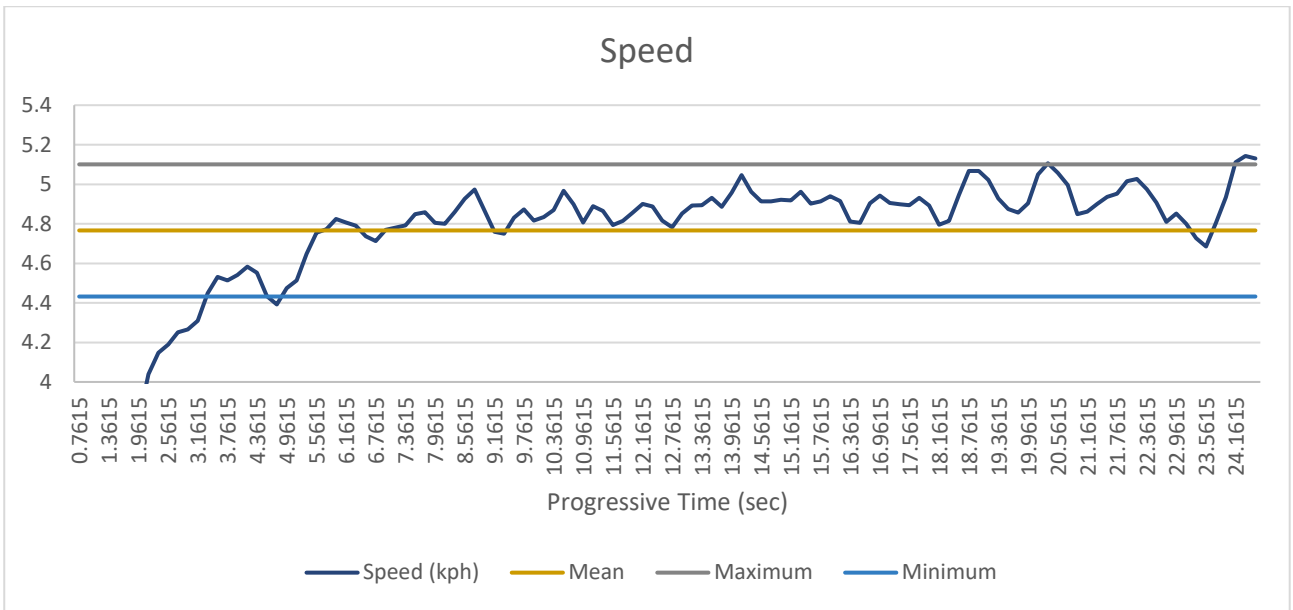


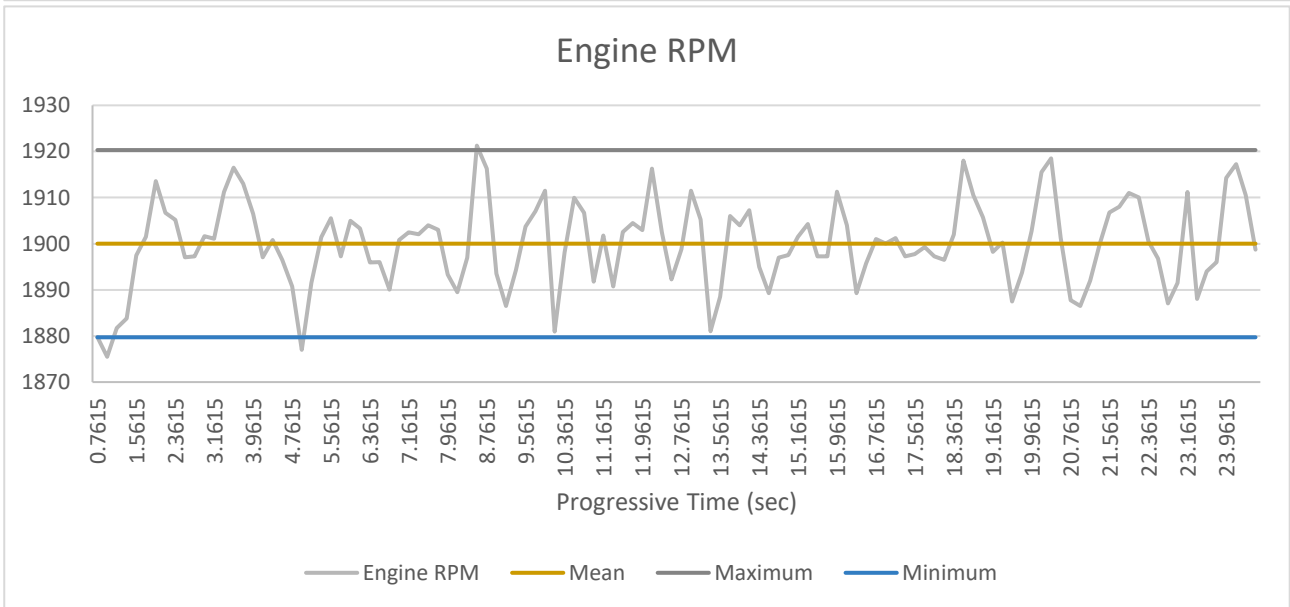
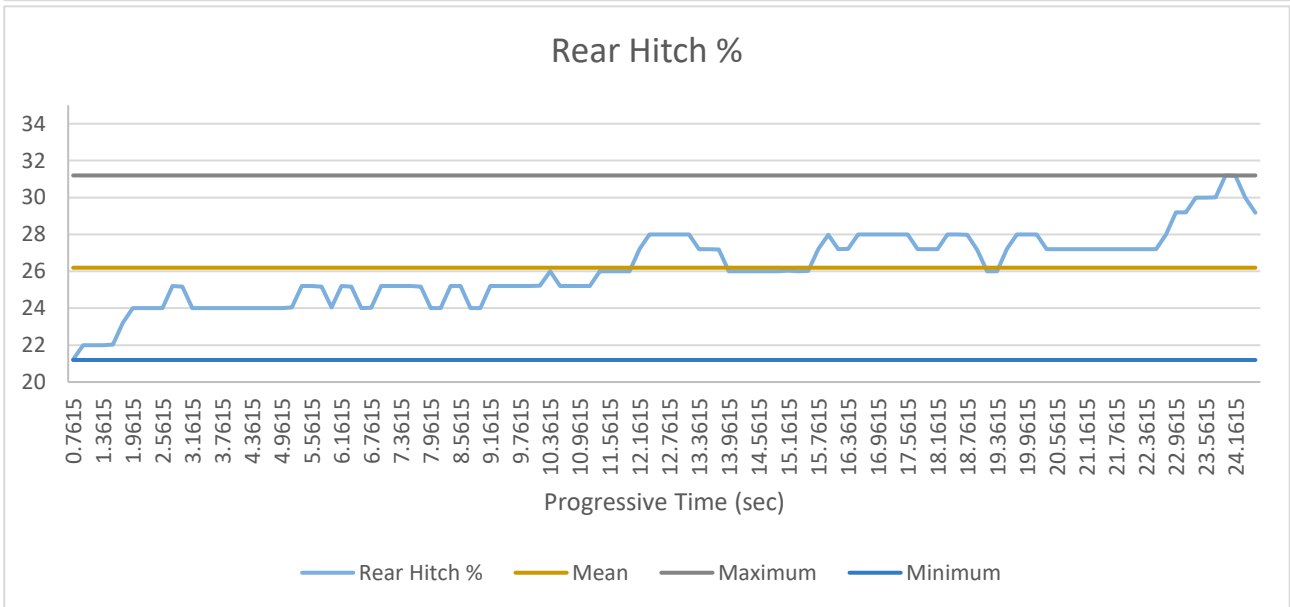
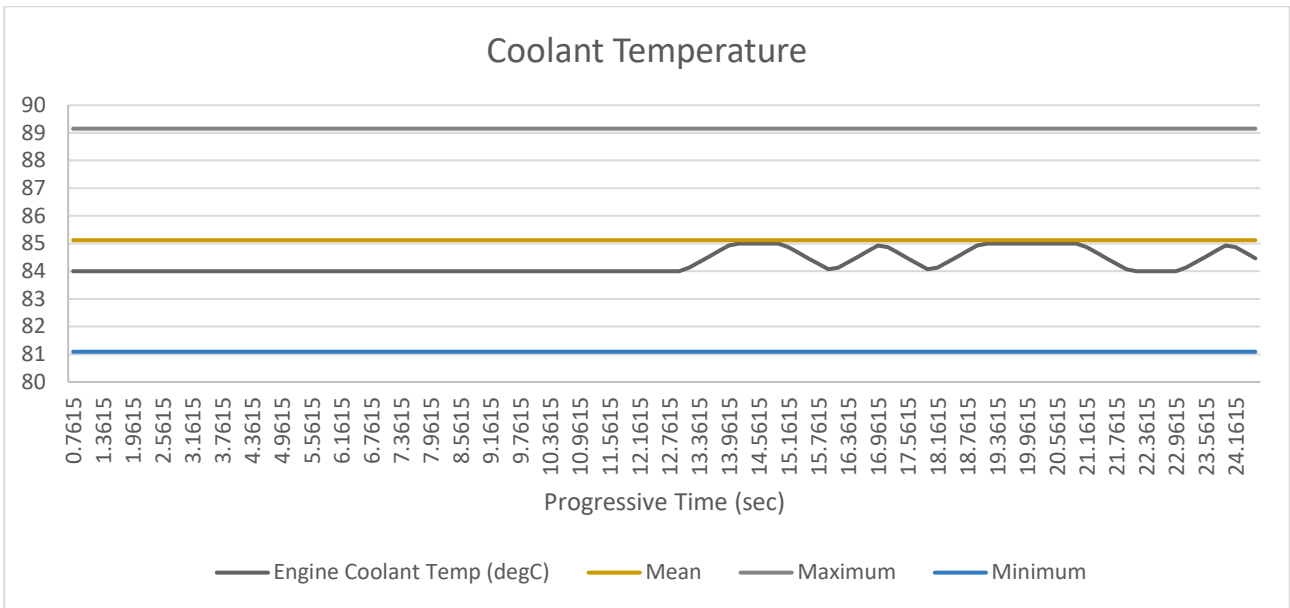




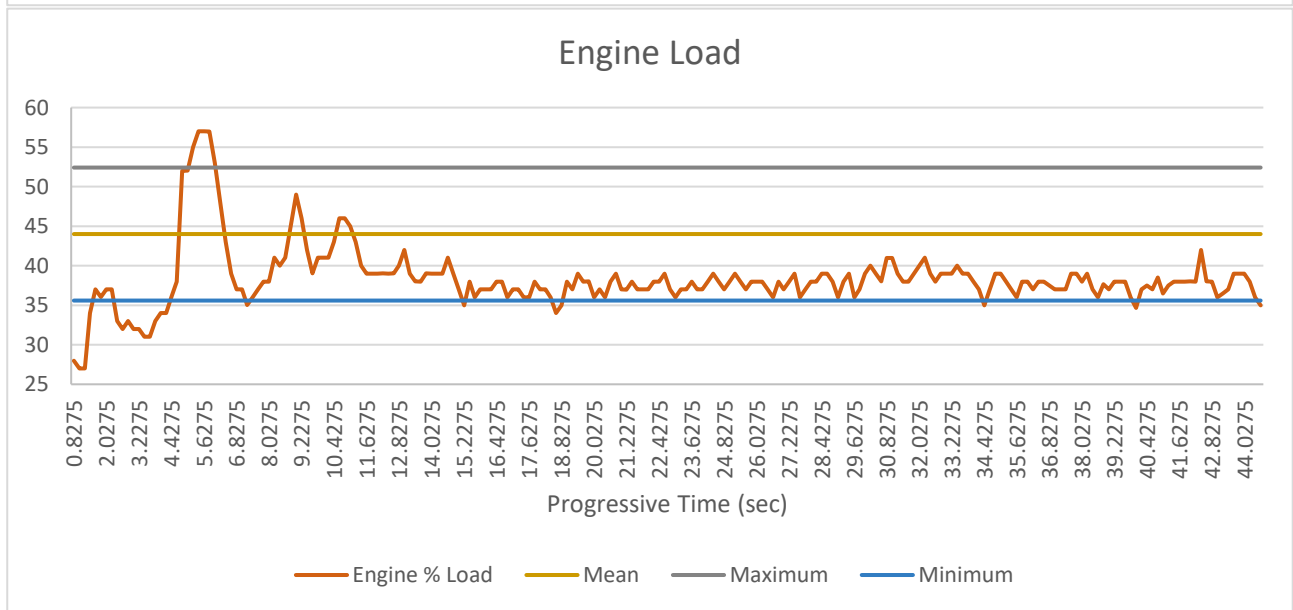
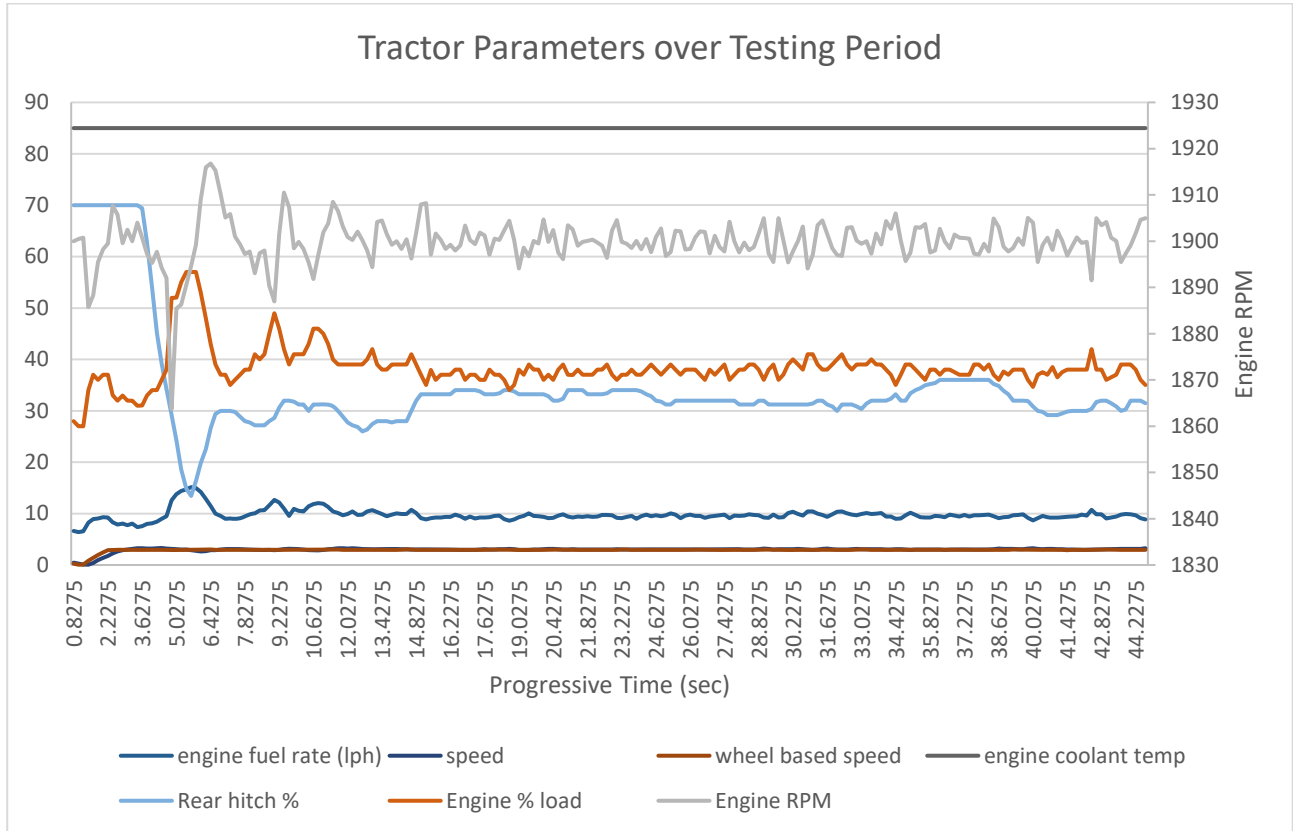
350mm – 5kph

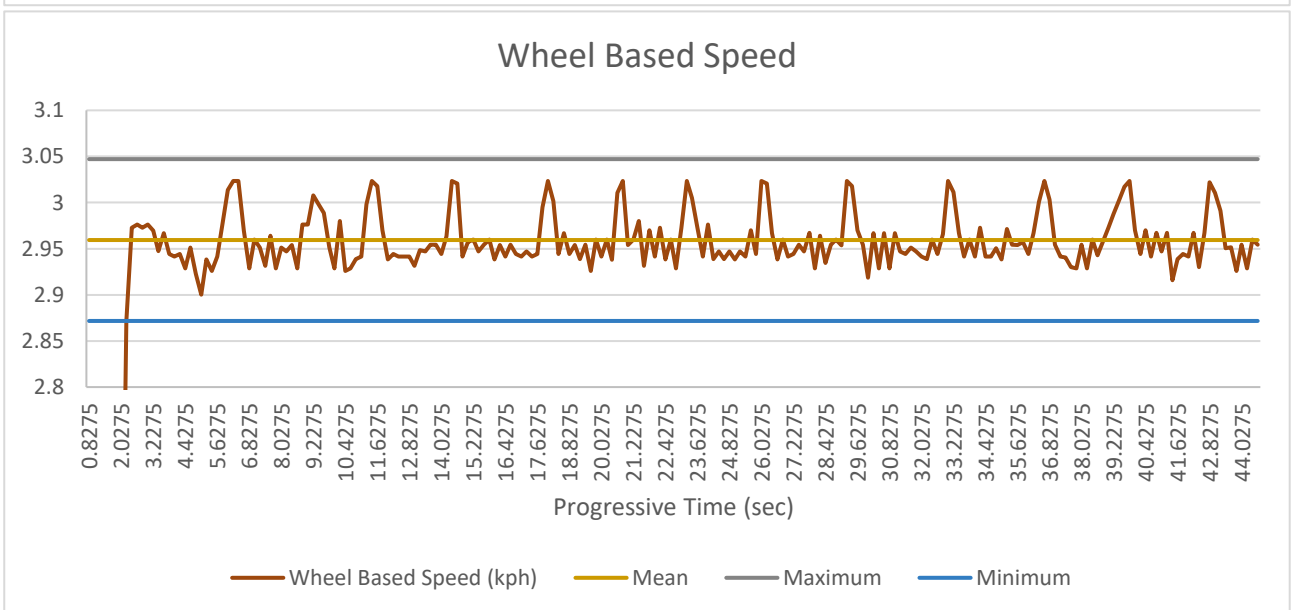
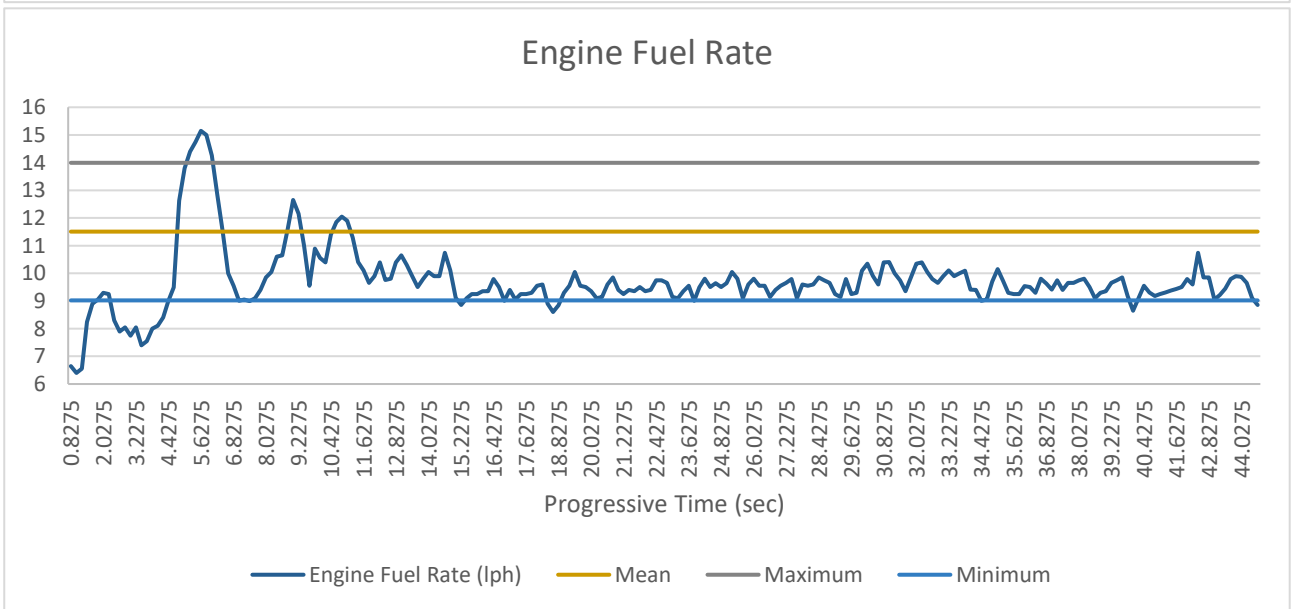
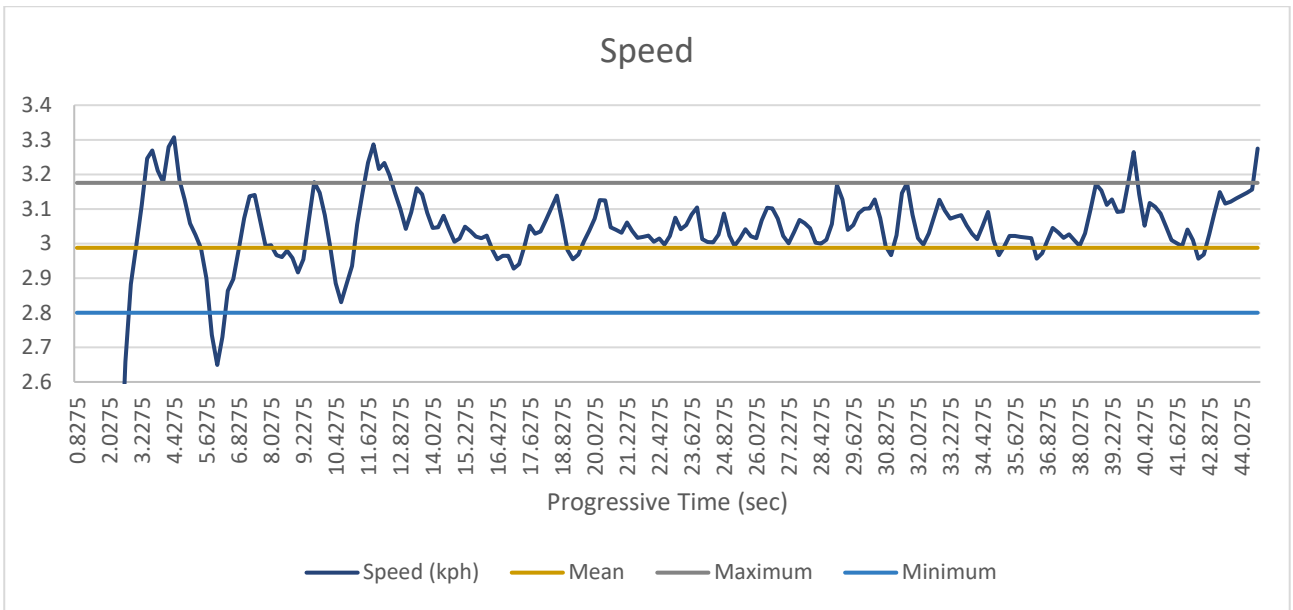


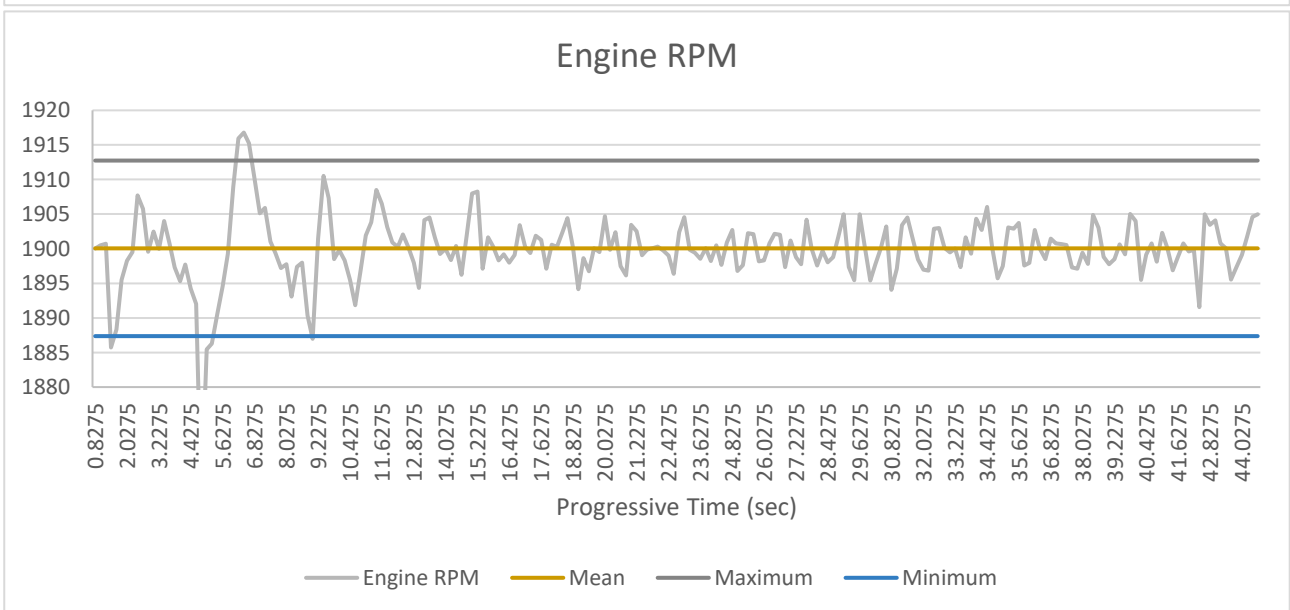
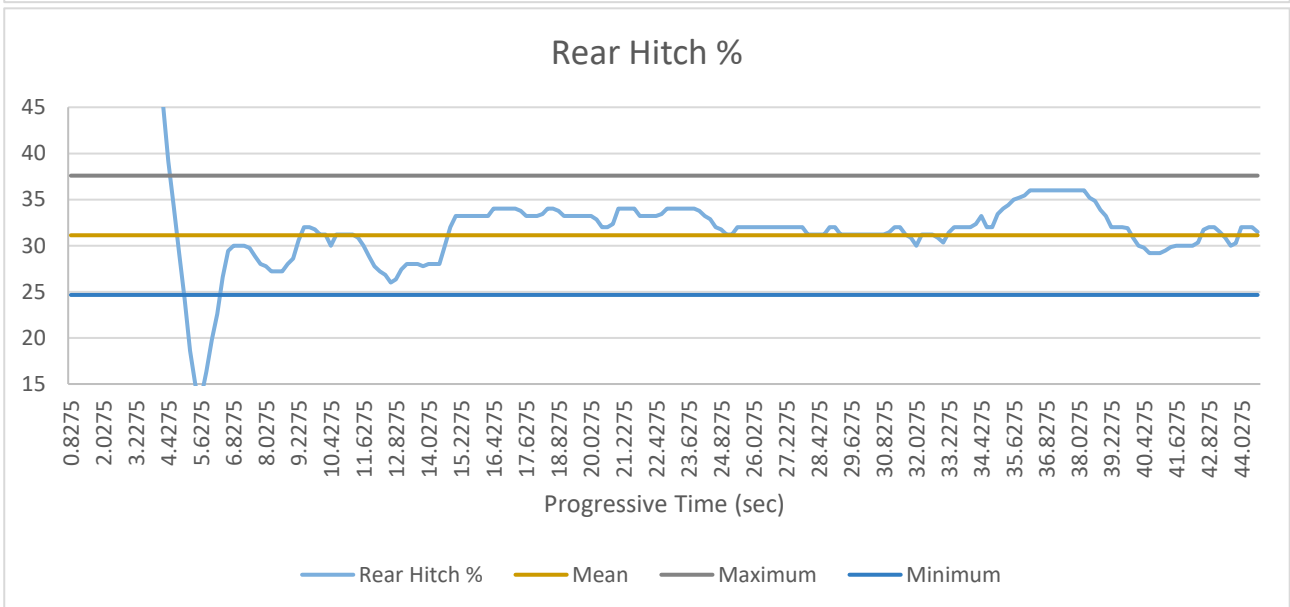
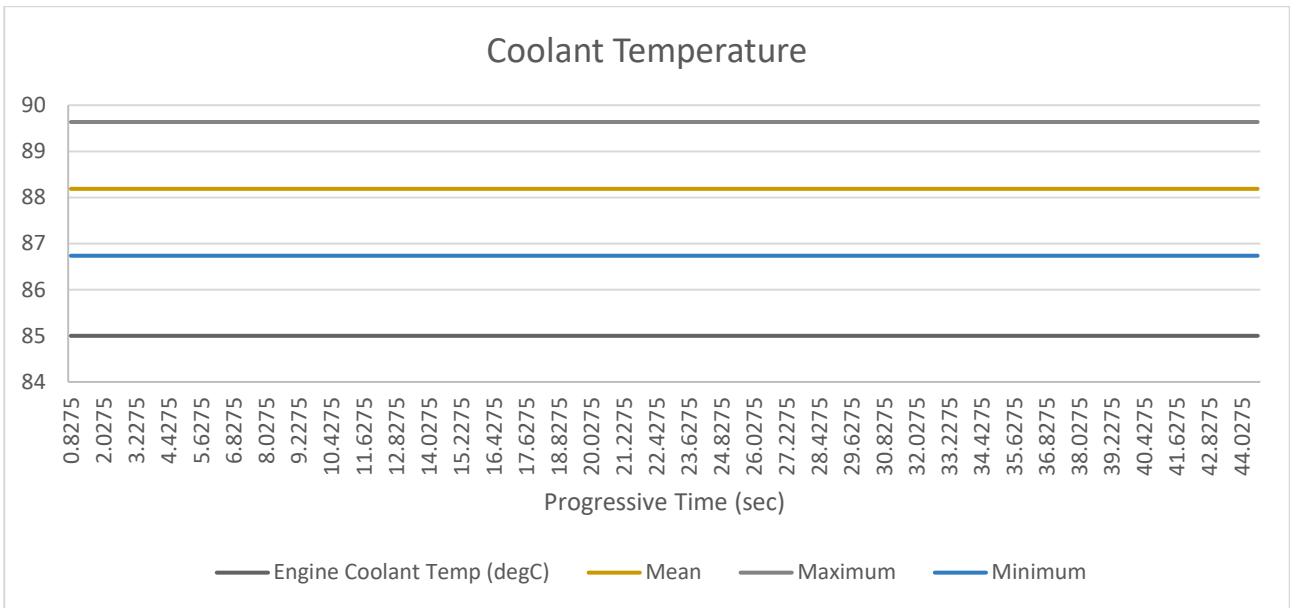




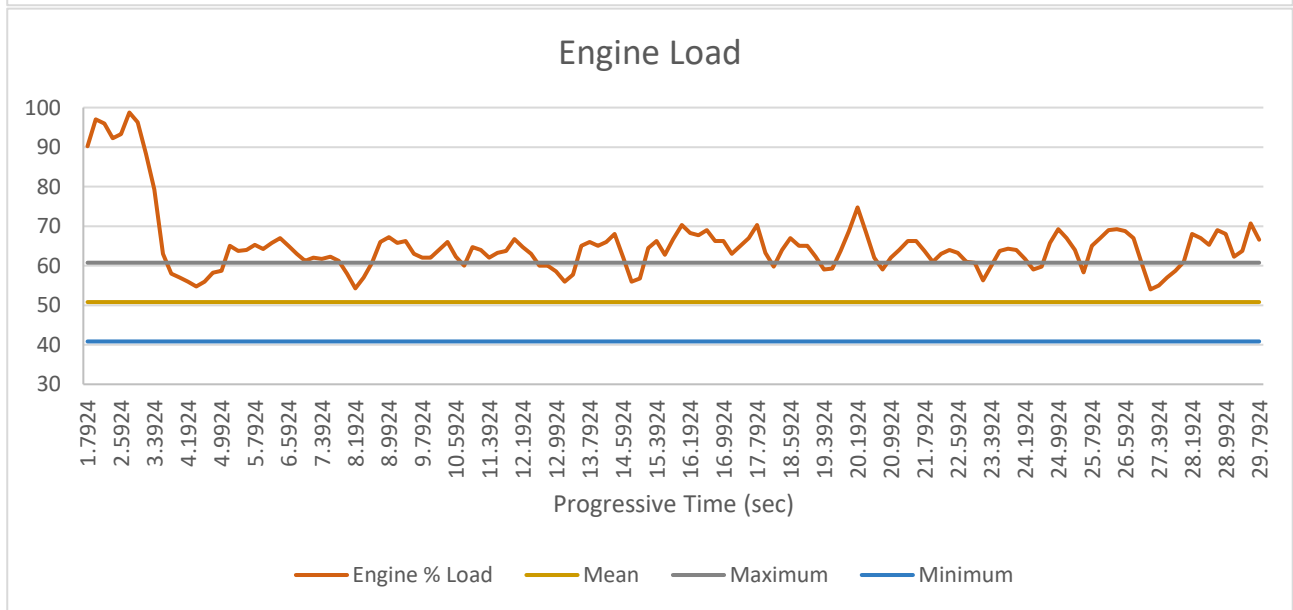
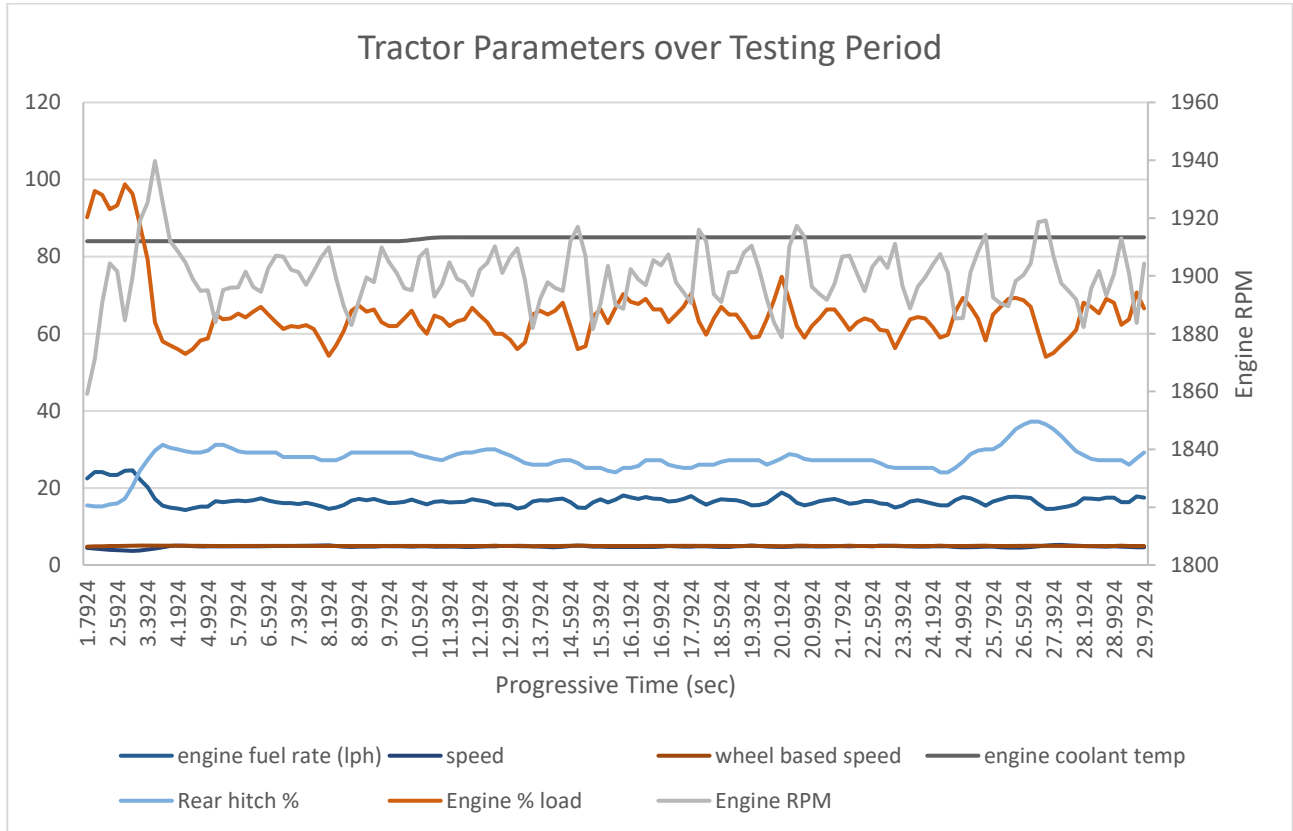
300mm – 3kph

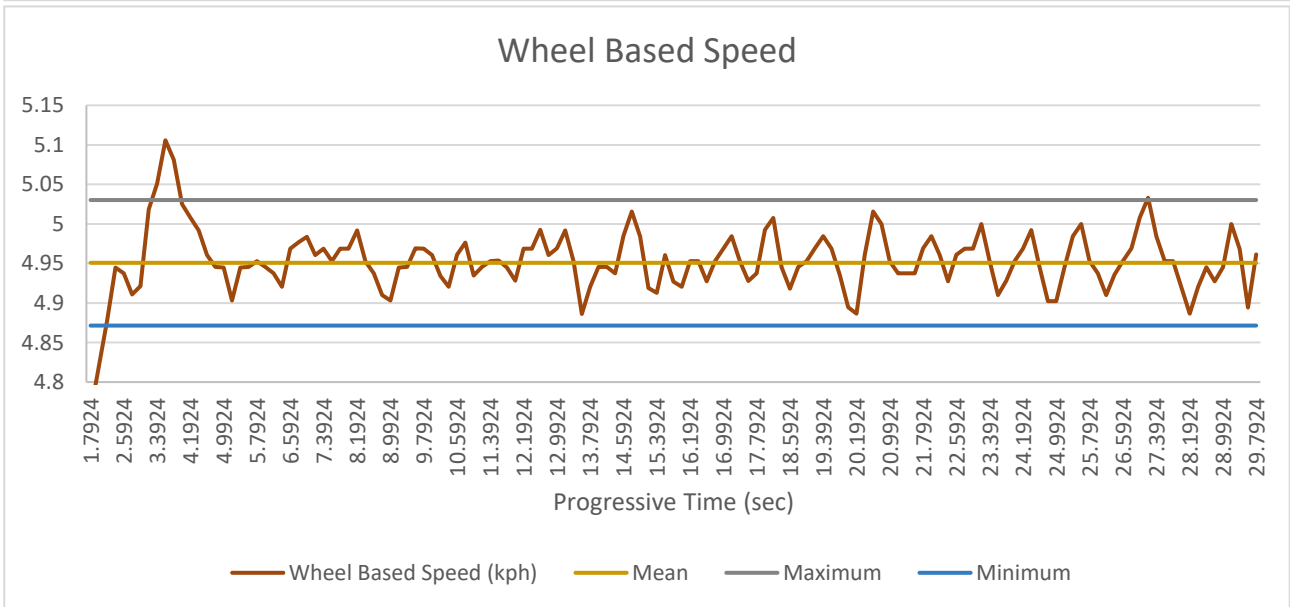
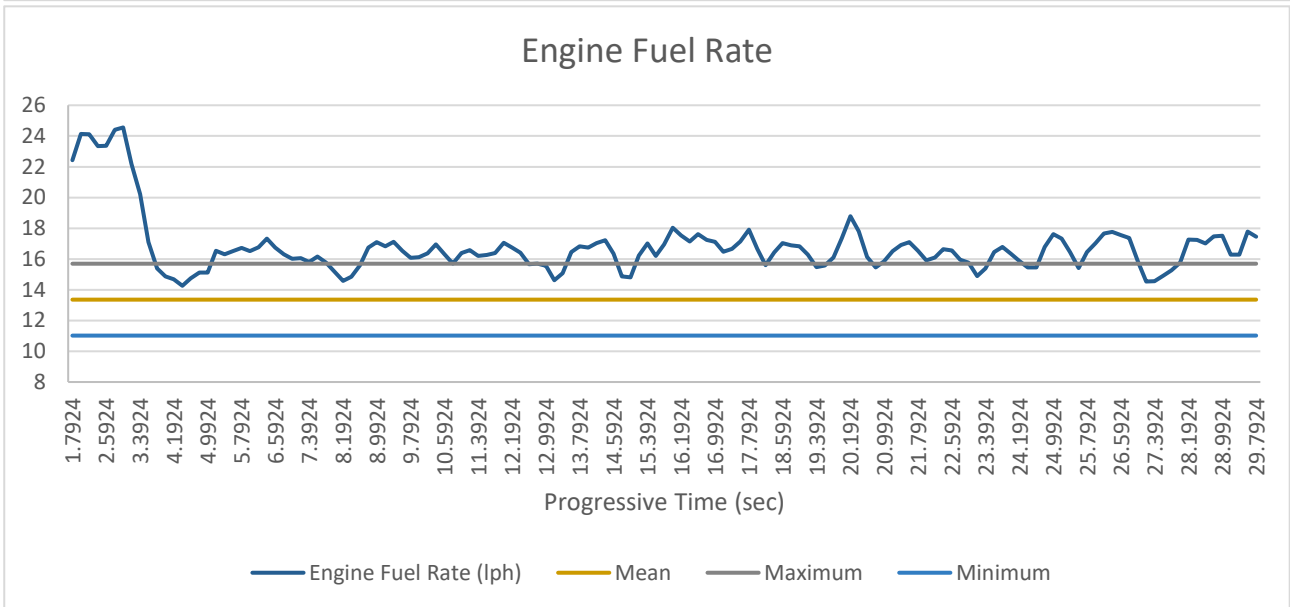
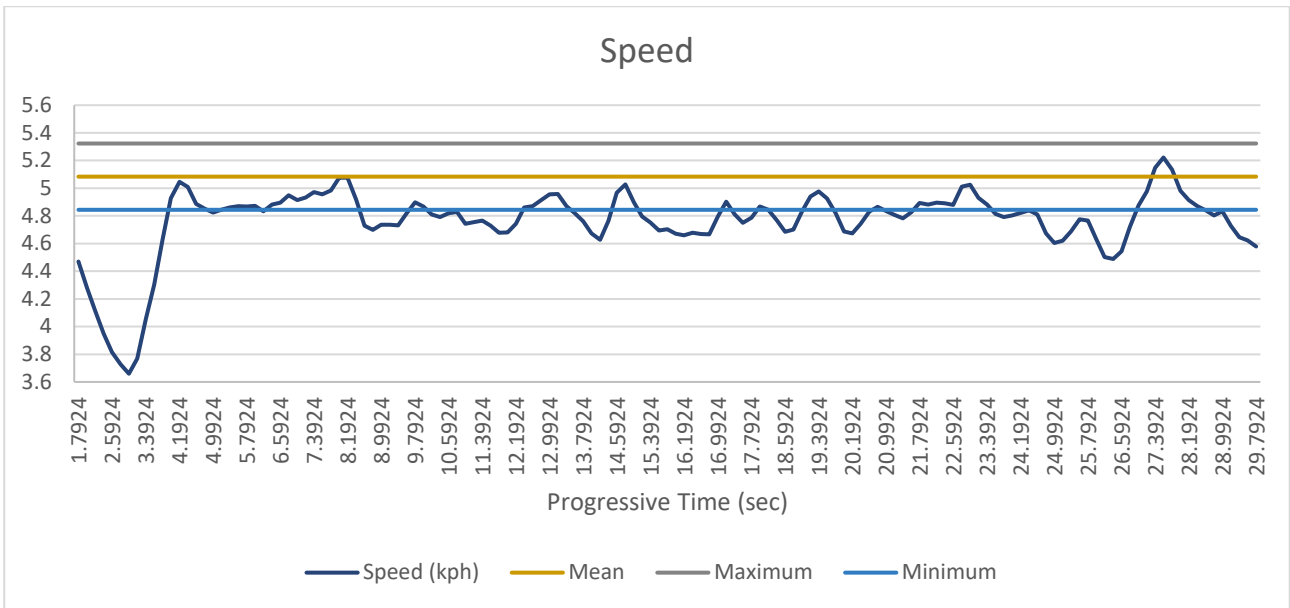


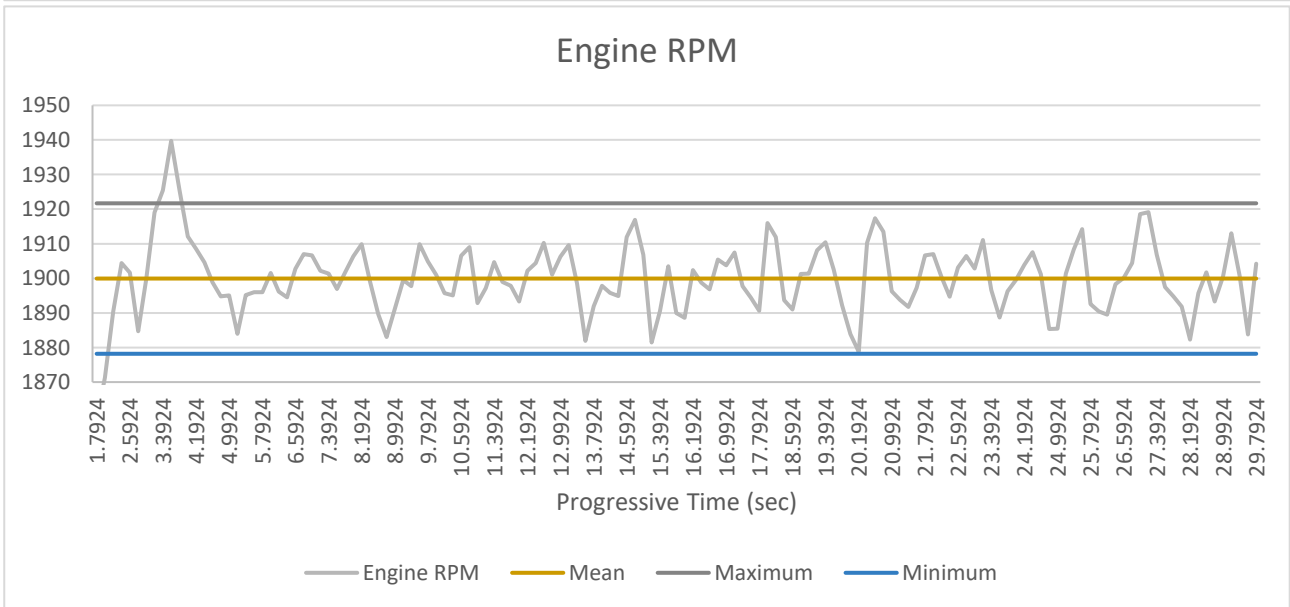
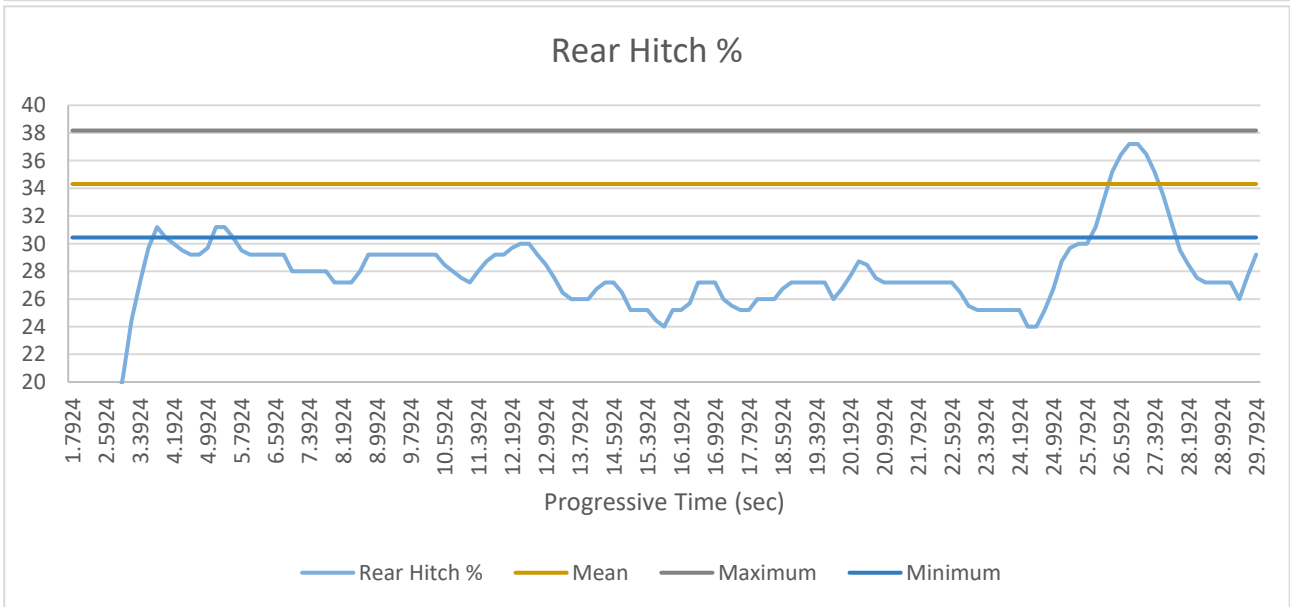
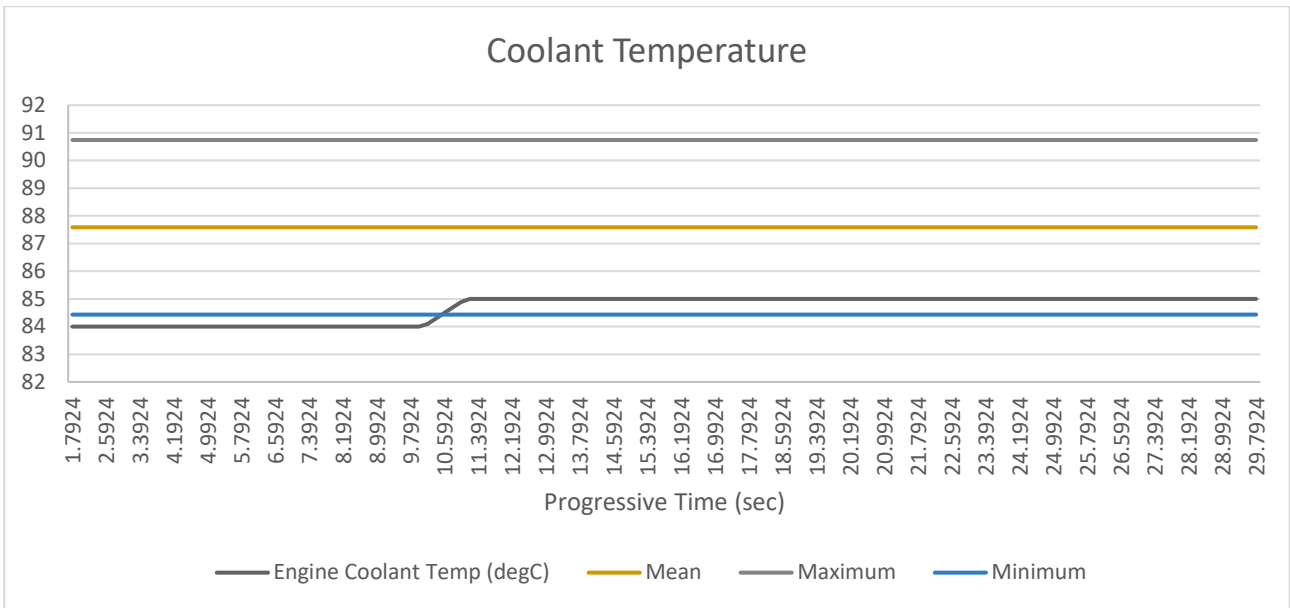




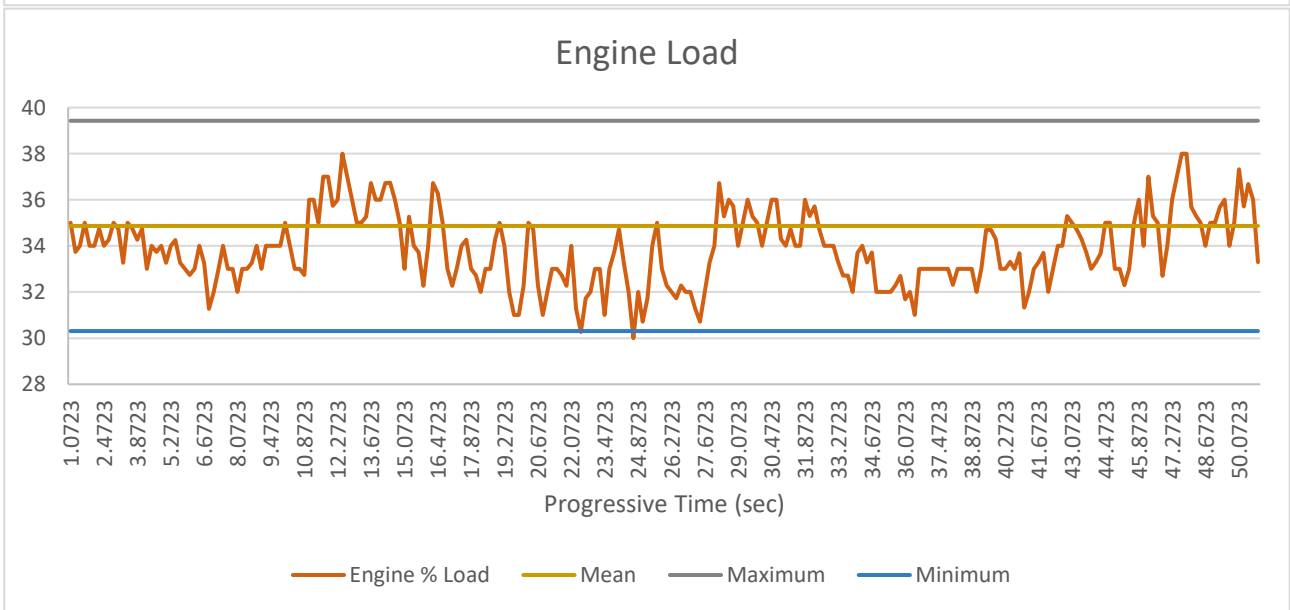
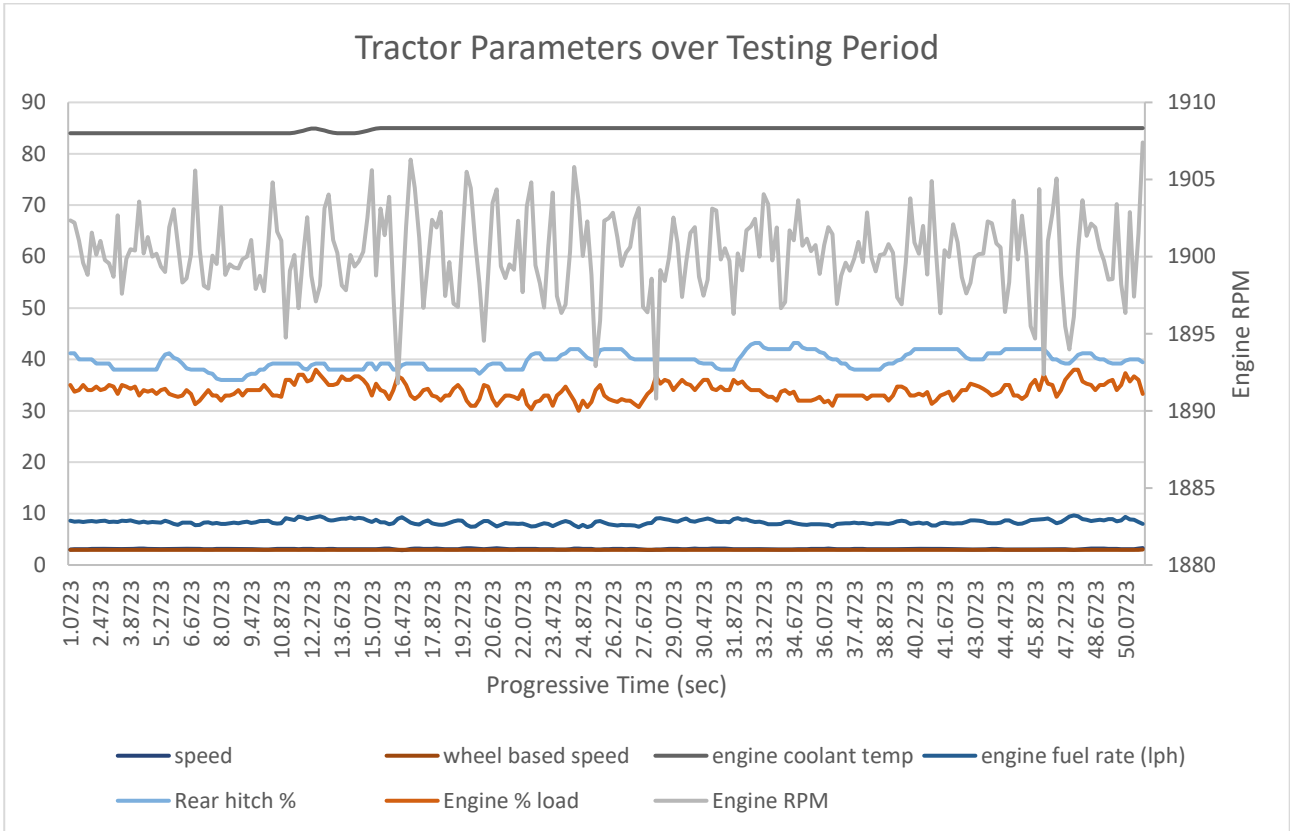
300mm – 5kph

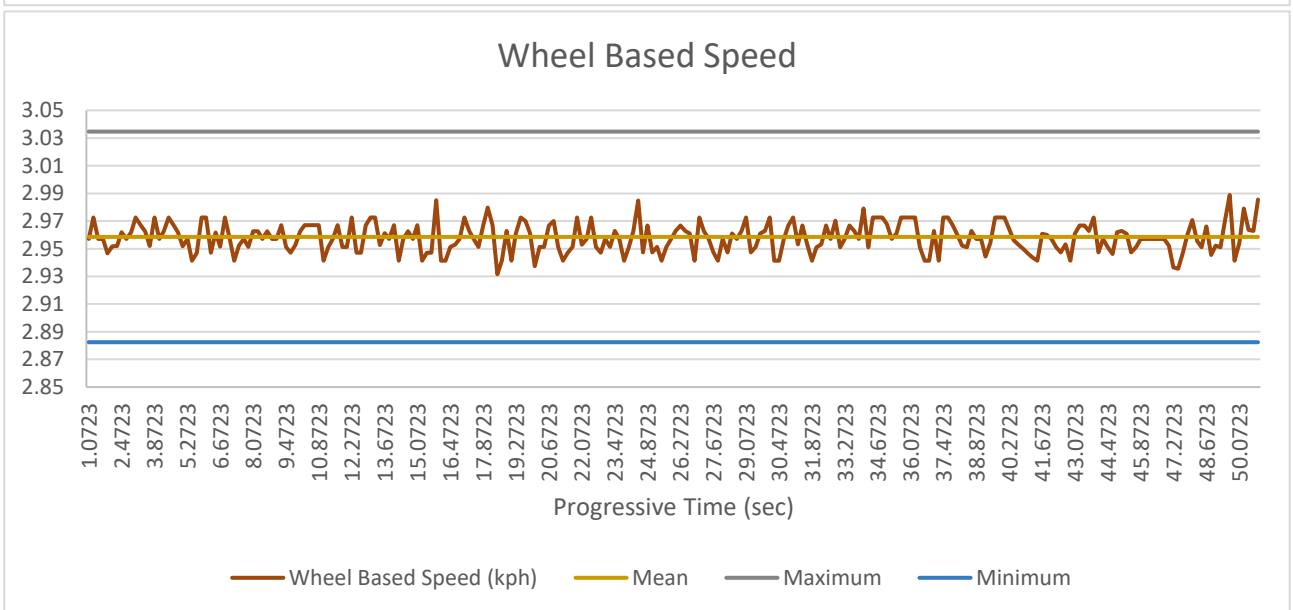
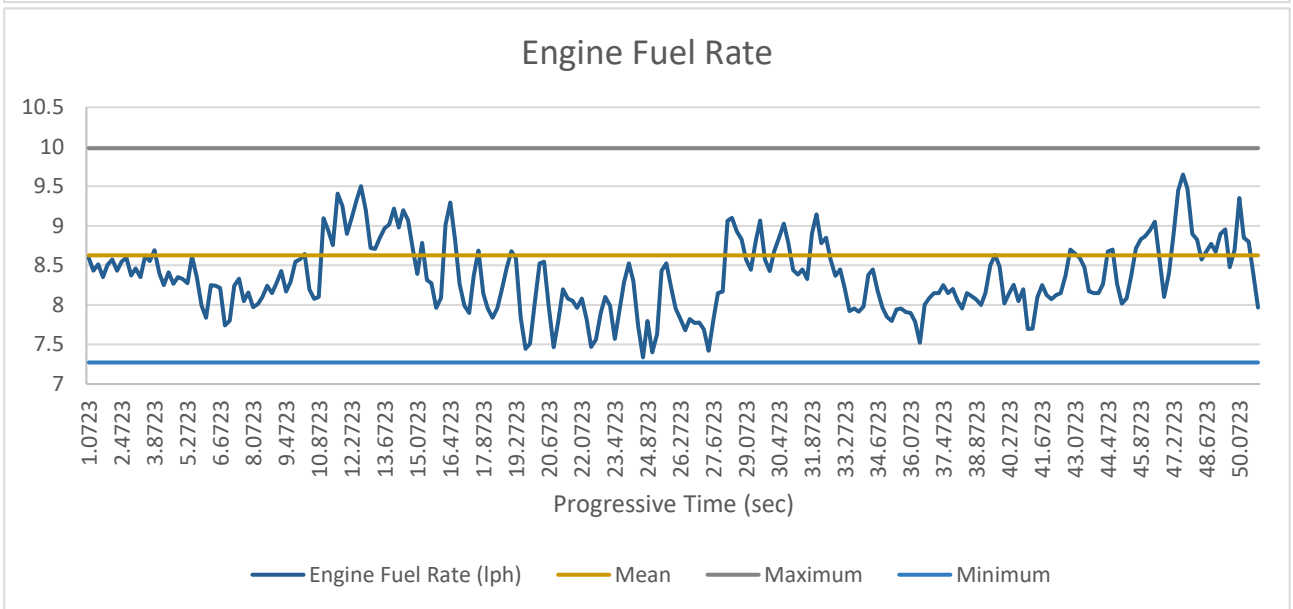
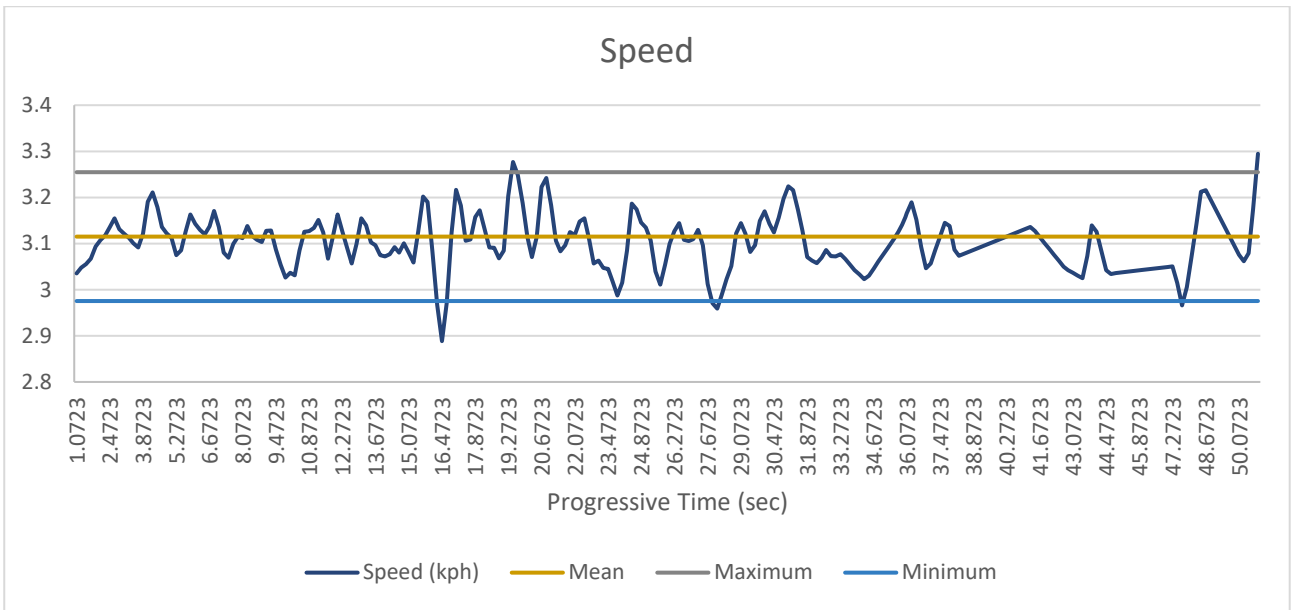




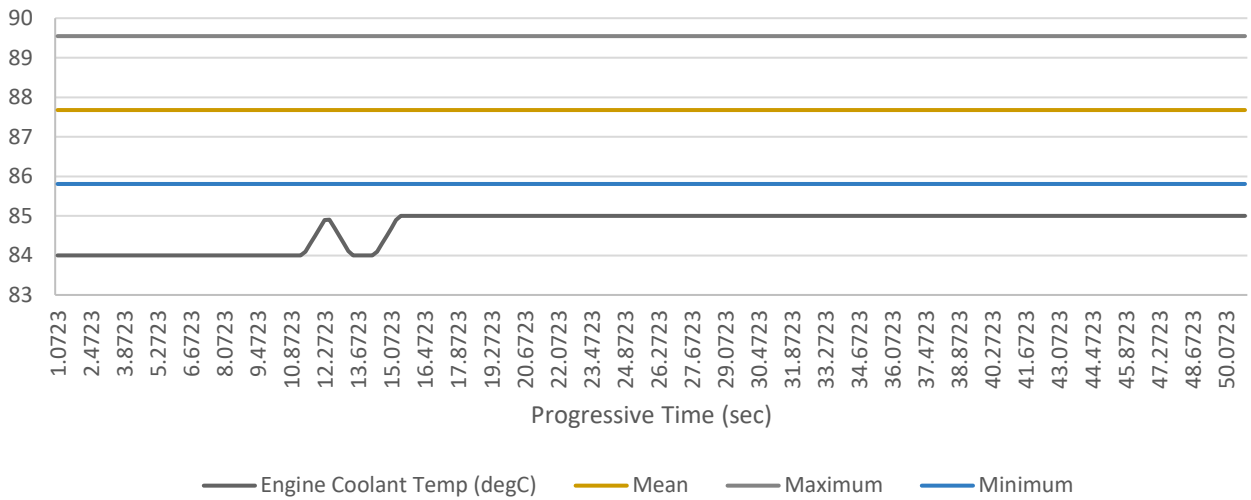


200mm – 3kph

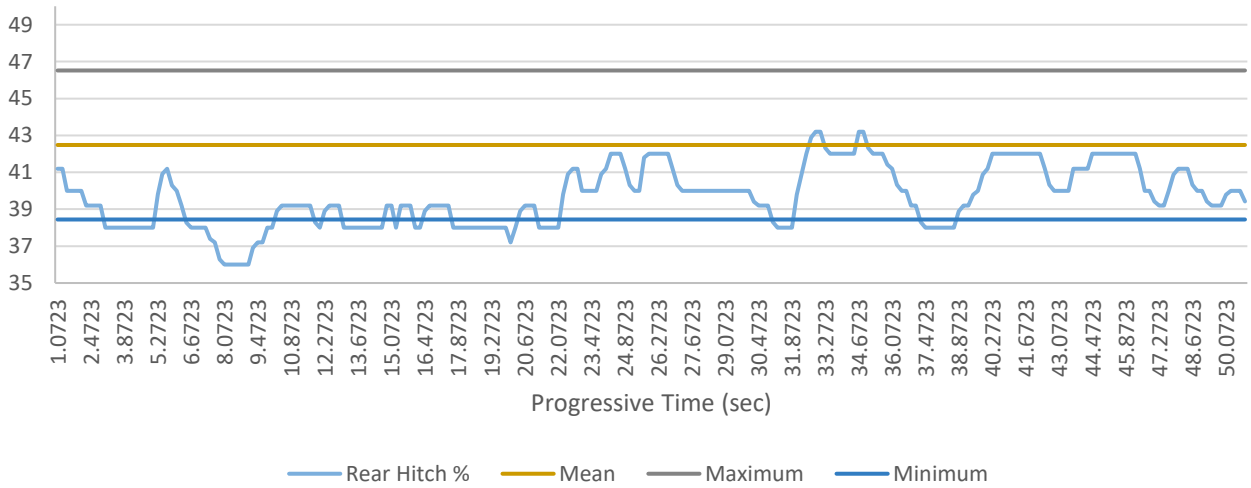




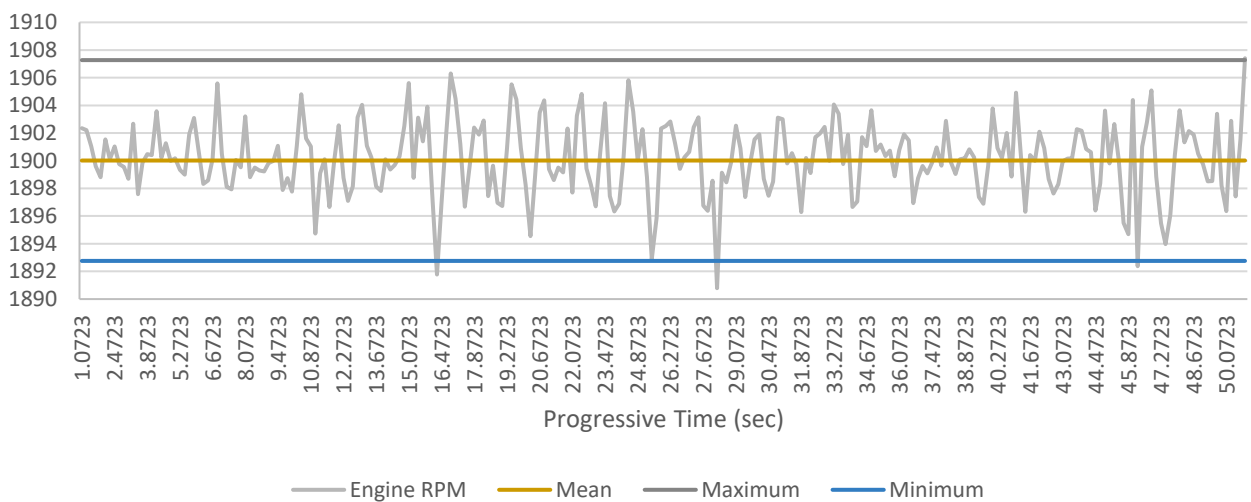
Coolant Temperature



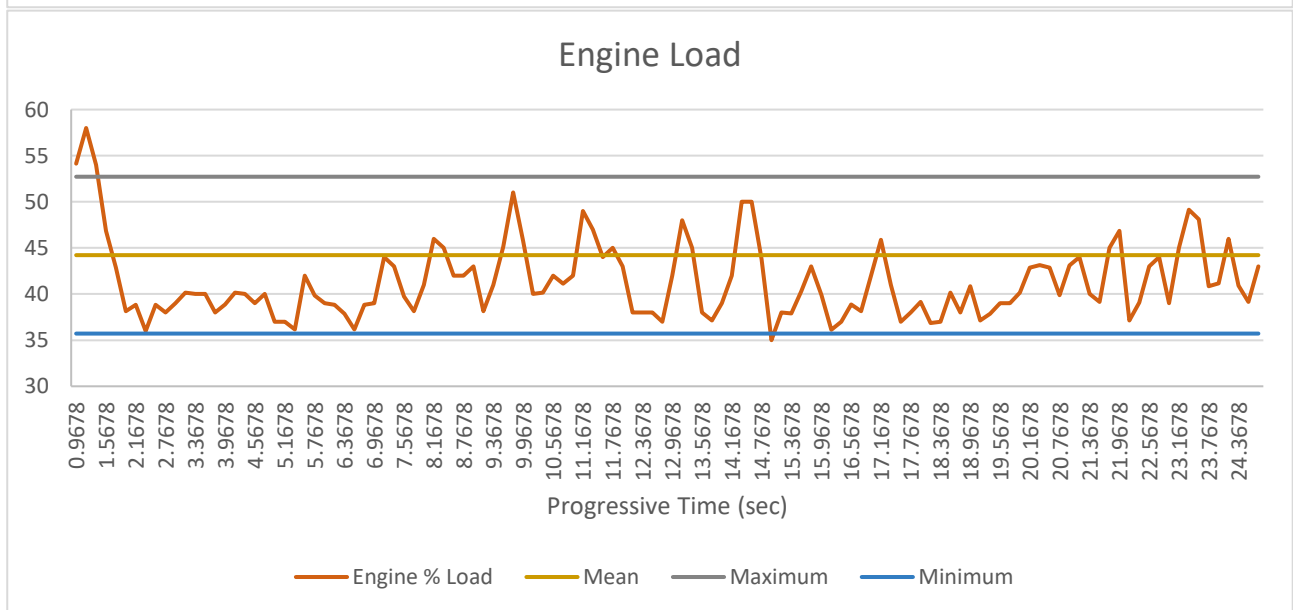
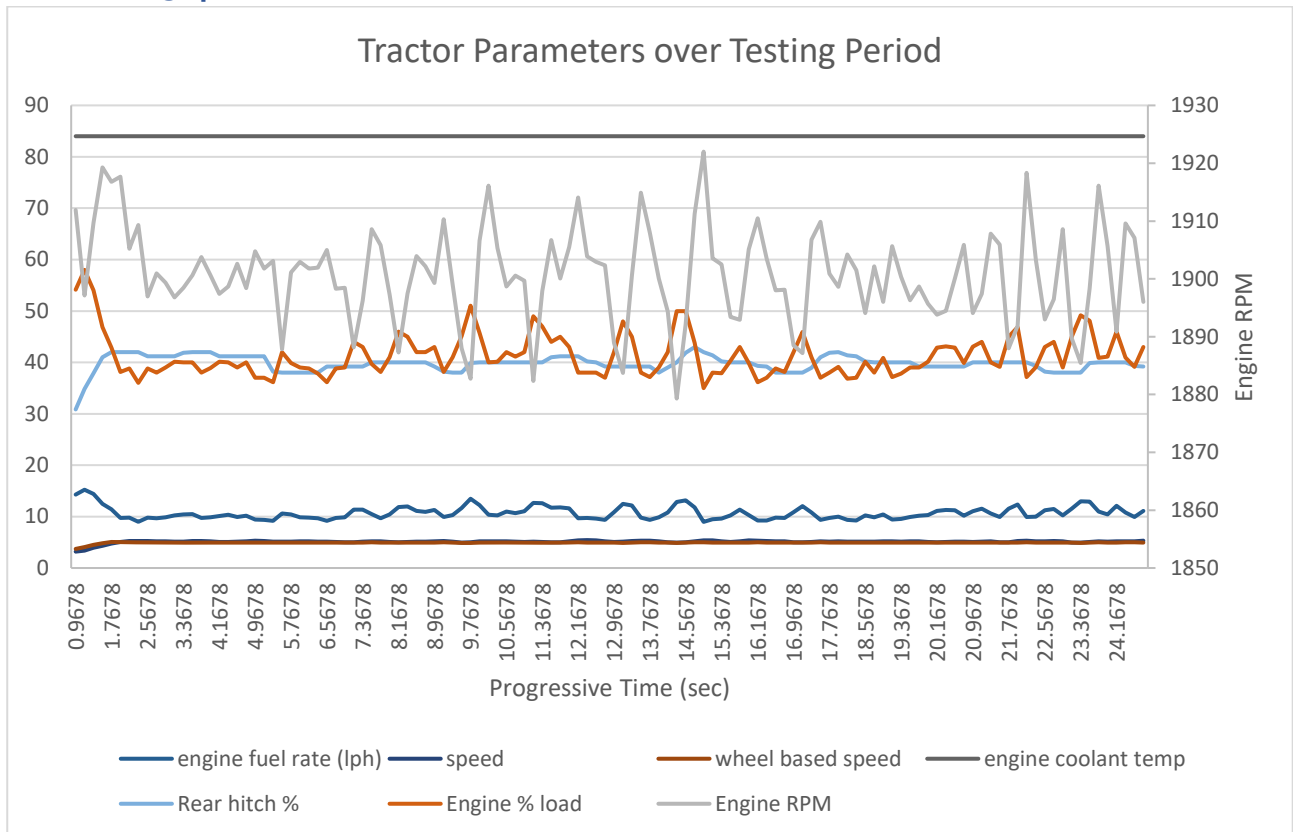
Rear Hitch %

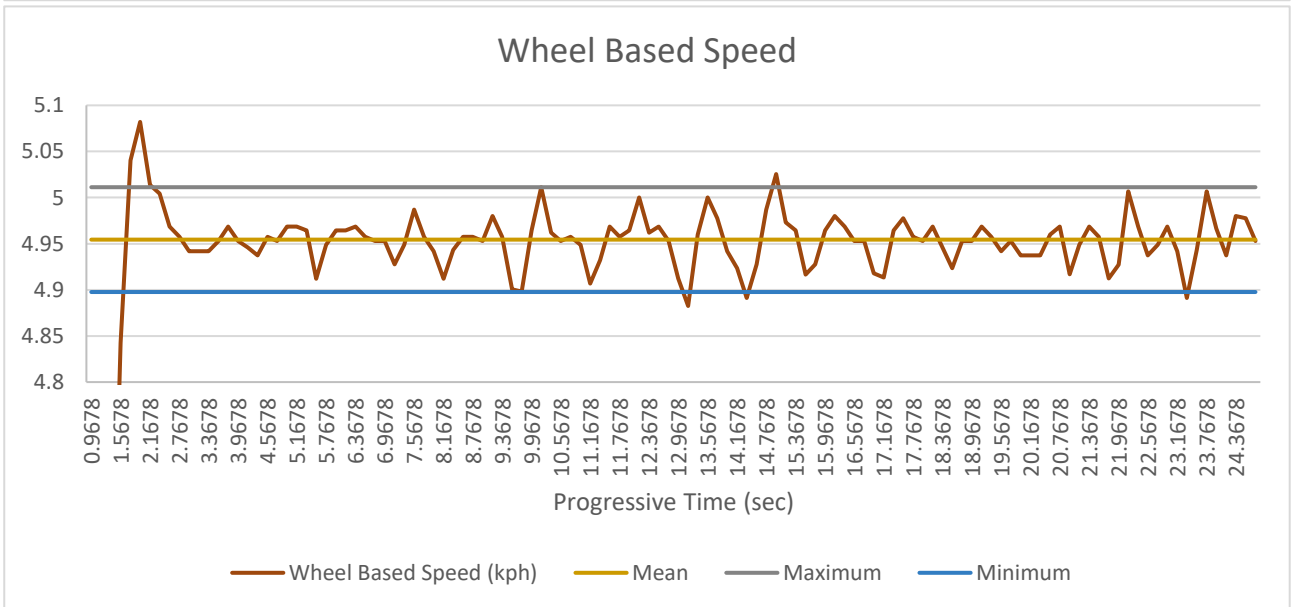
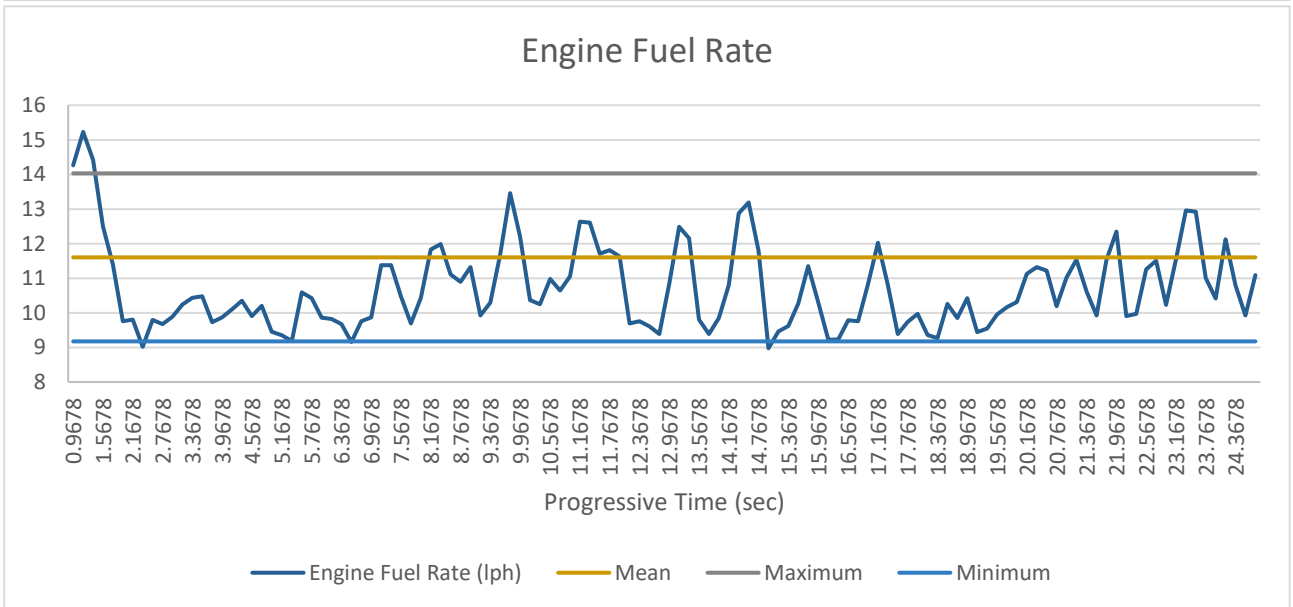
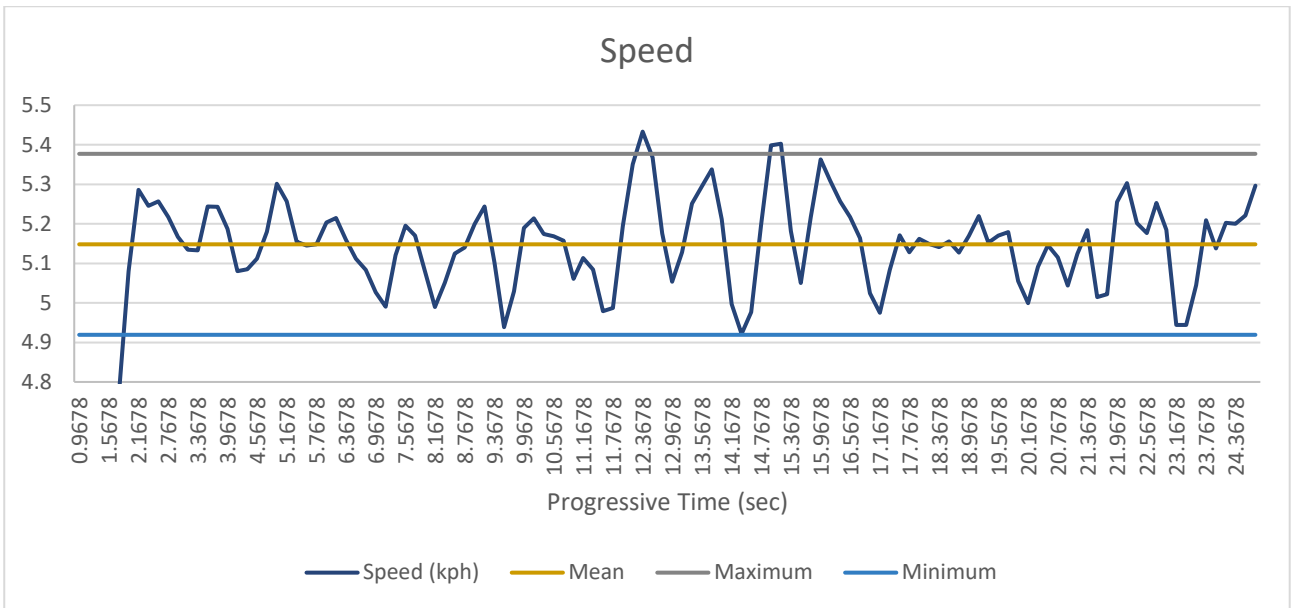


Engine RPM

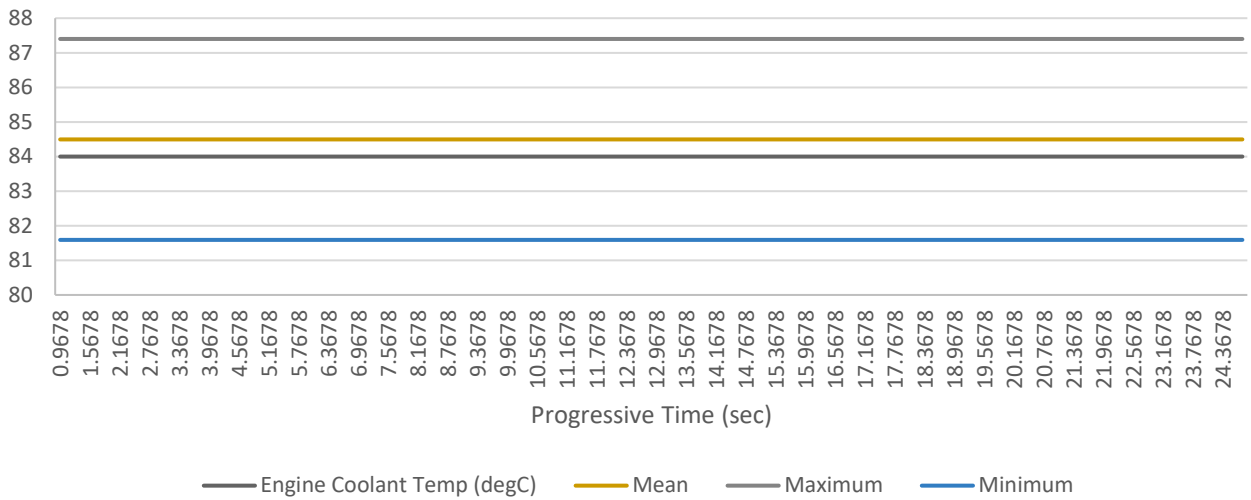


200mm – 5kph

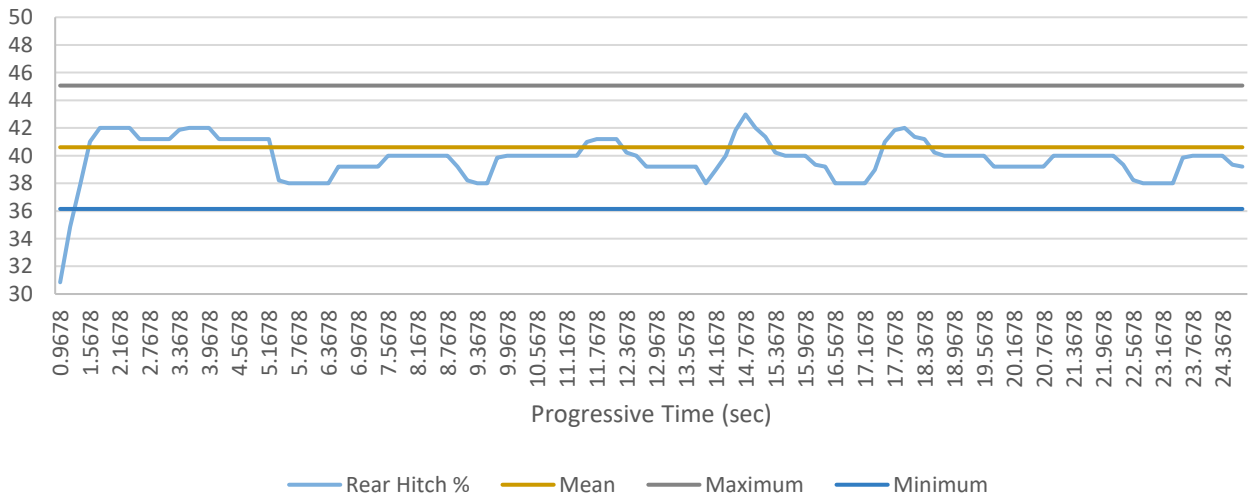




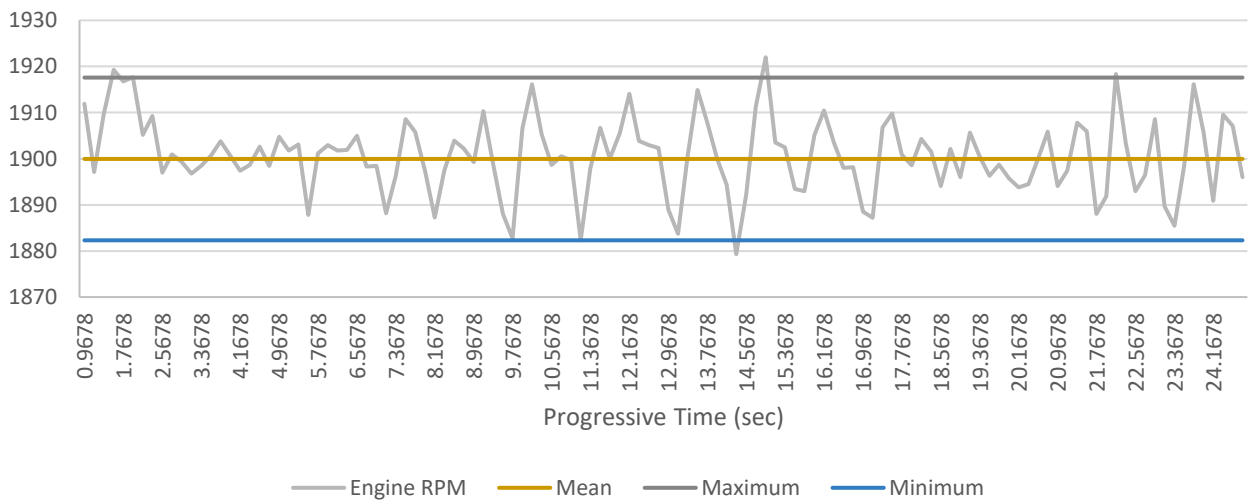
Coolant Temperature



Rear Hitch %

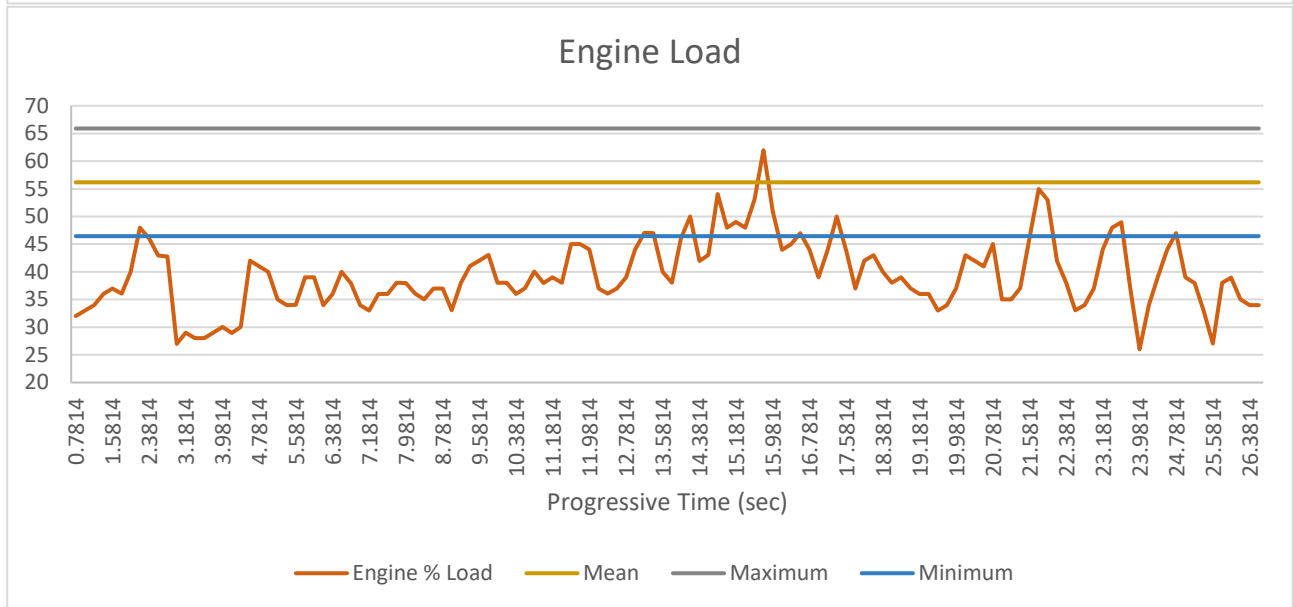
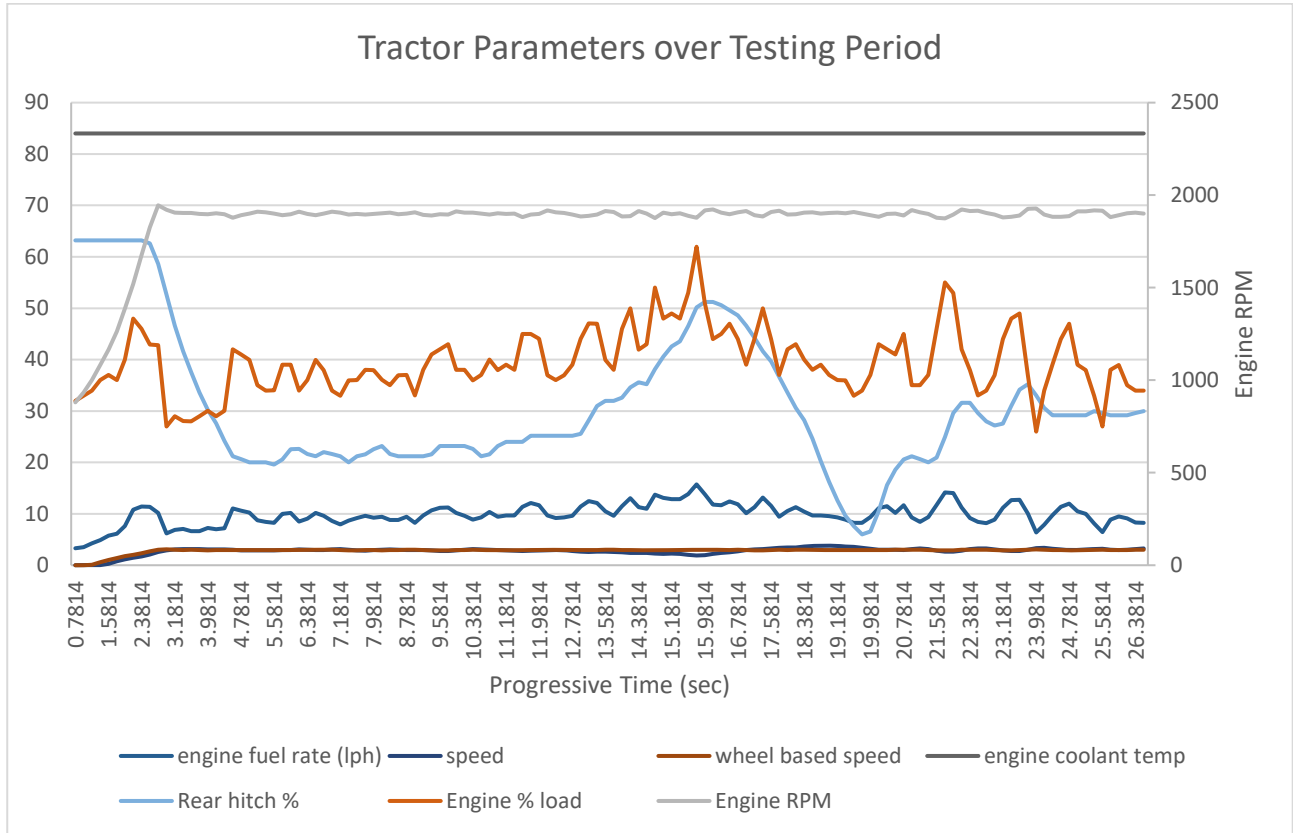


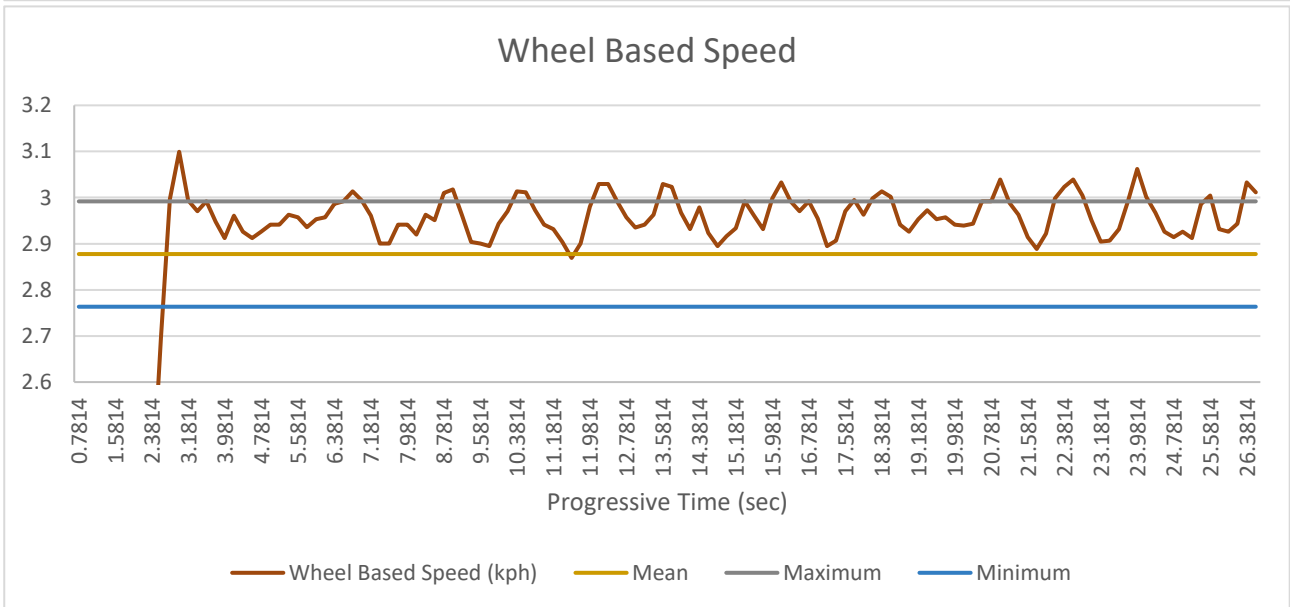
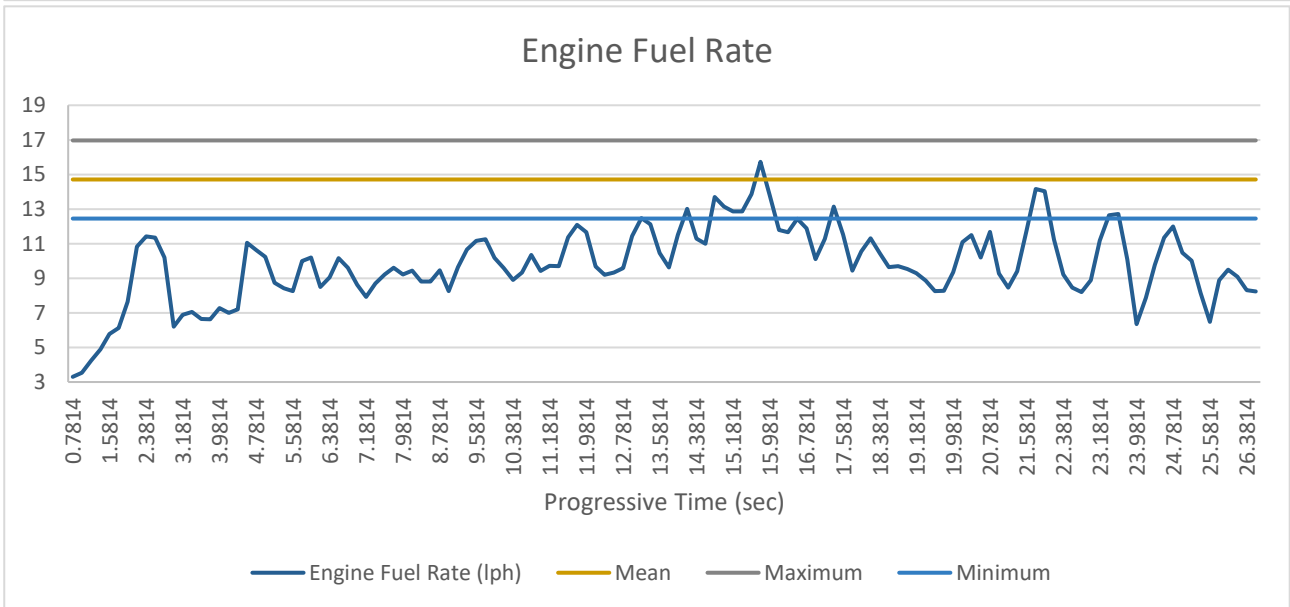
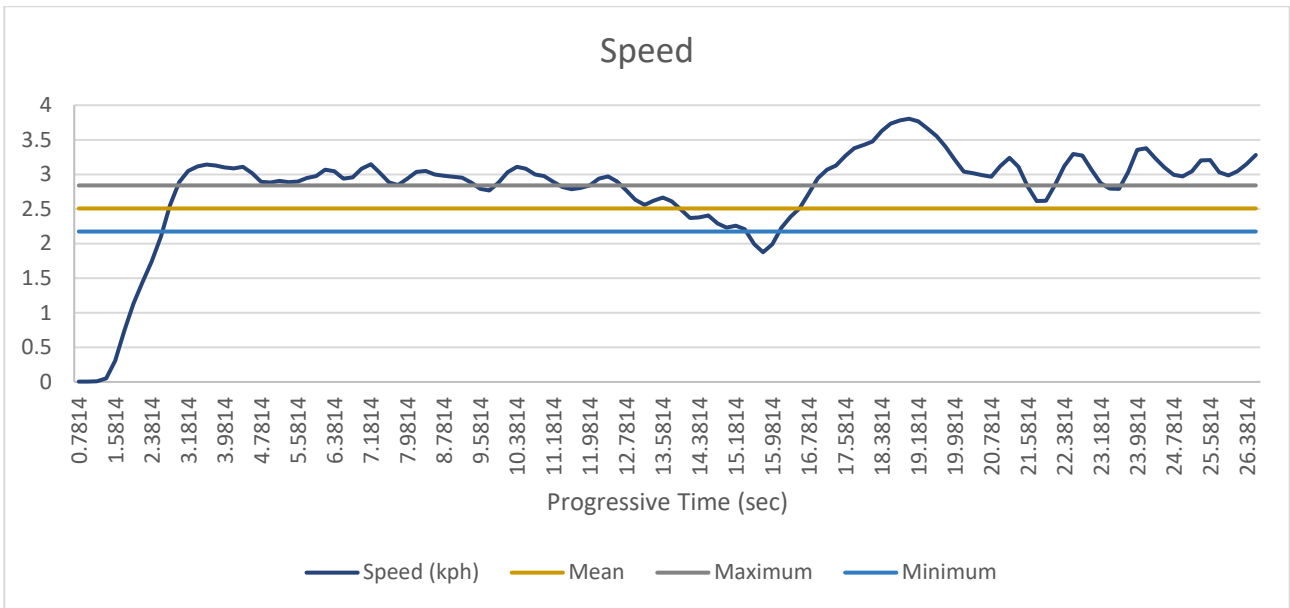
Engine RPM



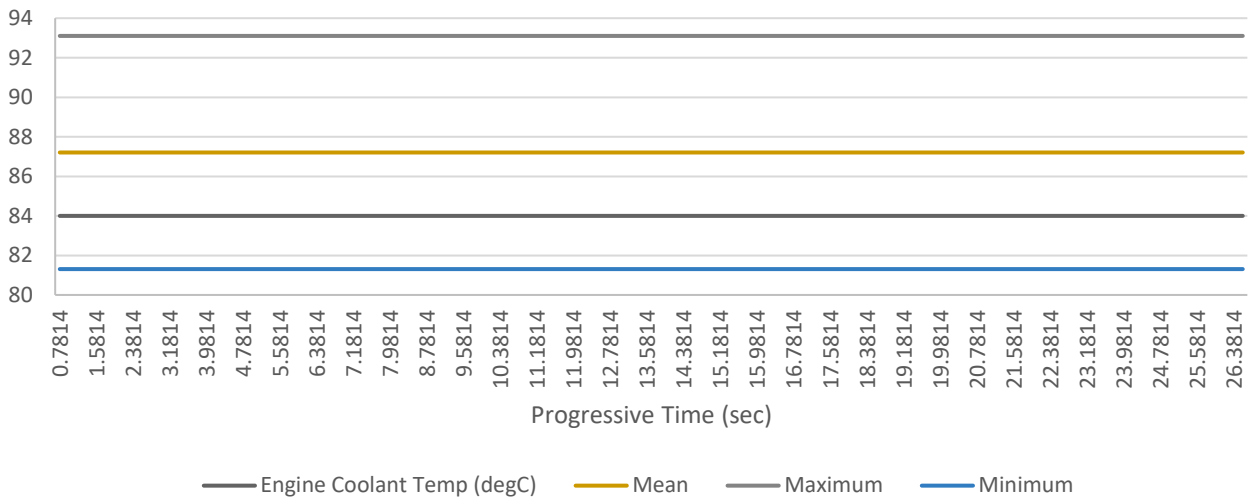
Appendix L – 3PL Deep Ripper – Traveling through washouts data

350mm – 3kph

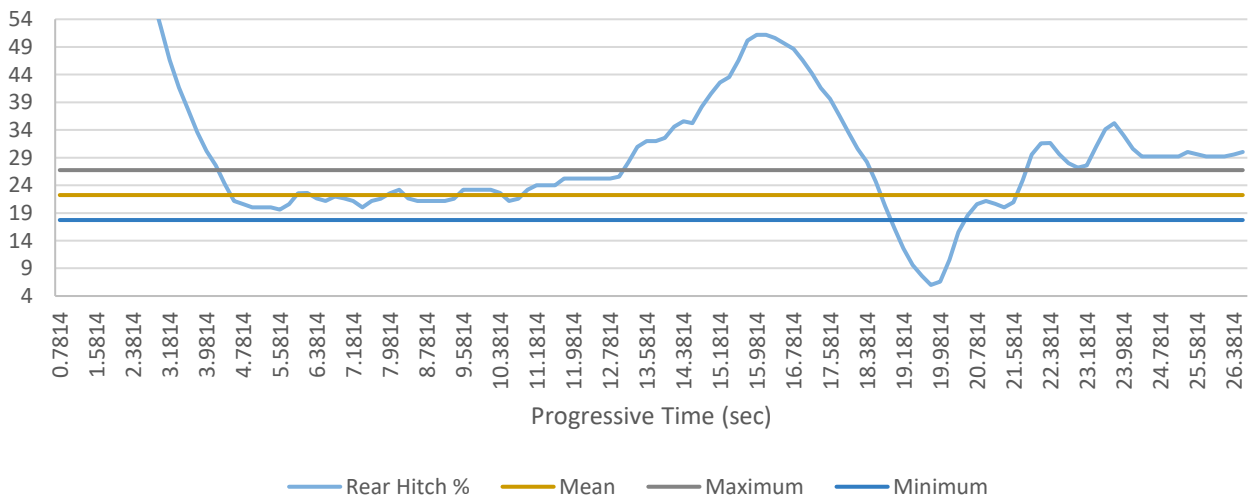




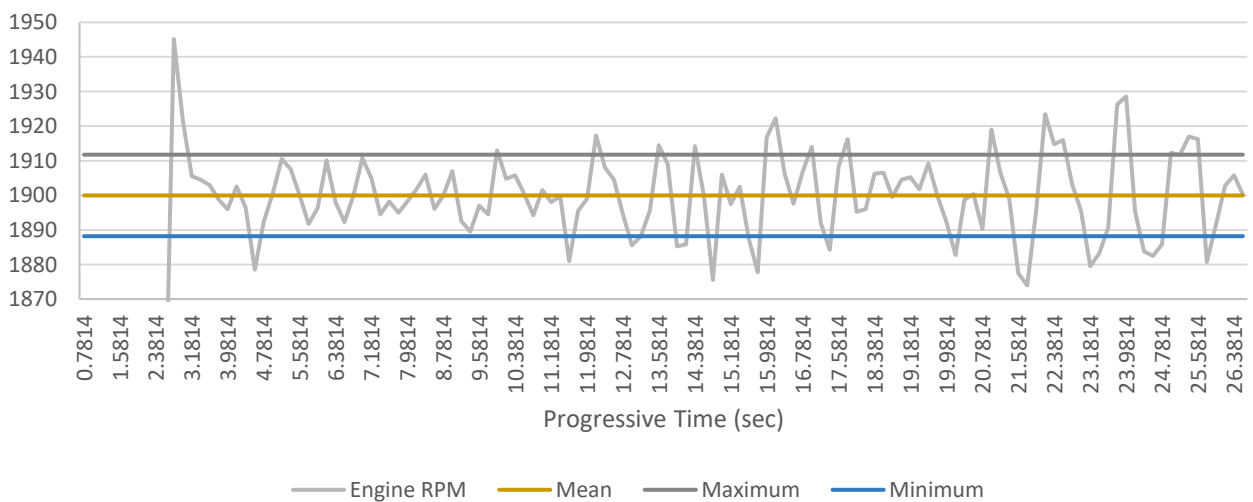
Coolant Temperature



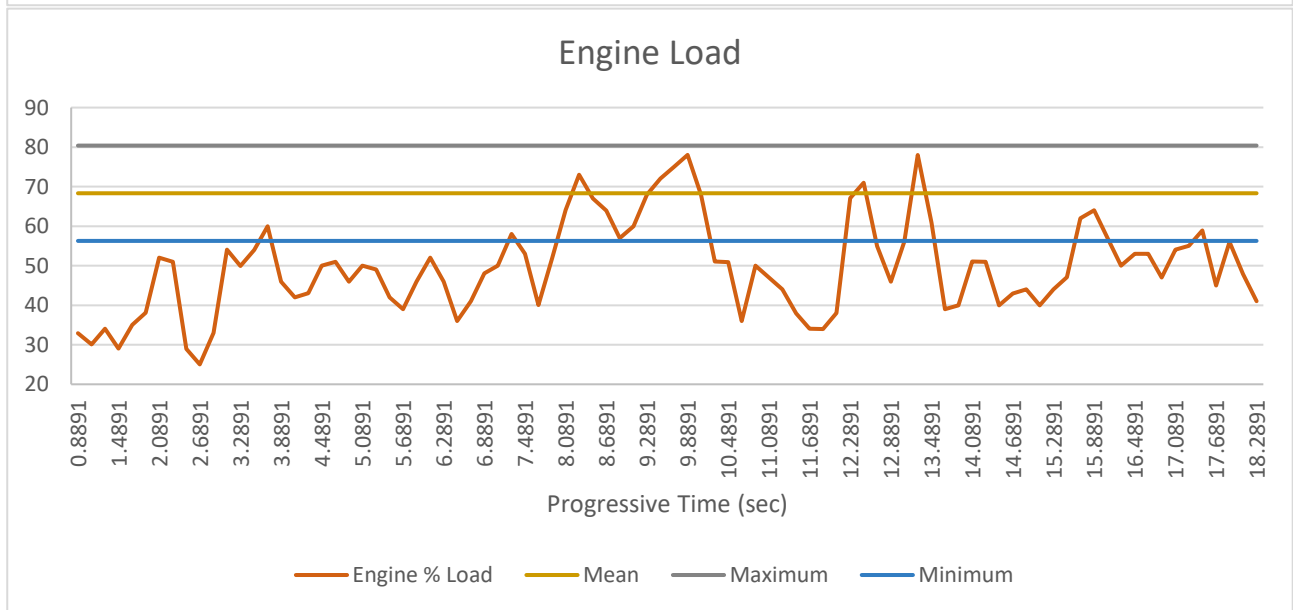
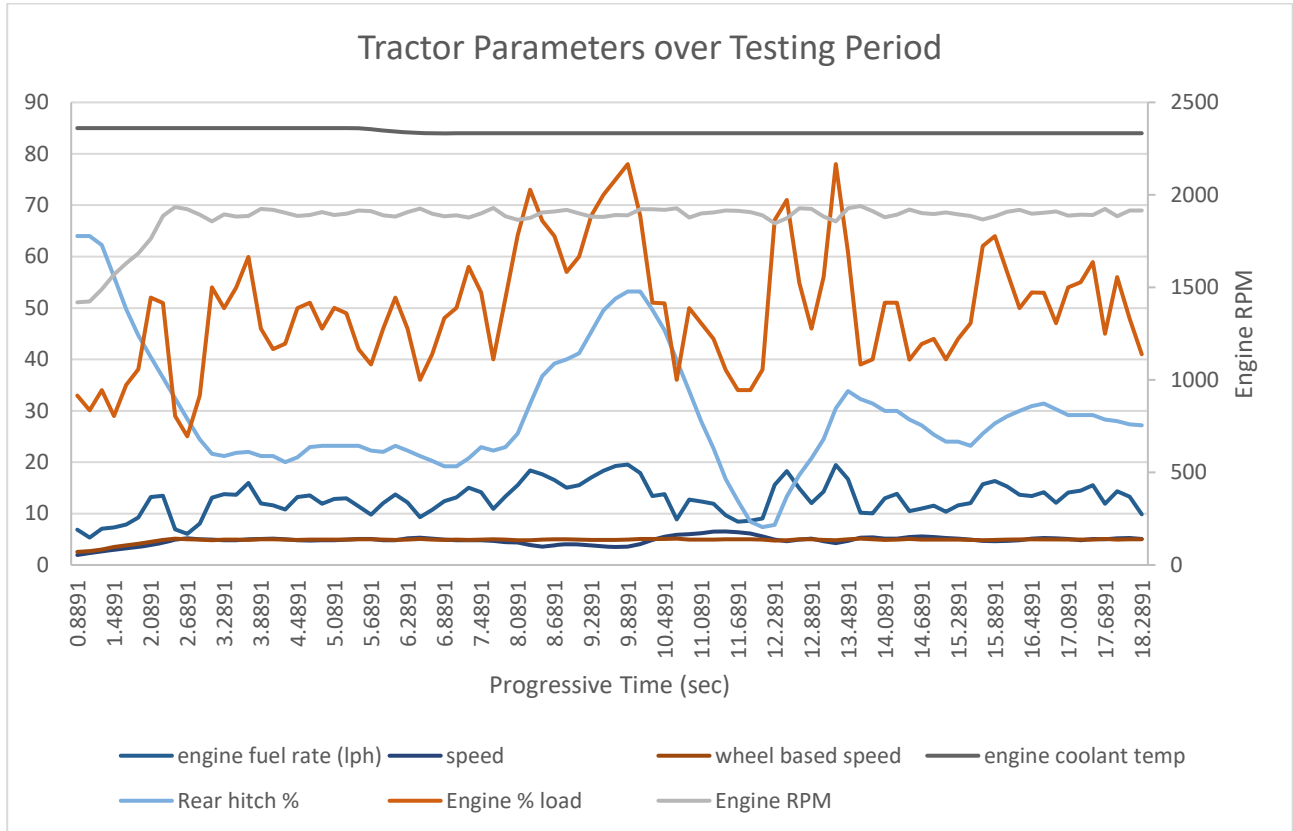
Rear Hitch %

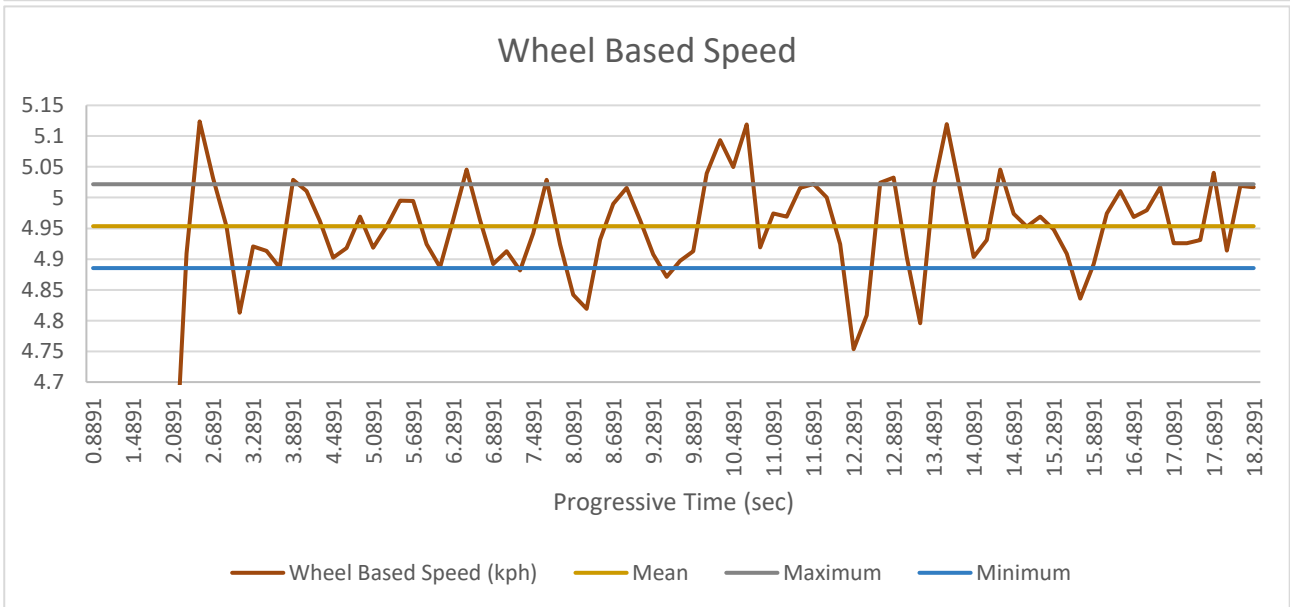
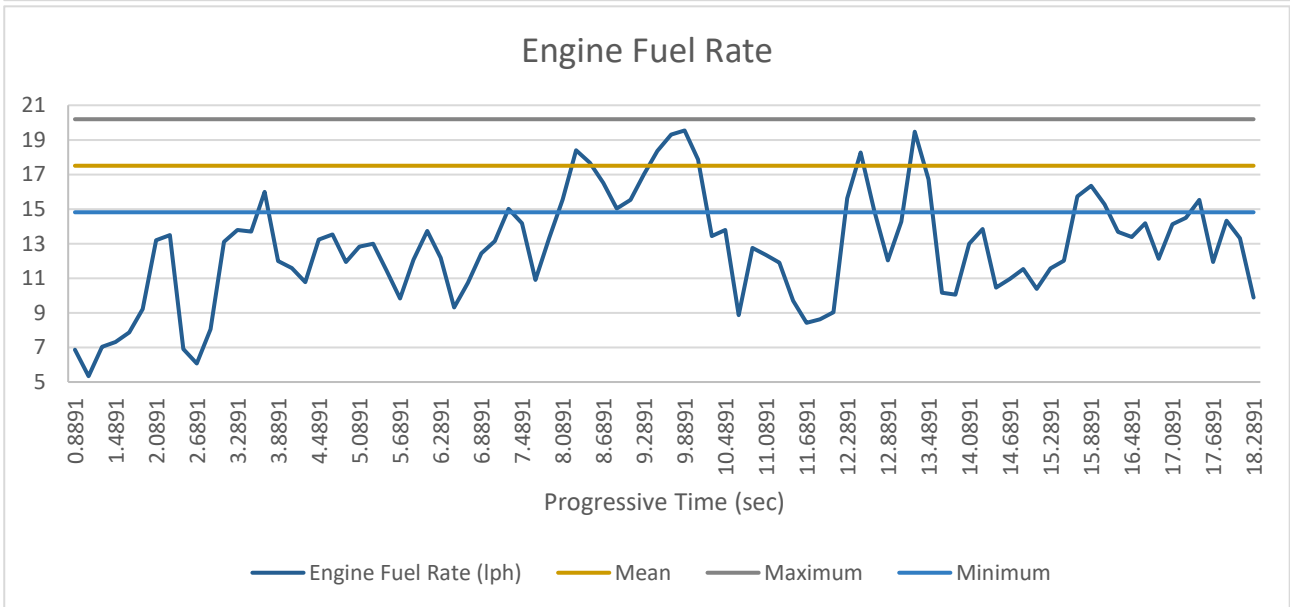
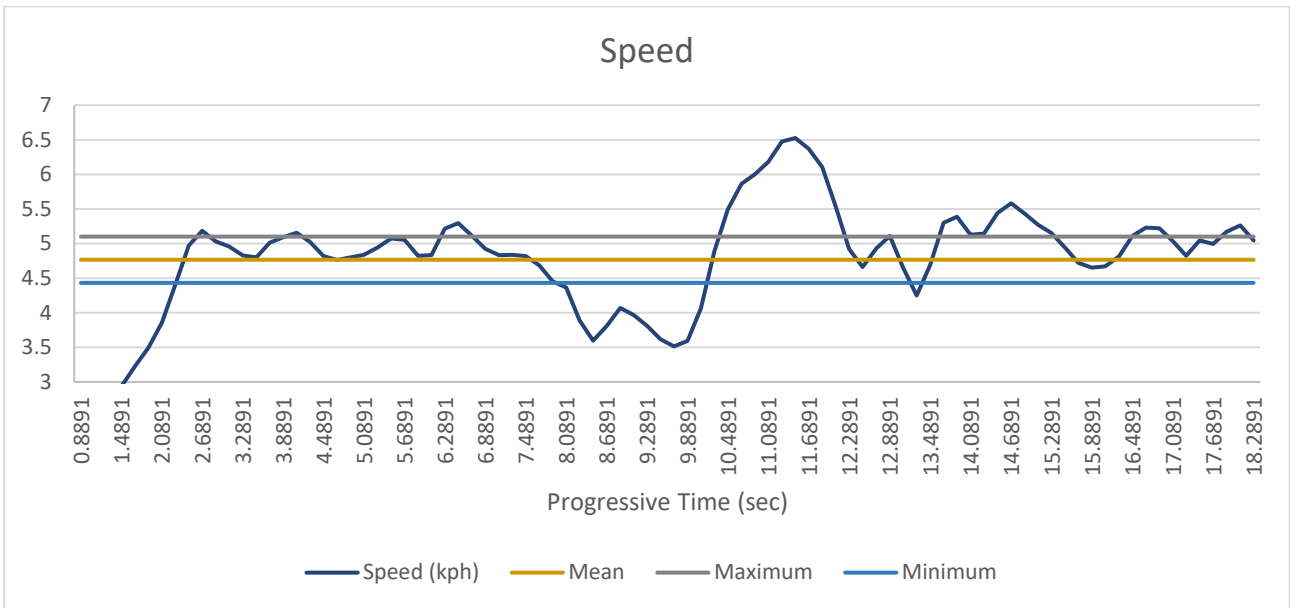


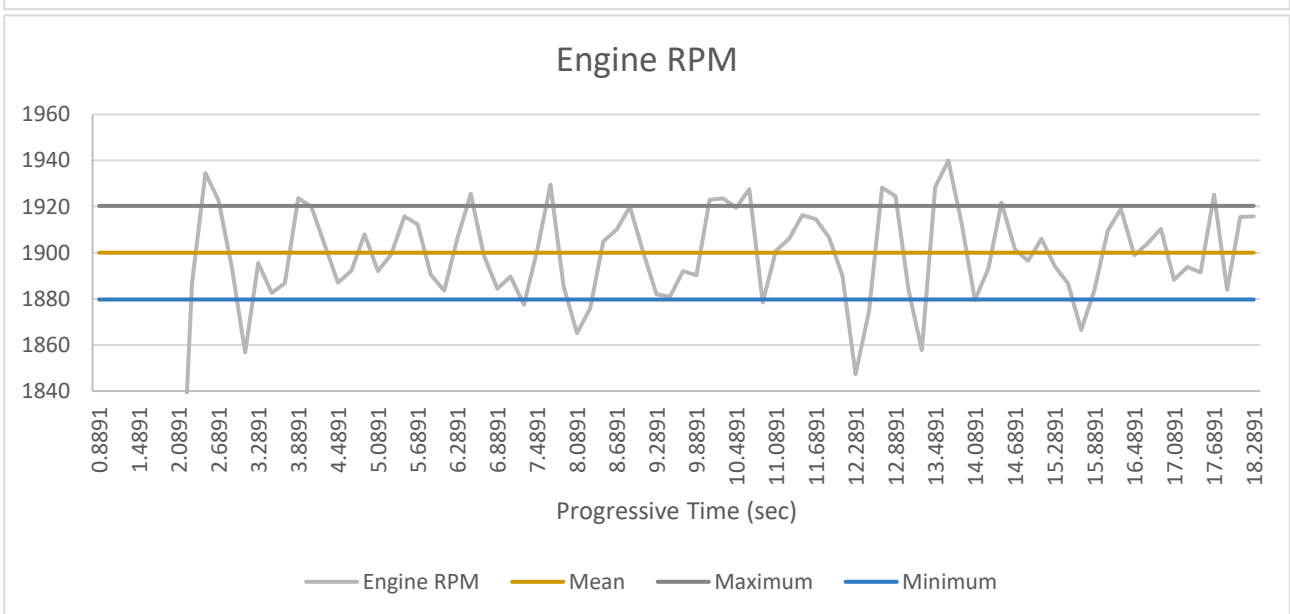
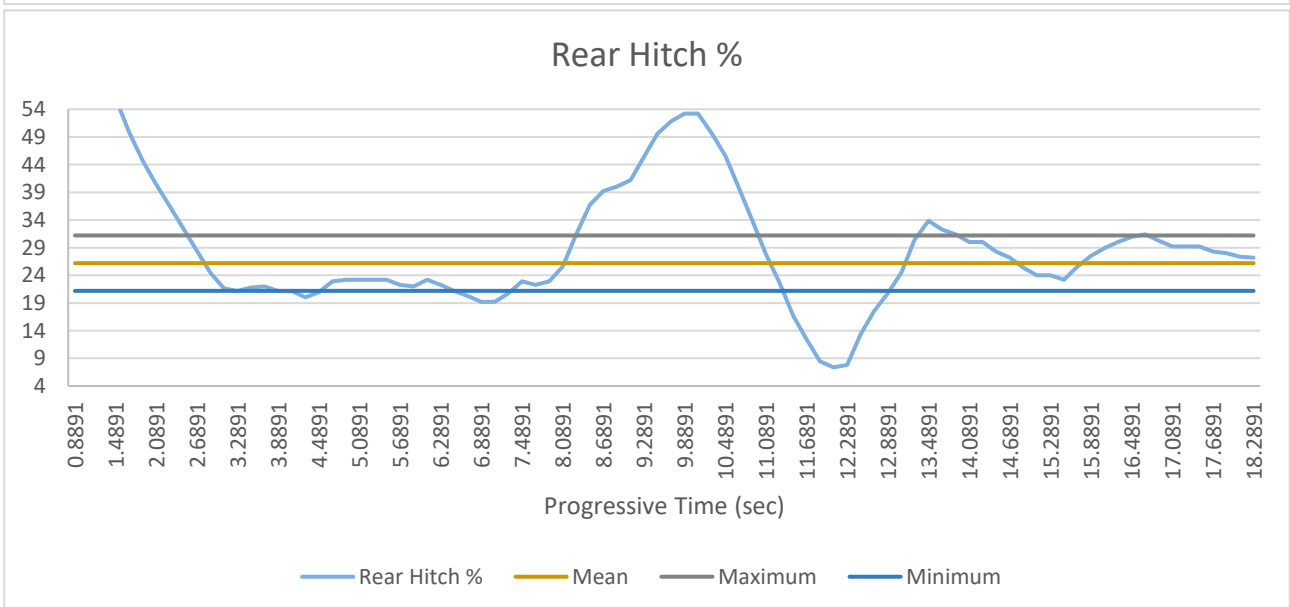
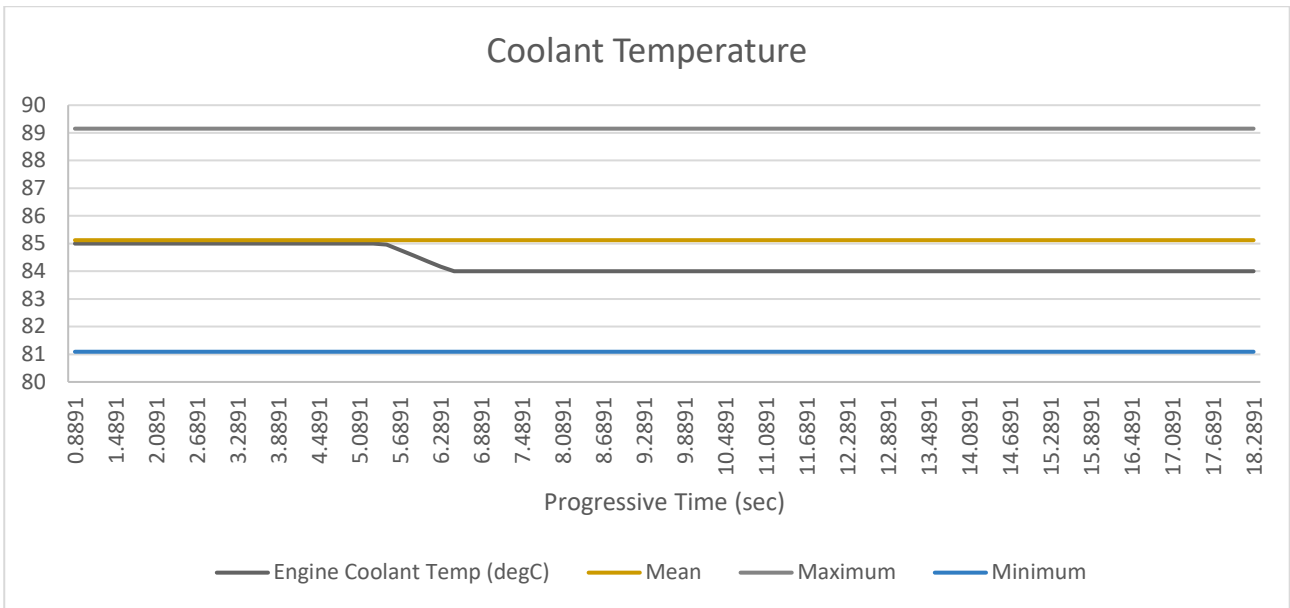
Engine RPM



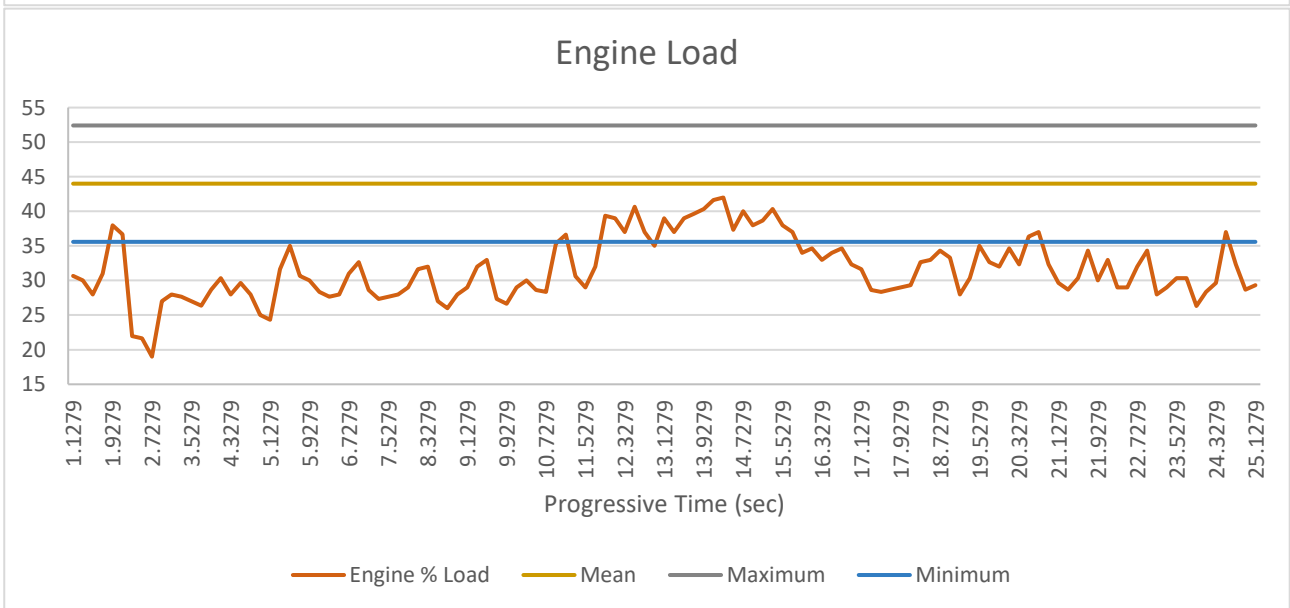
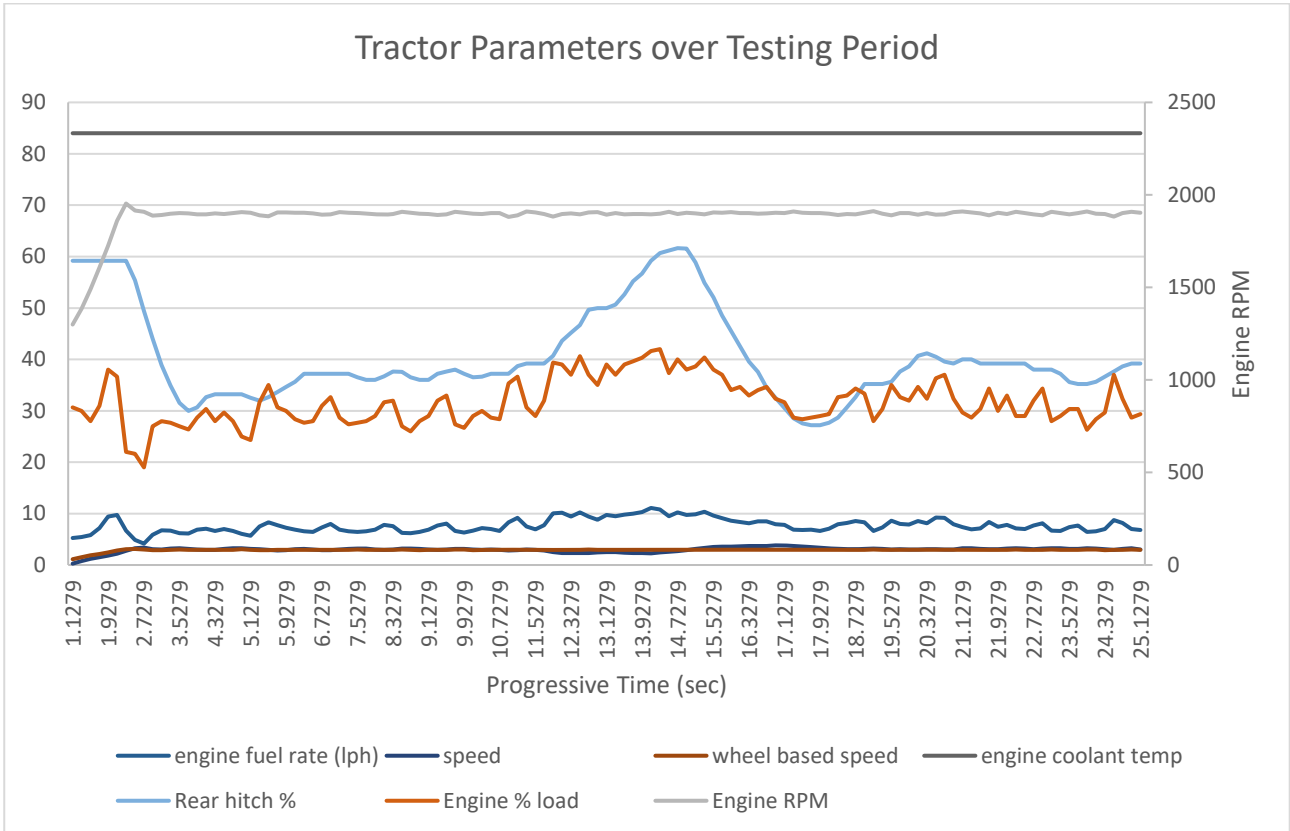
350mm – 5kph

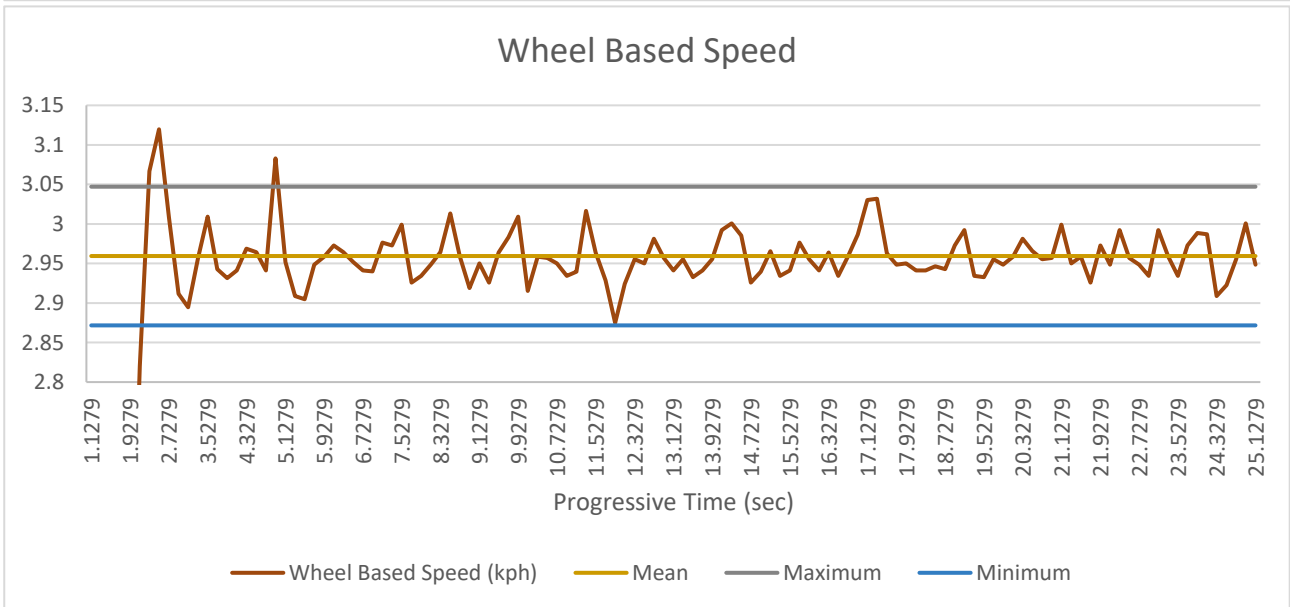
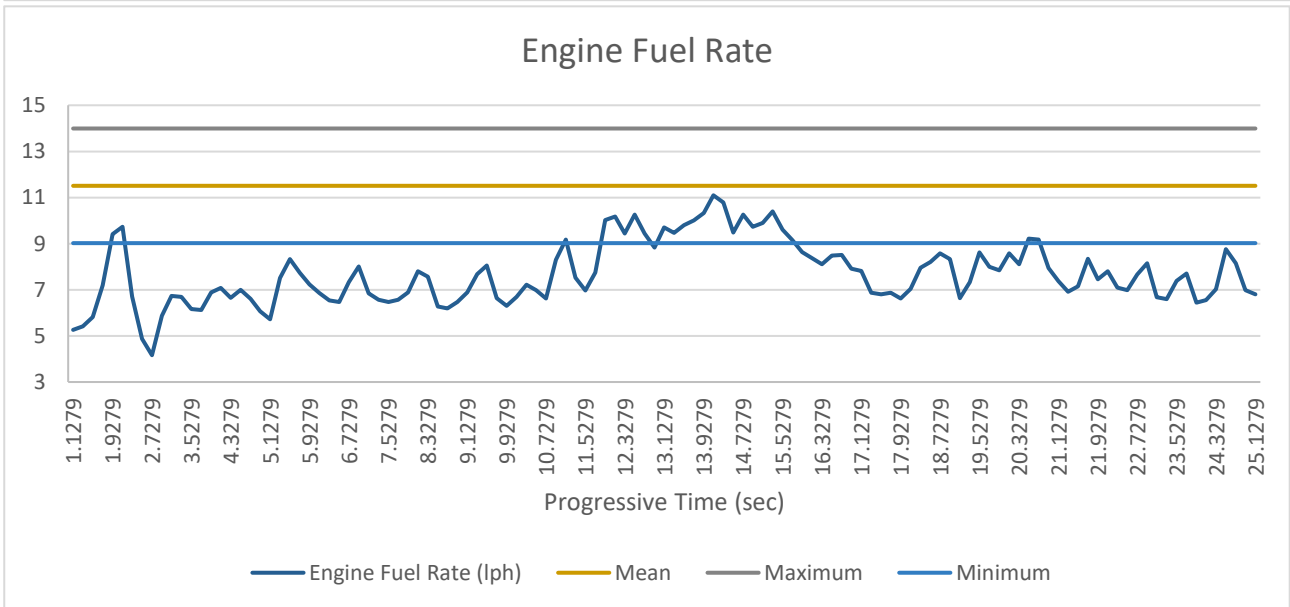
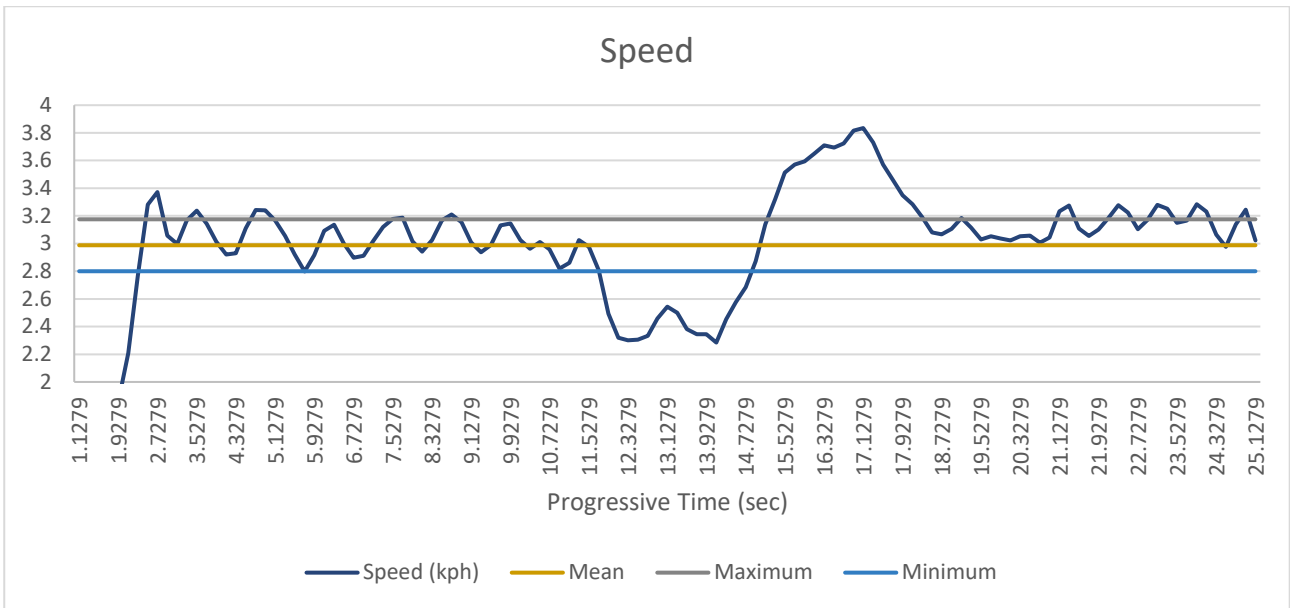


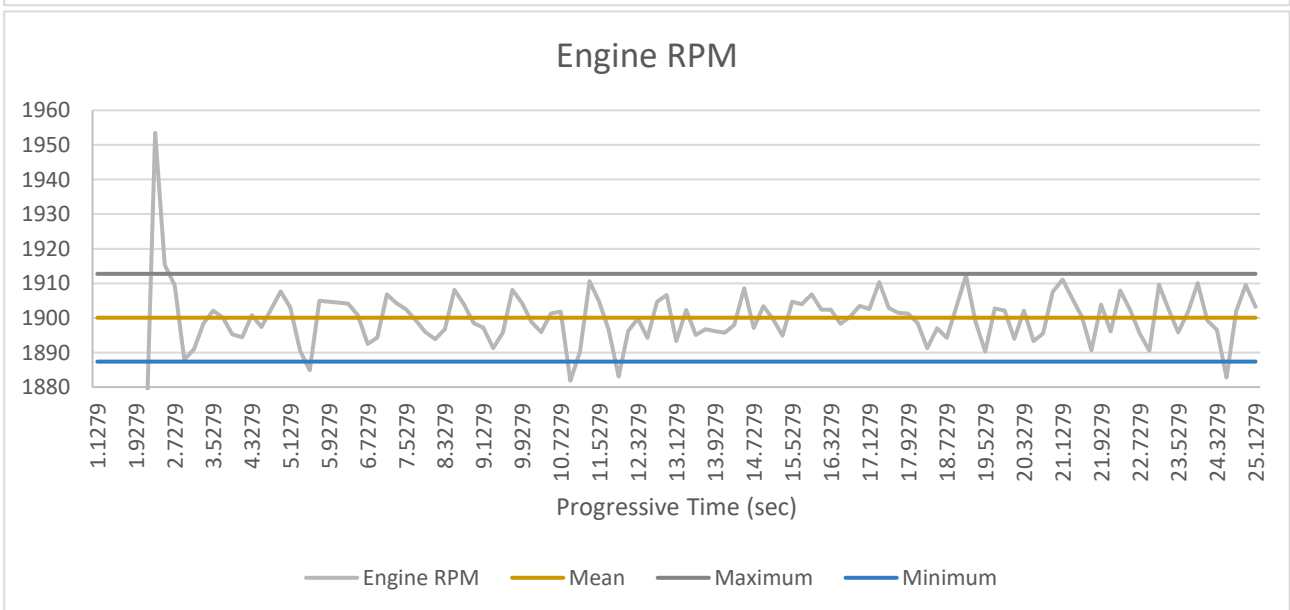
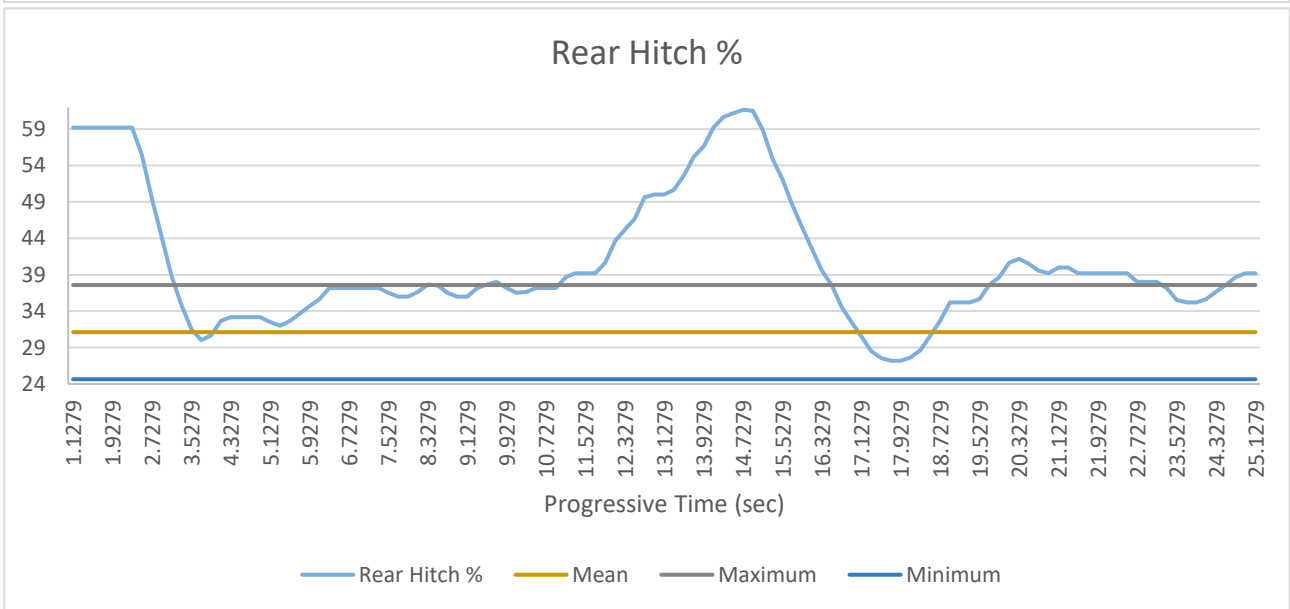
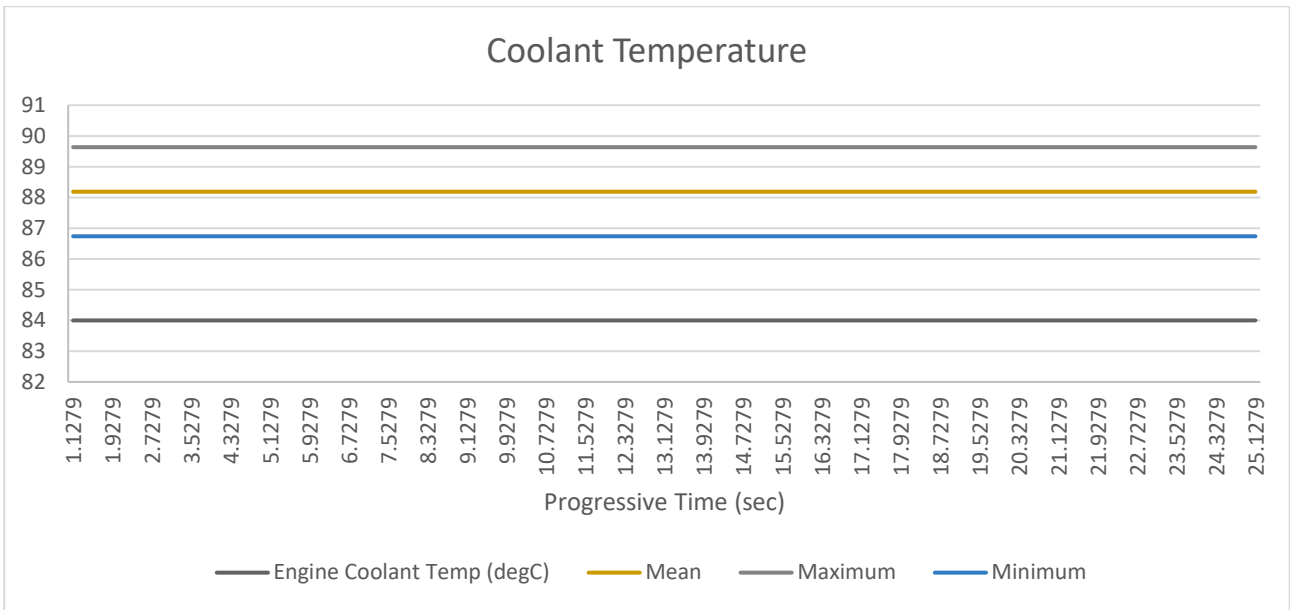




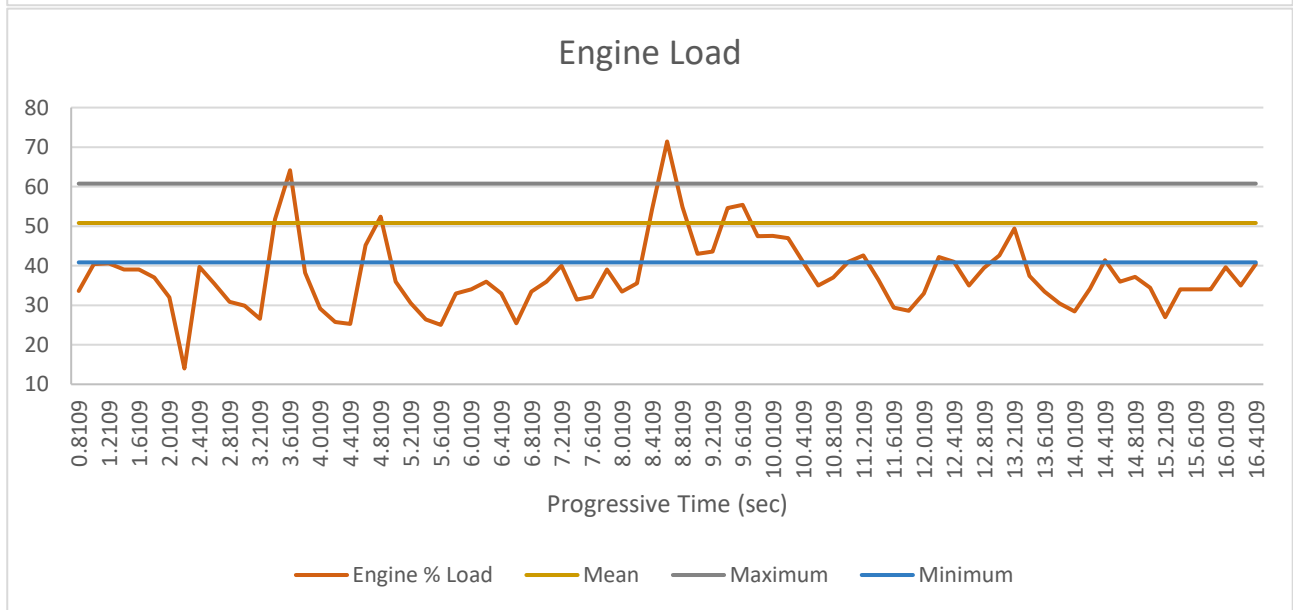
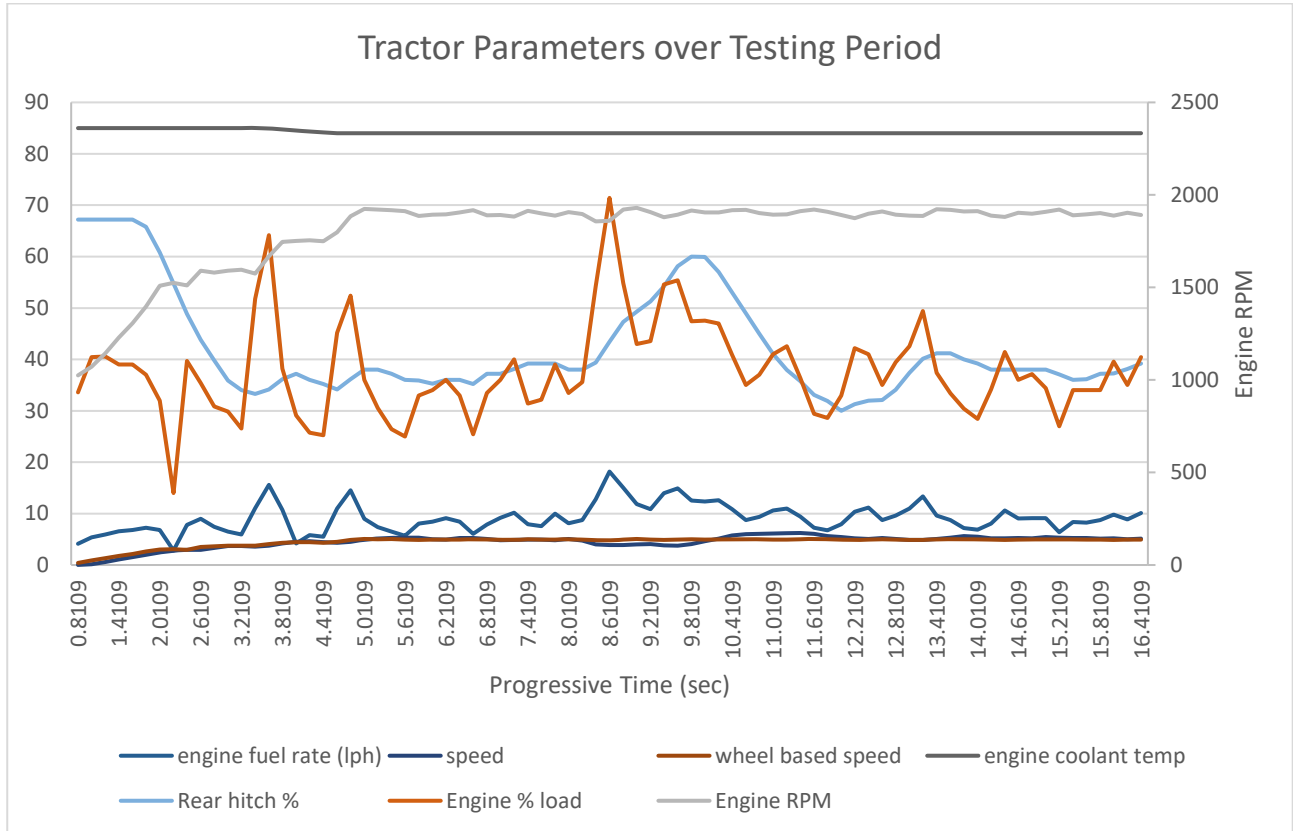
300mm – 3kph

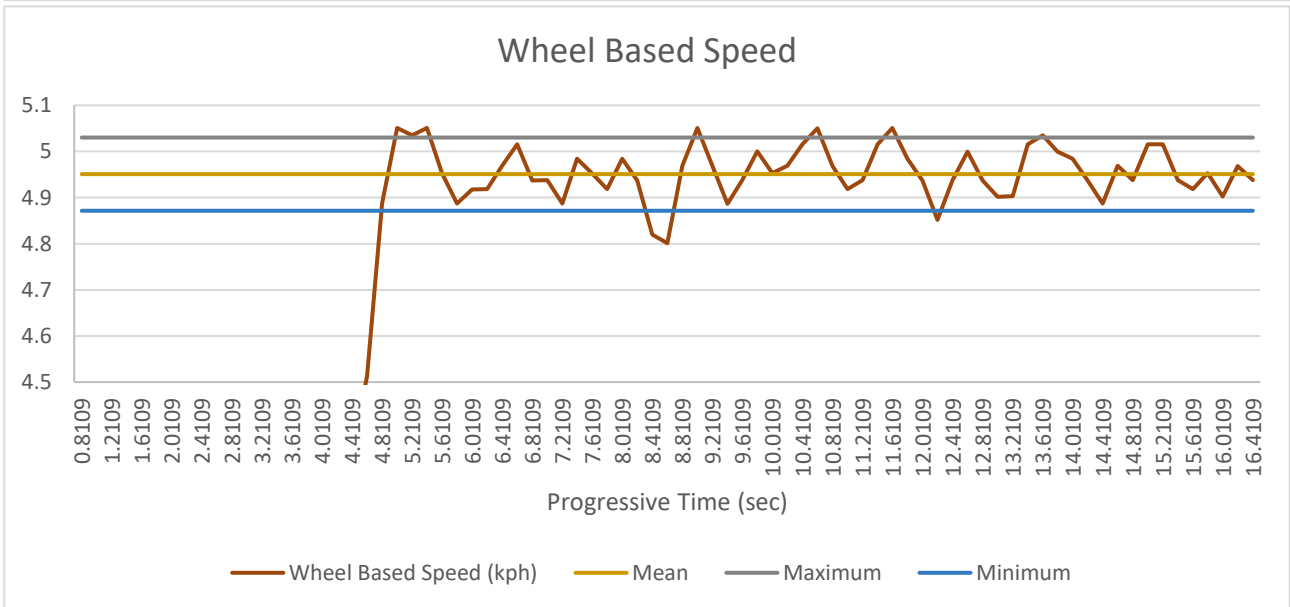
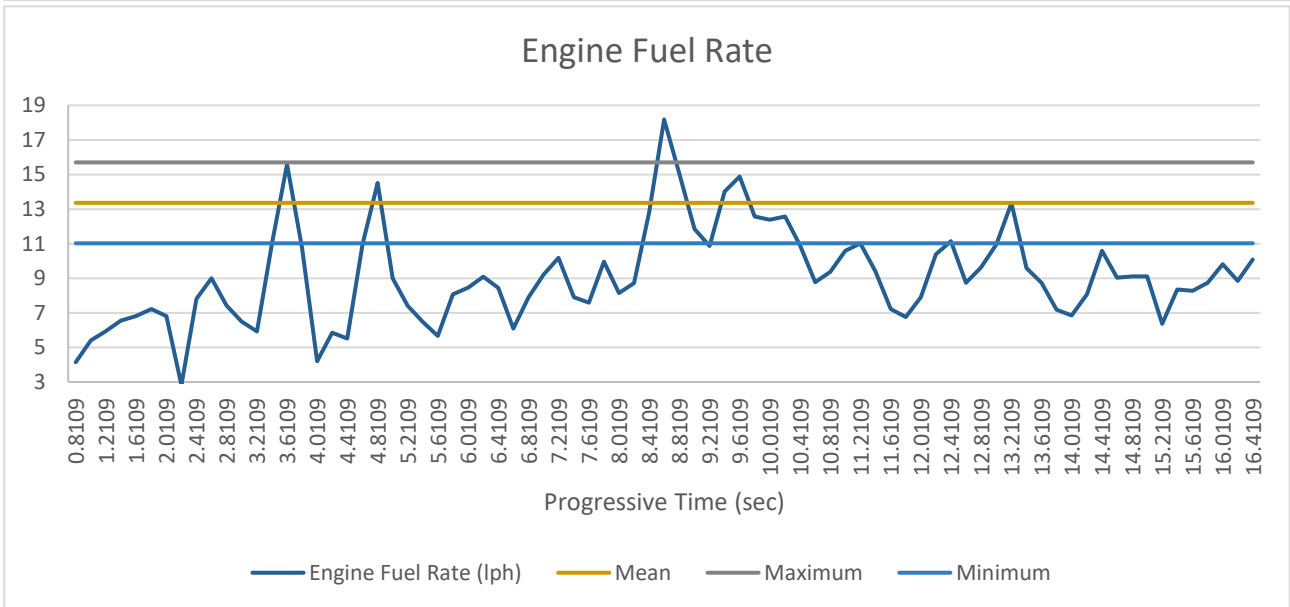
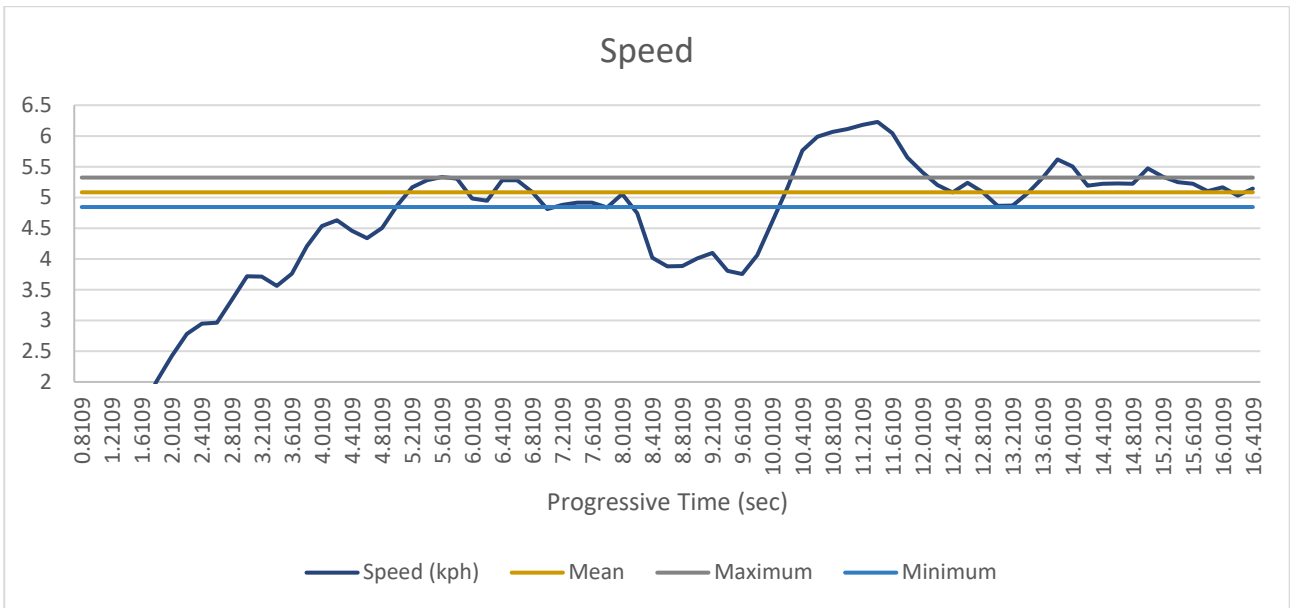


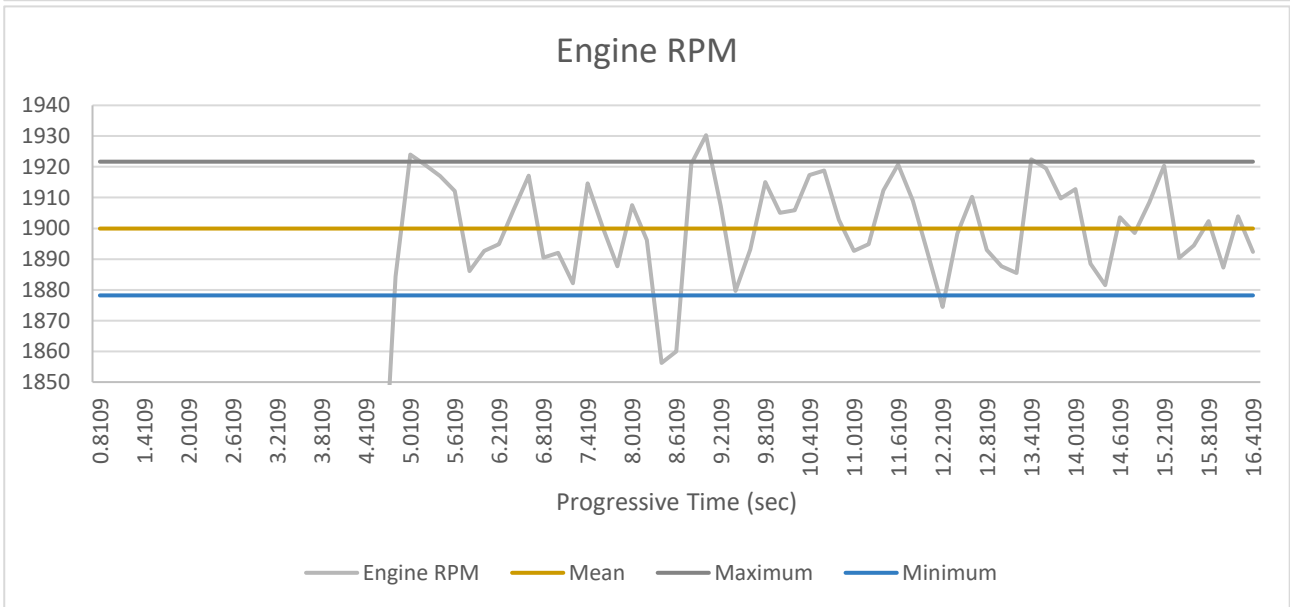
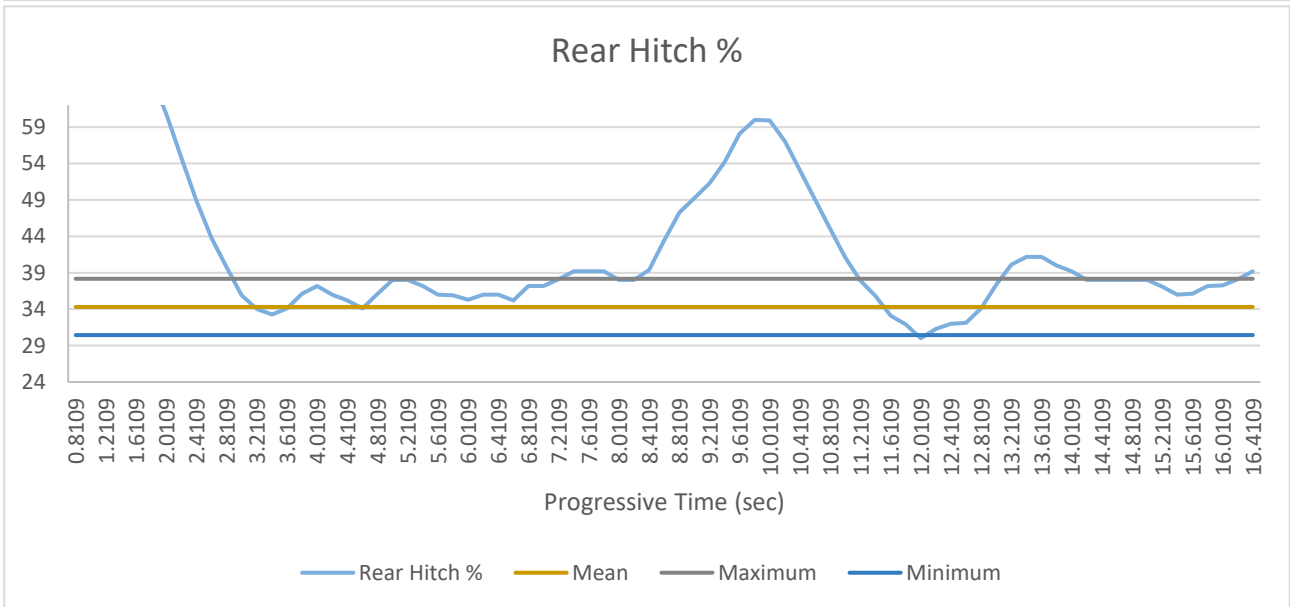
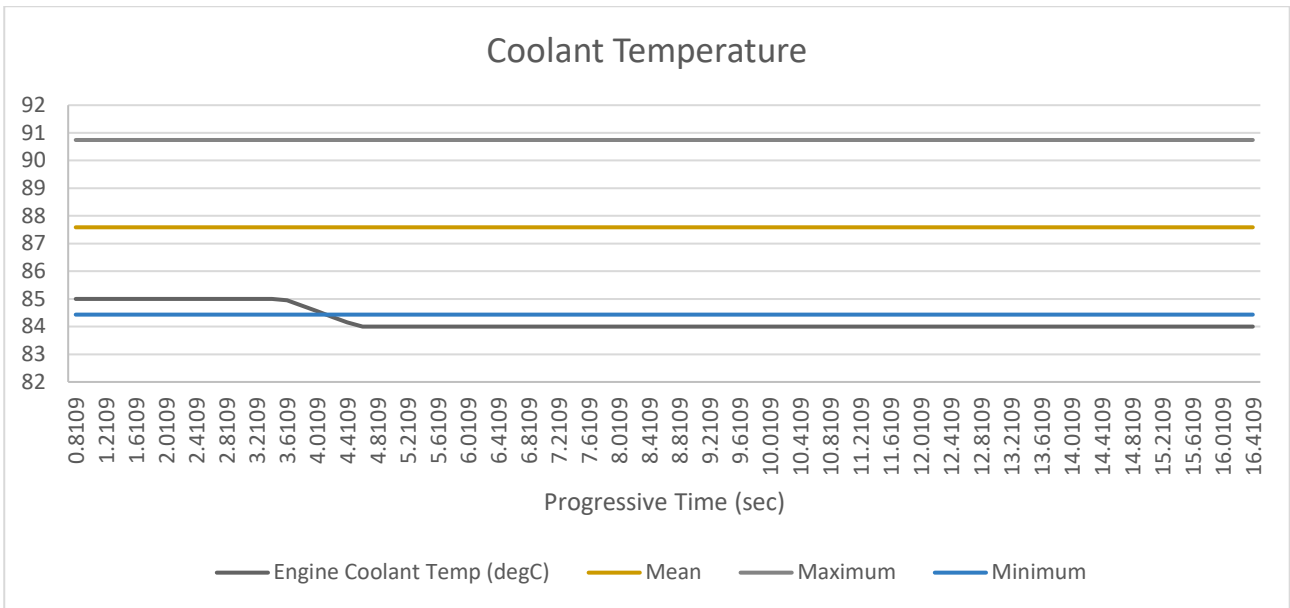




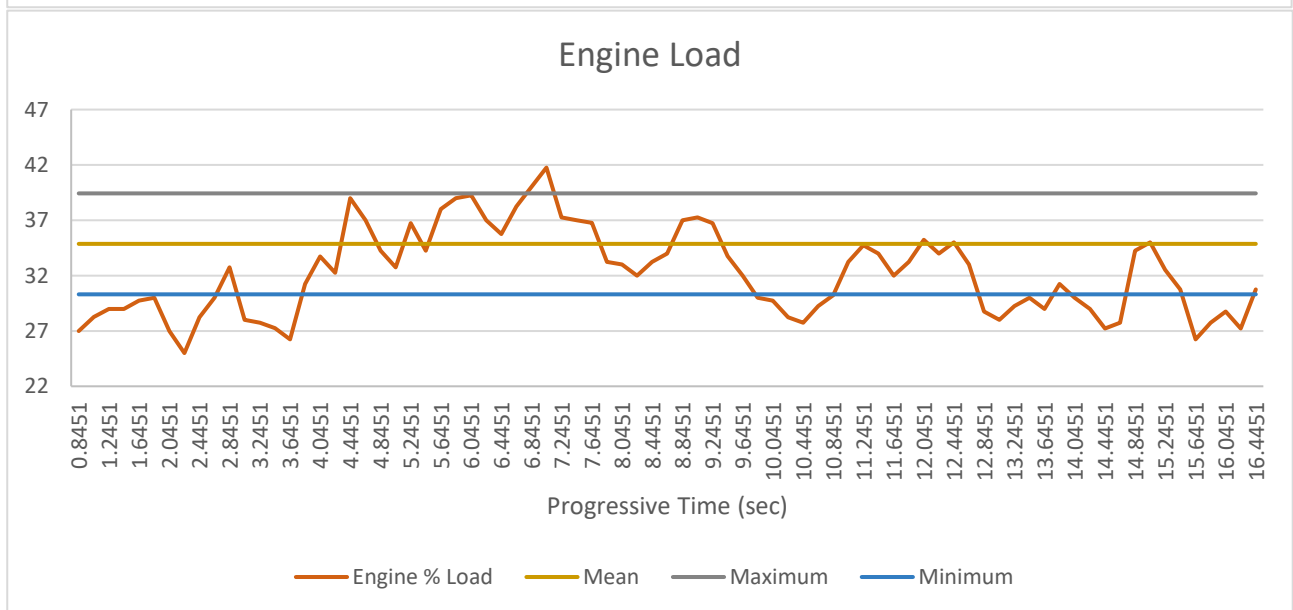
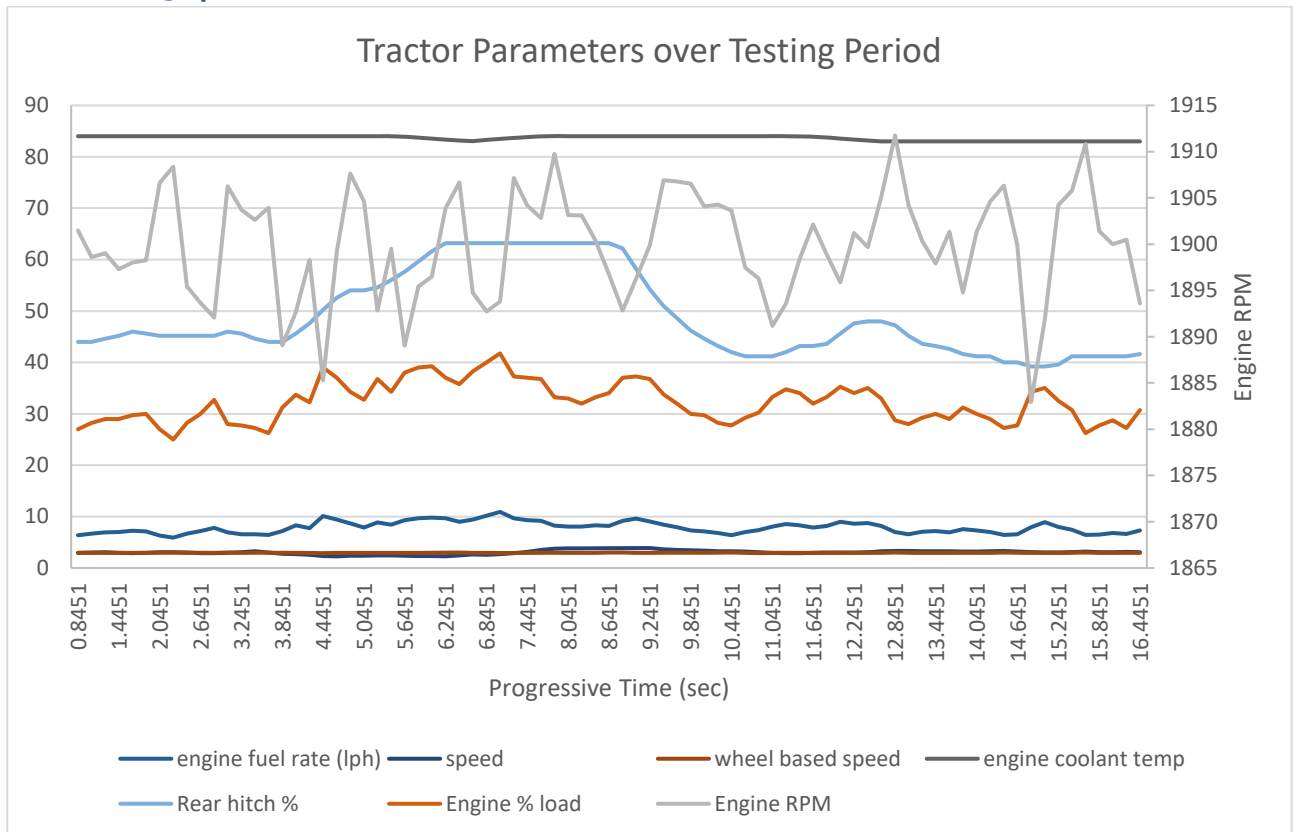
300mm – 5kph

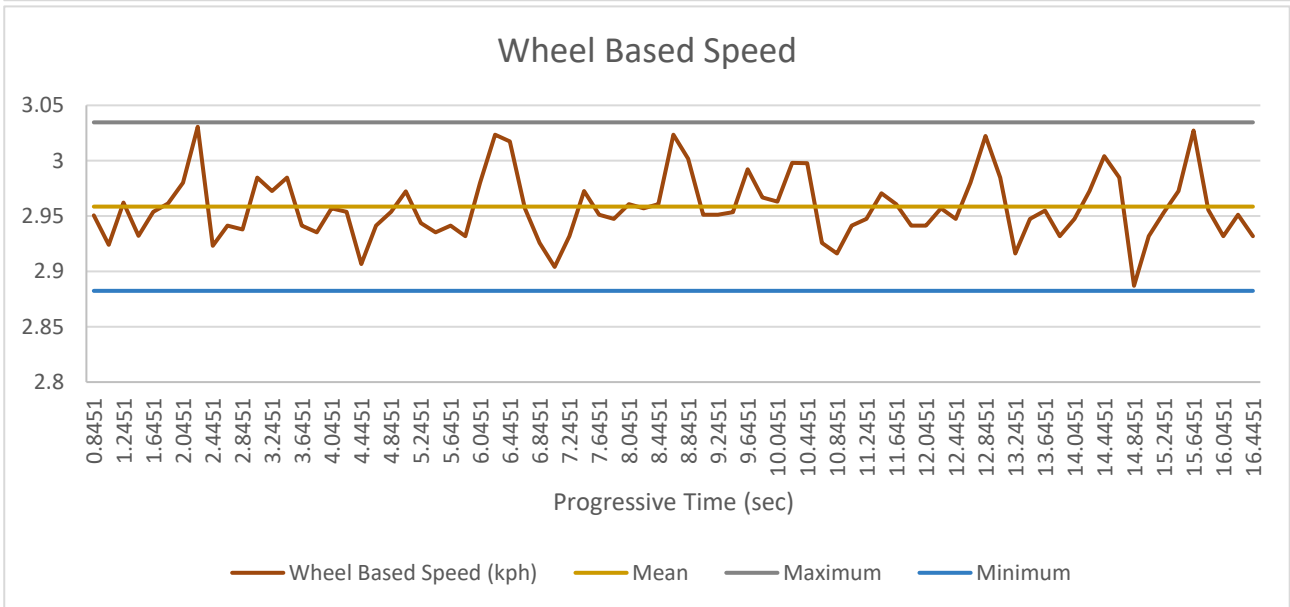
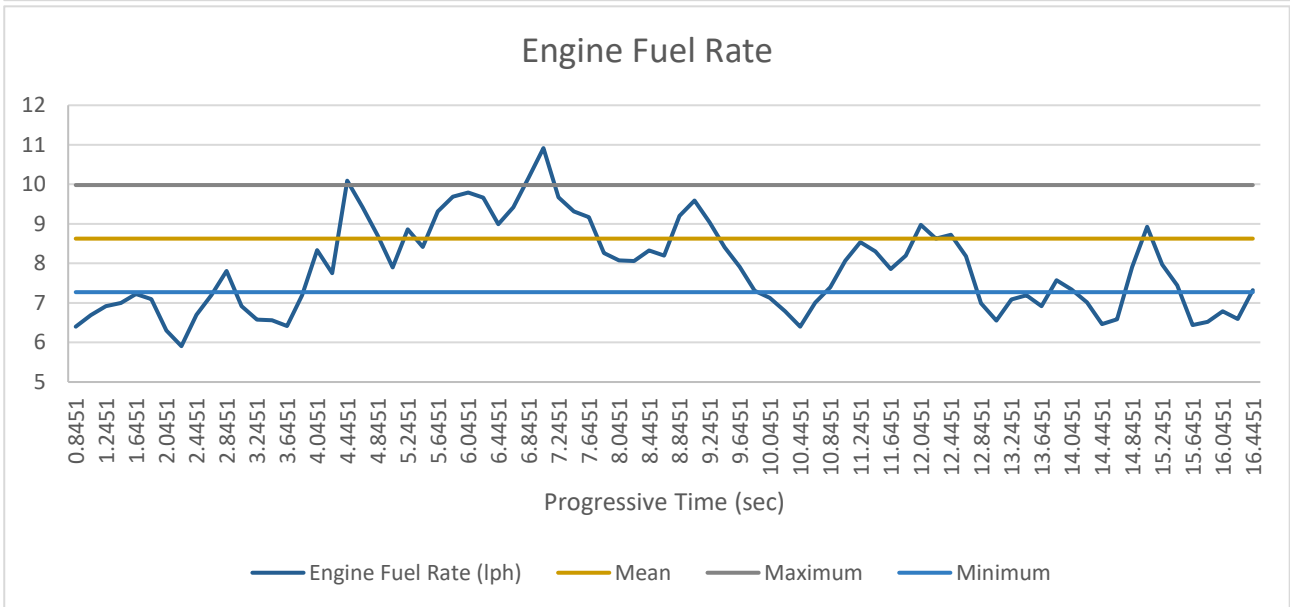
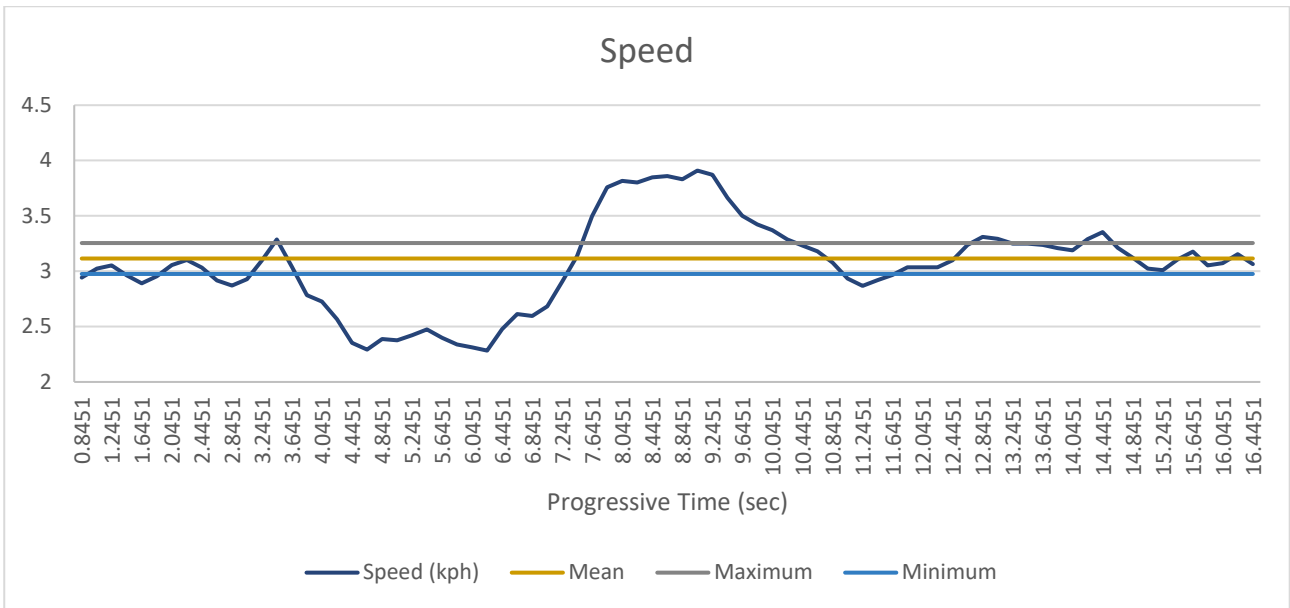


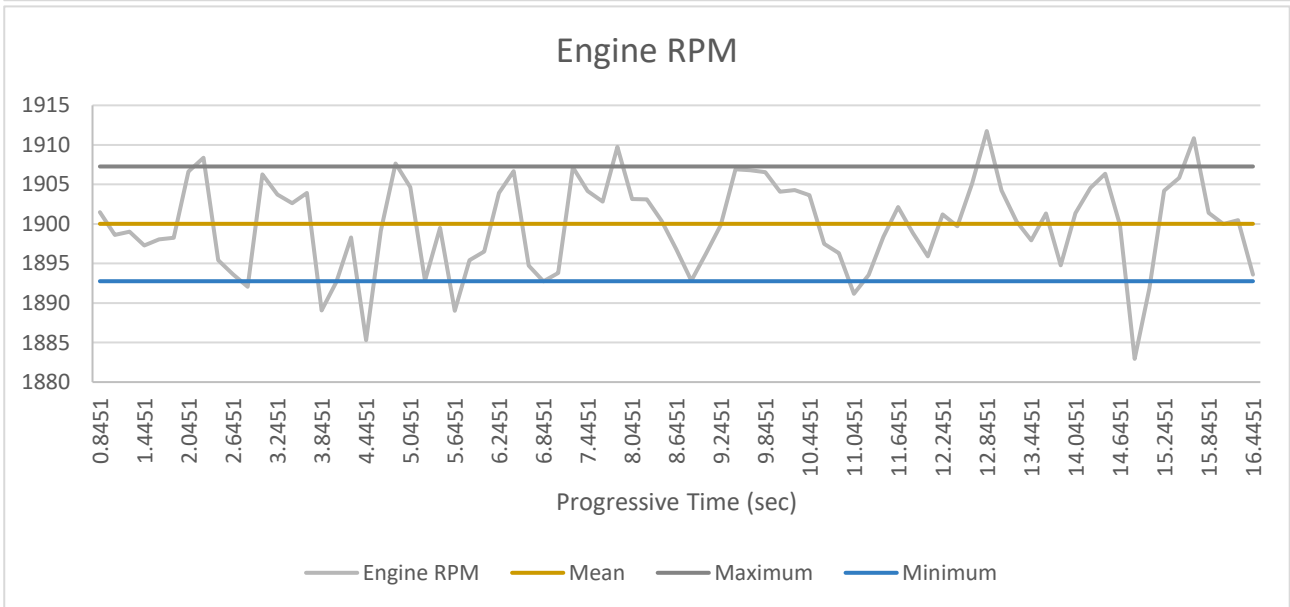
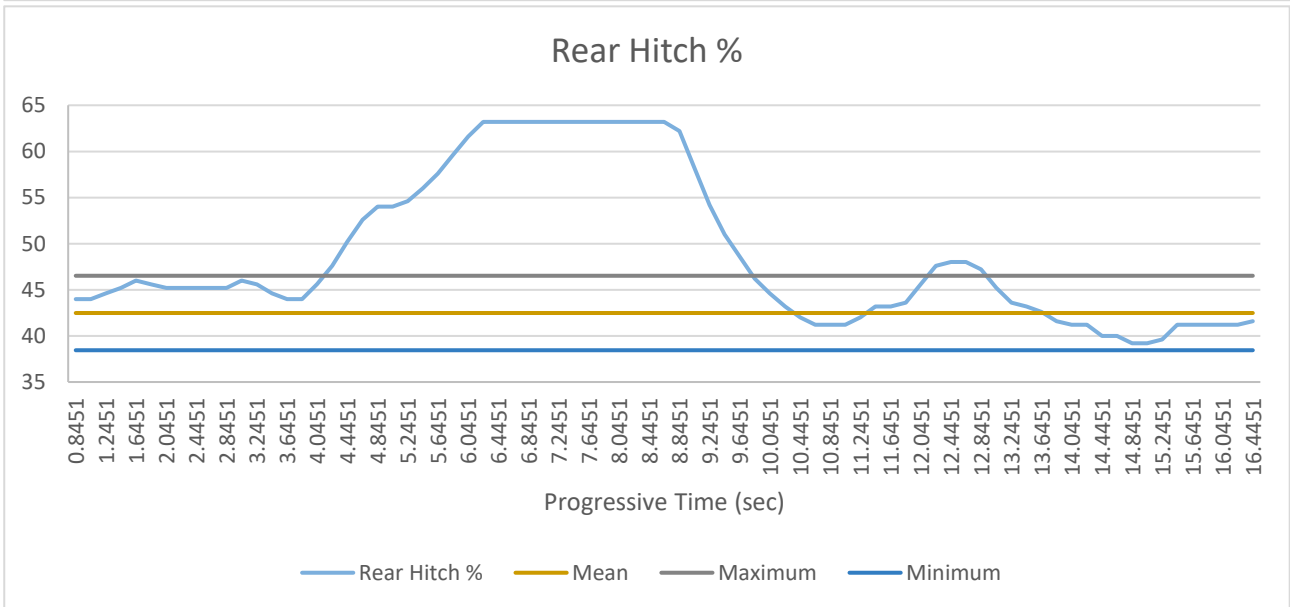
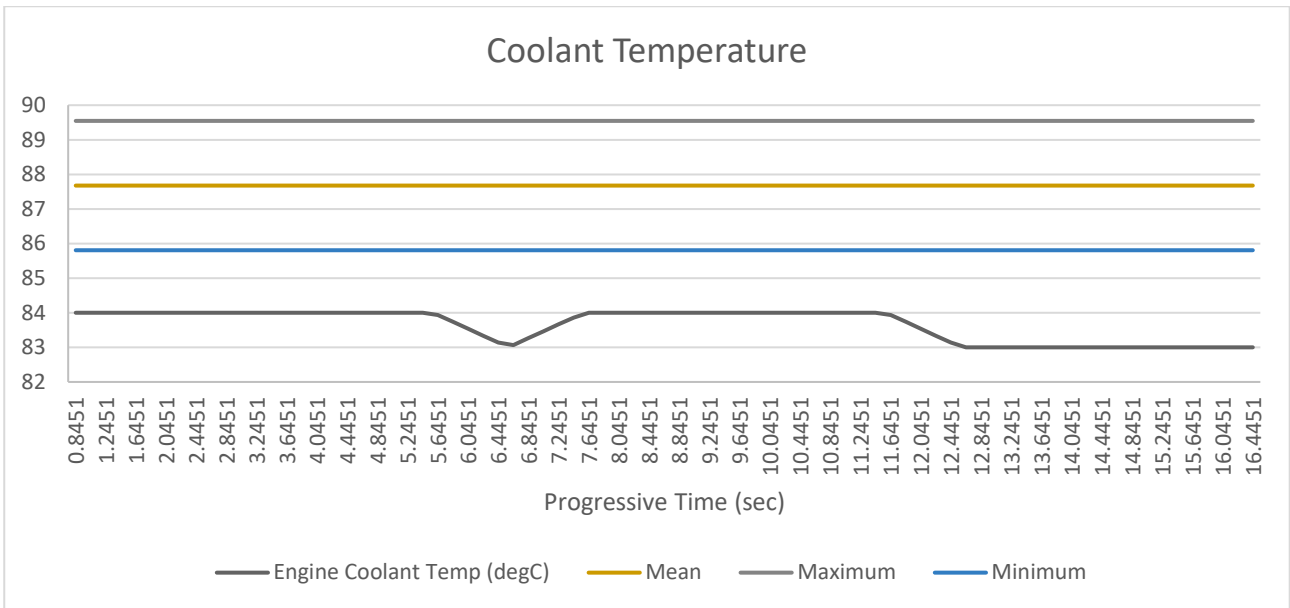




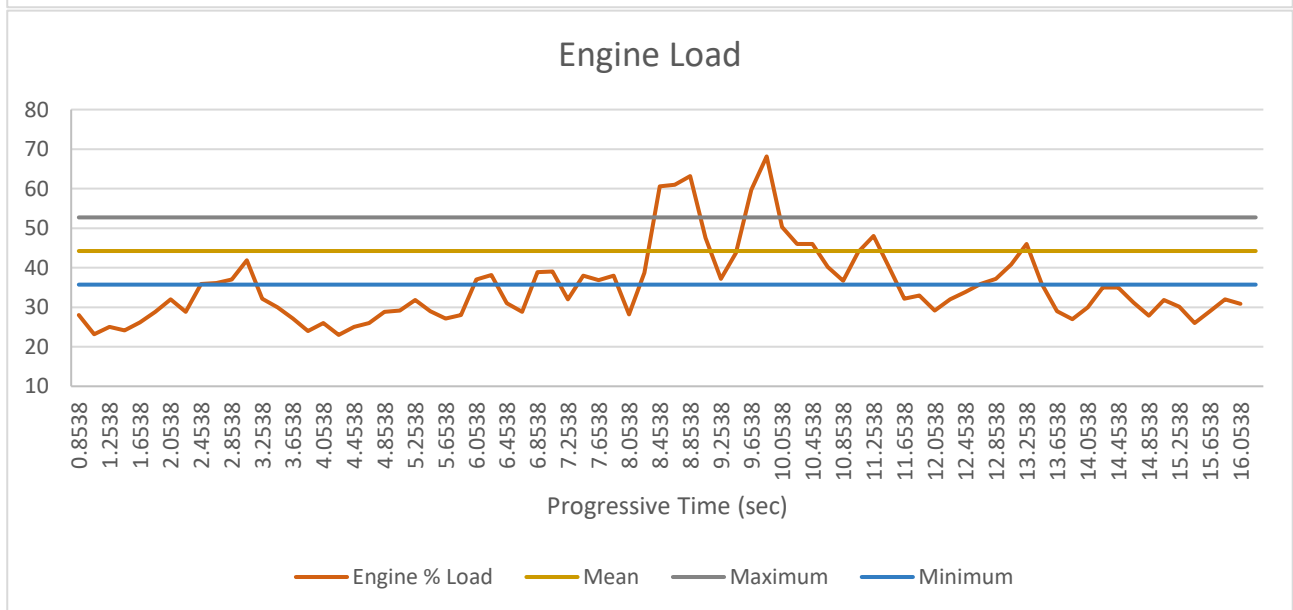
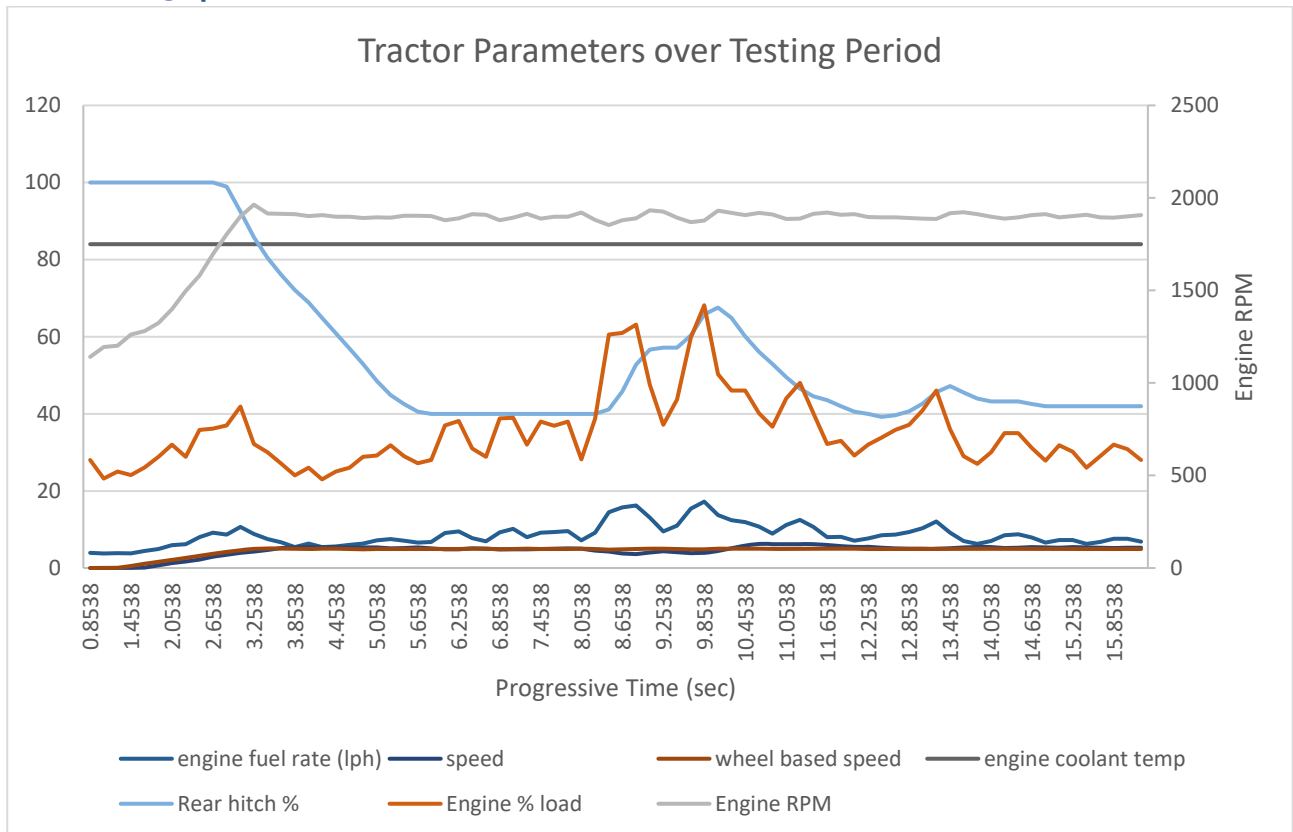
200mm – 3kph

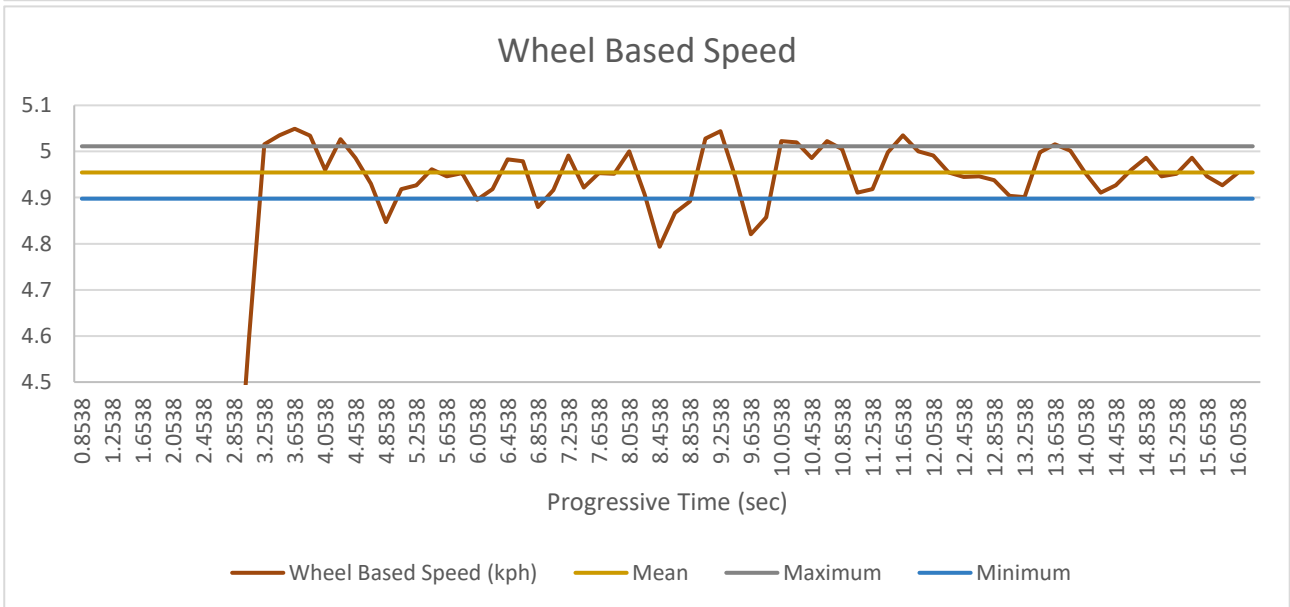
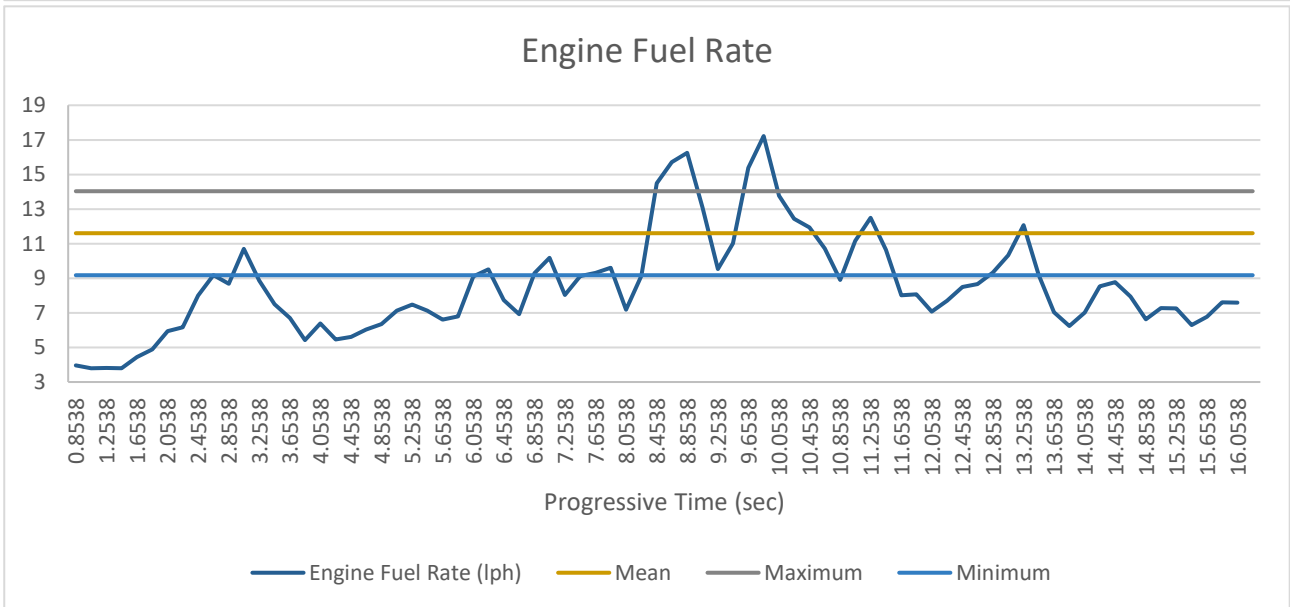
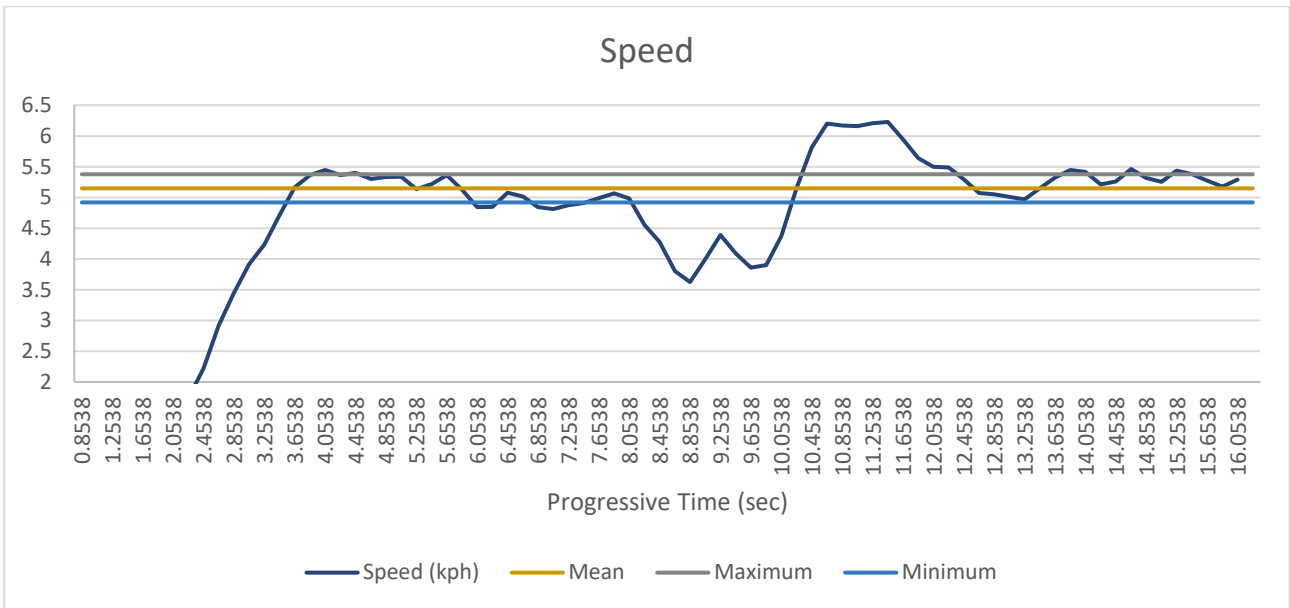




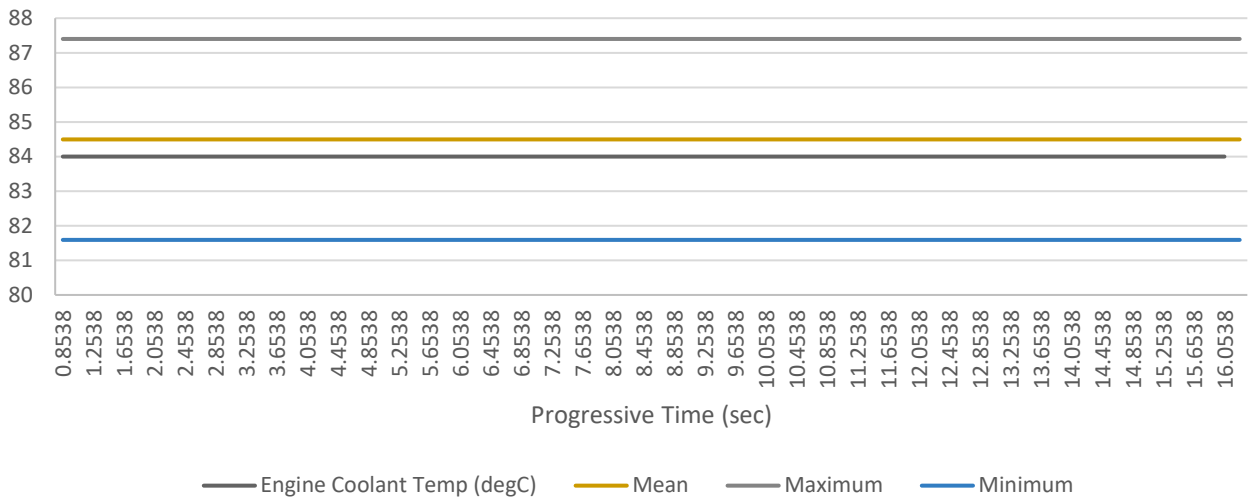


200mm – 5kph

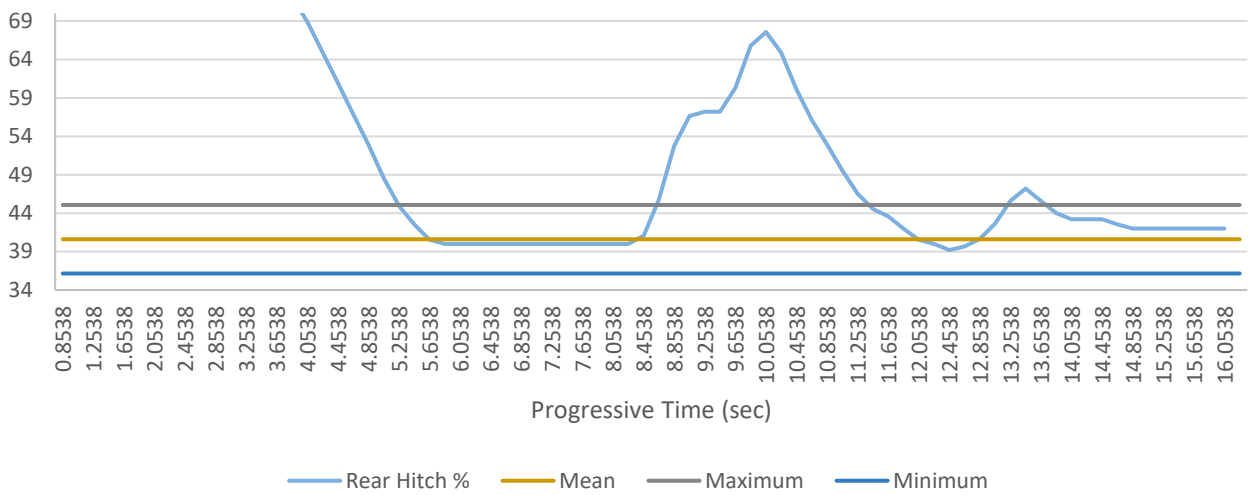




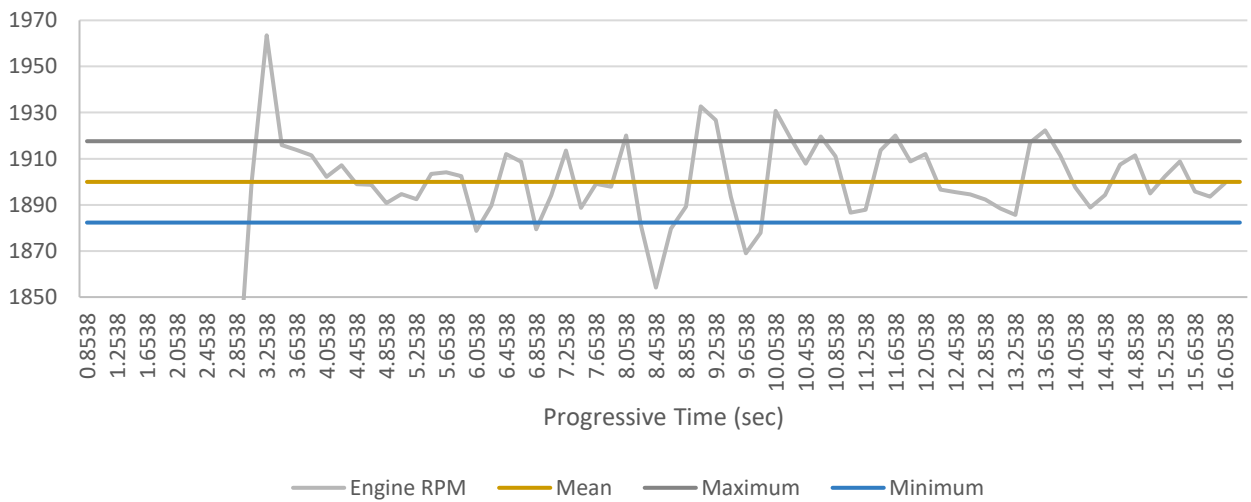
Coolant Temperature



Rear Hitch %

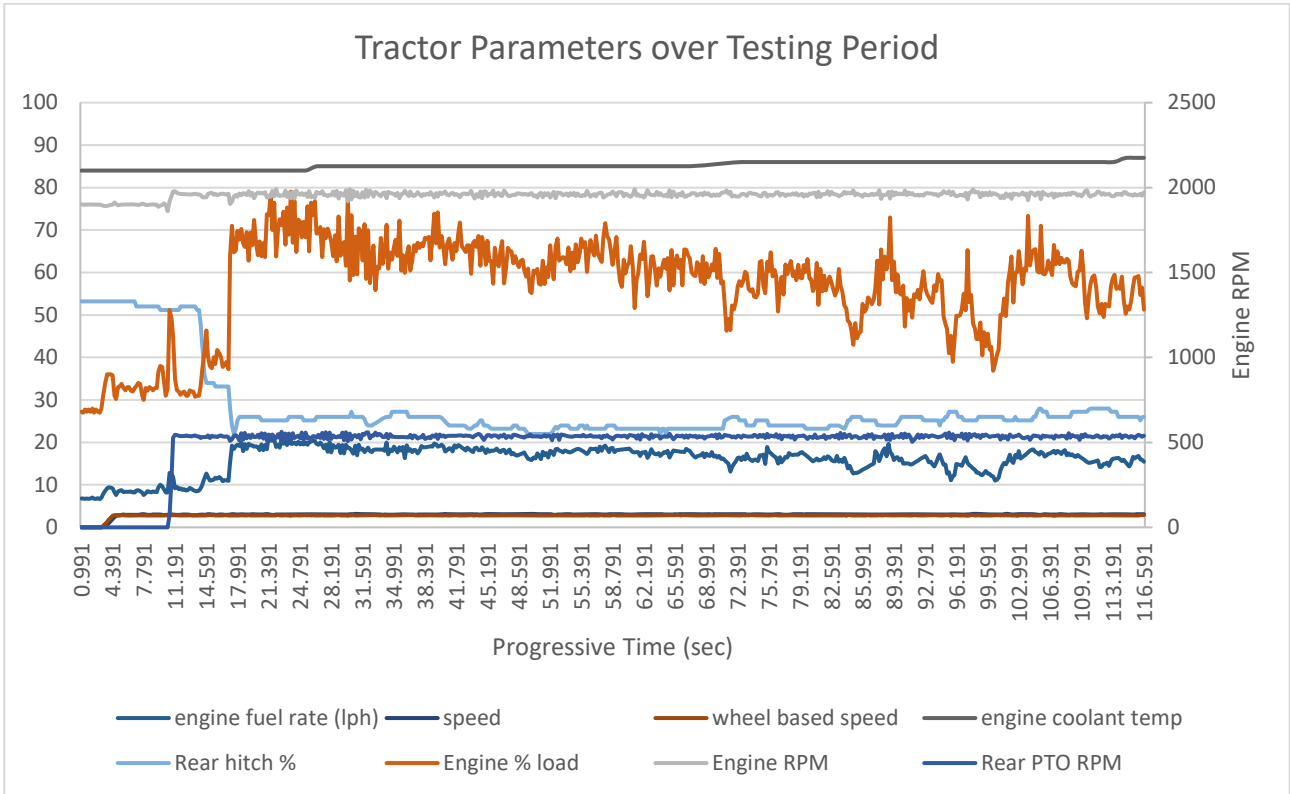


Engine RPM

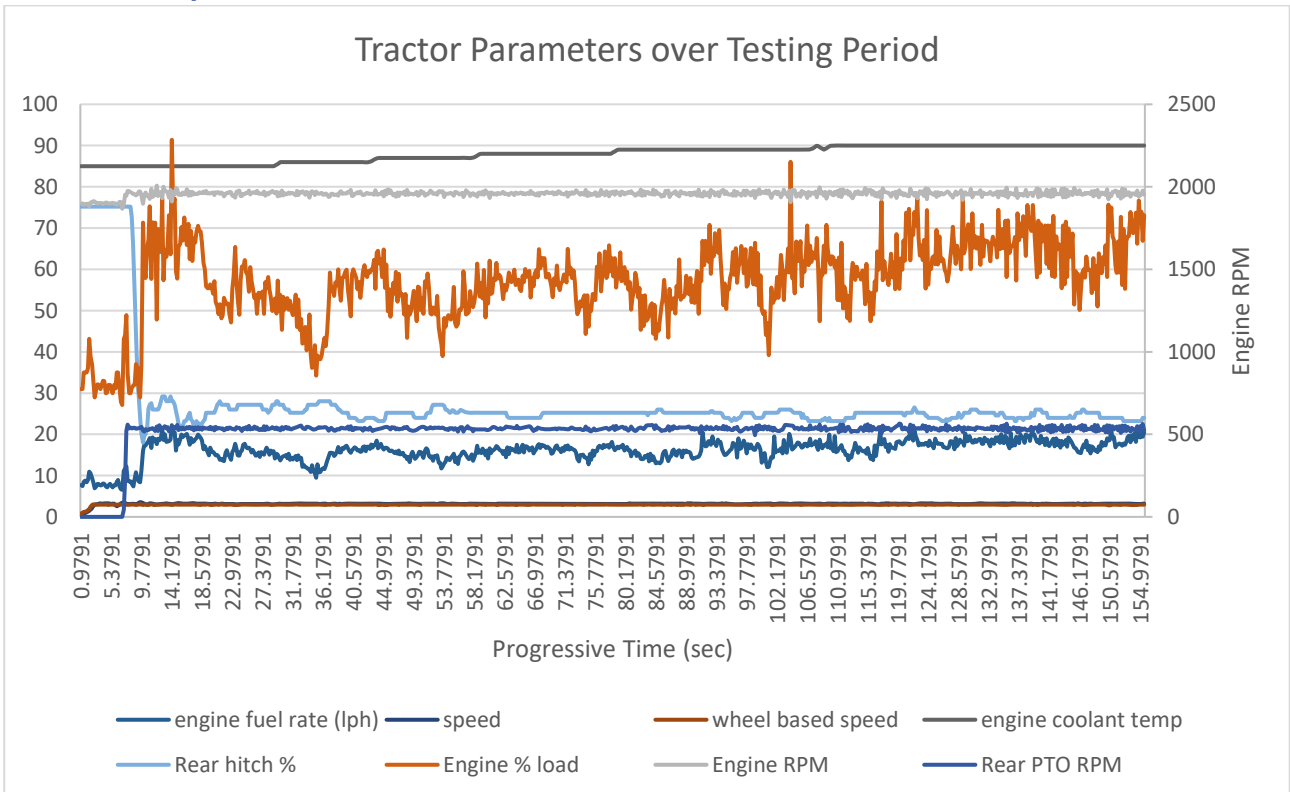


Appendix M – PTO Powered Mulcher – Virgin ground data

150mm - 3kph

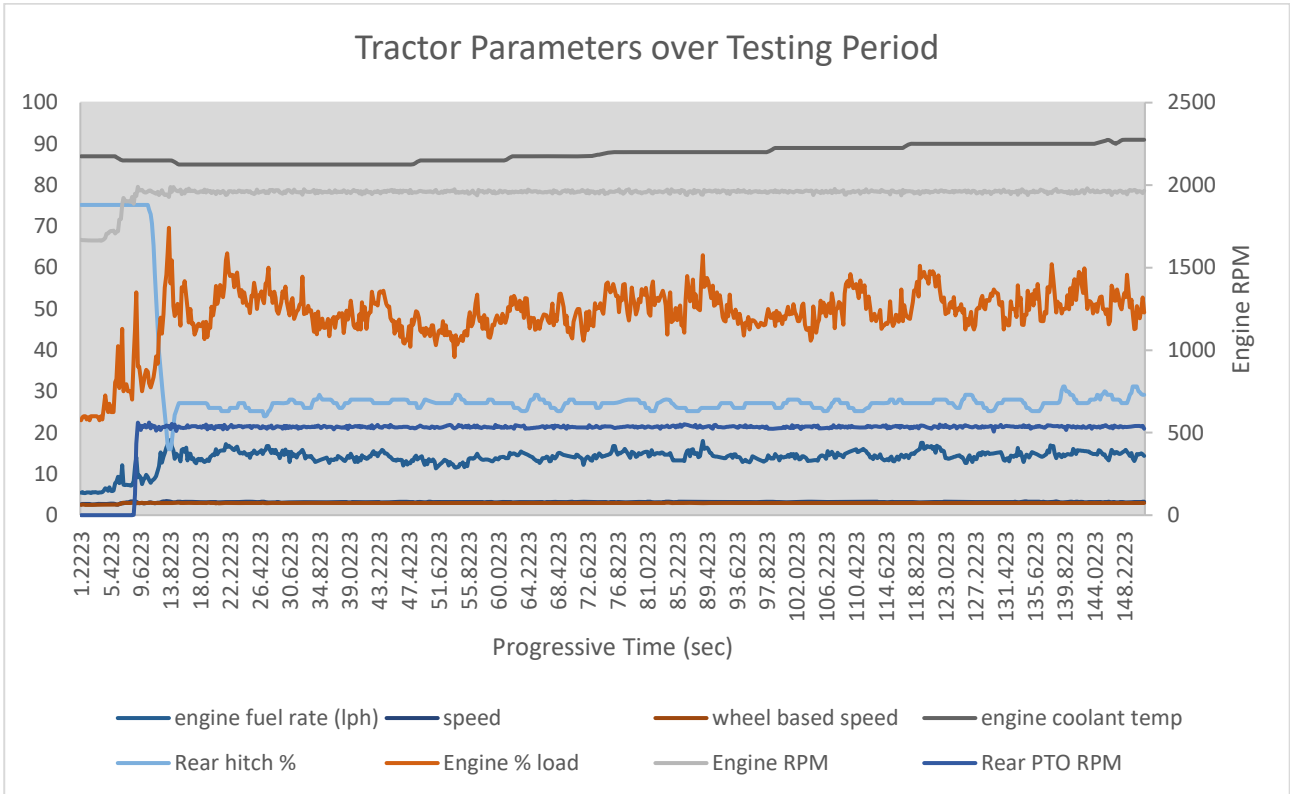


150mm - 3kph – 2

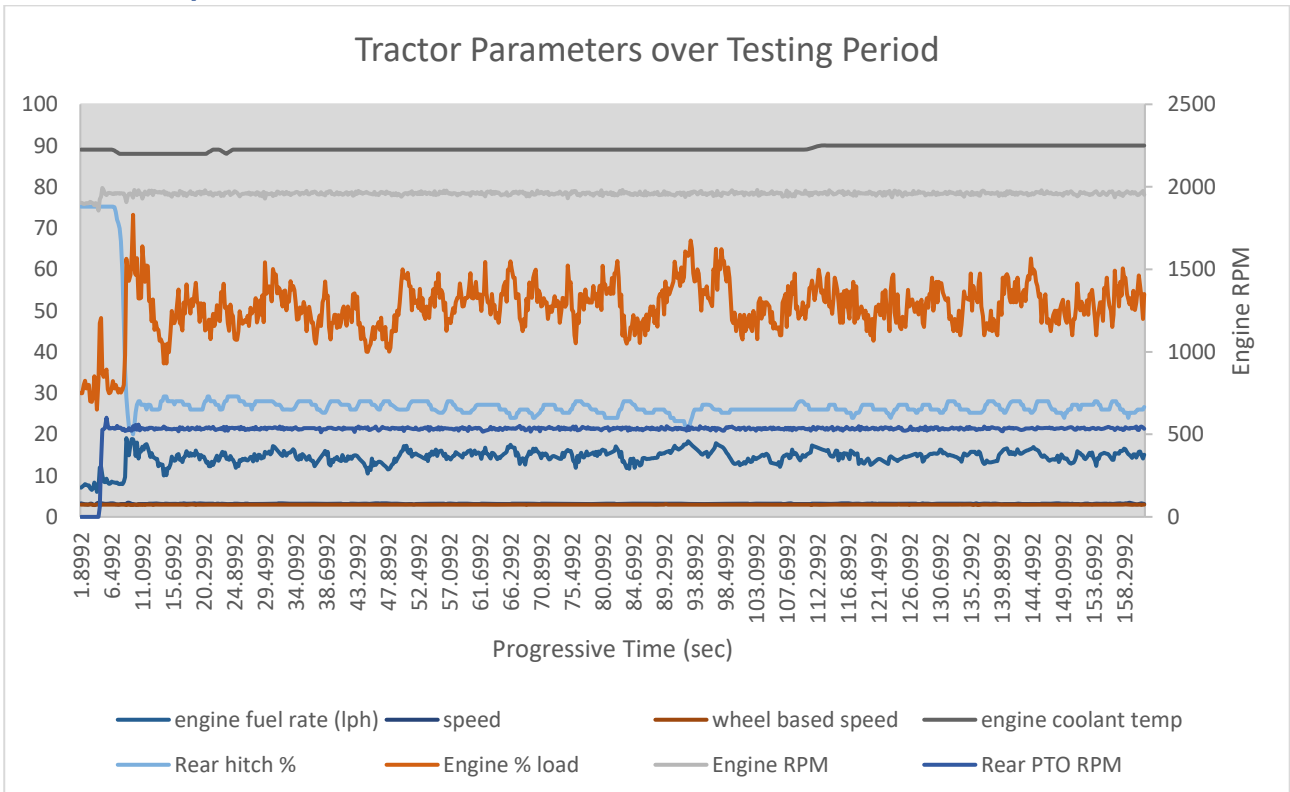


Appendix N – PTO Powered Mulcher – Pre-ripped ground data

150mm - 3kph



150mm - 3kph - 2



Appendix P - USQ Safety Risk Management Plan



UNIVERSITY
OF SOUTHERN
QUEENSLAND

USQ Safety Risk Management System

Safety Risk Management Plan

Risk Management Plan ID: RMP_2022_6782	Status: Approve
Approver: Craig Baillie	Supervisor: Sam Green
Assessment Title: Tractor operation for data collection for research project	
Assessment Date: 2022-03-16	
Workplace (Division/Faculty/Section): 457000 - Centre for Agricultural Engineering	
Review Date:	

Context

DESCRIPTION

What is the task/event/purchase/project/procedure?	Collecting data using the tractors at USQ as well as some of the tillage equipment
Why is it being conducted?	To collect data for a student research project
Where is it being conducted?	Throughout the CAE
Course code (if applicable)	ENG4111
ChemicalName (if applicable)	

WHAT ARE THE NORMAL CONDITIONS?

Personnel involved	Sam Green
Equipment	John Deere tractors, tillage equipment
Environment	Various plots around the CAE
Other	
Briefly explain the procedure/process	Tillage operations will be undertaken using the tractor and then a modification will be made to the implement and the data collected again to allow differences to be identified.

Assessment Team - who is conducting the assessment?

Accessor(s)	Sam Green
Others consulted:	

Draft Approval

Drafters Name:	Sam Green	Draft Date: 2022-03-16
Drafters Comments:		
Assessment Approval:	There are risks not marked as ALARP	
Maximum Residual Risk Level:	Low - Manager/Supervisor Approval Required	

Approval

Approvers Name:	Craig Baillie
Approvers Position Title:	HoS, School of Agriculture and Environmental Science
ApproversComments:	Common Sense is more appropriately termed as assessing the situation before interacting with machinery.
Approval Decision:	Approve
Approval/Reject Date:	2022-03-30

Supporting Attachments

